APPENDIX A

CALEEMOD RESULTS

Stockton & T

Sacramento County, Summer

1.0 Project Characteristics

1.1 Land Usage

| Land Uses | Size | Metric | Lot Acreage | Floor Surface Area | Population |
|----------------------------------|--------|---------------|-------------|--------------------|------------|
| Parking Lot | 96.00 | Space | 0.00 | 38,400.00 | 0 |
| Unenclosed Parking with Elevator | 78.00 | 1000sqft | 0.00 | 78,000.00 | 0 |
| Apartments Mid Rise | 214.00 | Dwelling Unit | 2.92 | 214,000.00 | 571 |
| Single Family Housing | 24.00 | Dwelling Unit | 2.00 | 43,200.00 | 64 |
| Regional Shopping Center | 6.00 | 1000sqft | 0.00 | 6,000.00 | 0 |

1.2 Other Project Characteristics

| Urbanization | Urban | Wind Speed (m/s) | 3.5 | Precipitation Freq (Days) | 58 |
|----------------------------|--------------------------|----------------------------|-------|----------------------------|-------|
| Climate Zone | 6 | | | Operational Year | 2018 |
| Utility Company | Sacramento Municipal Uti | lity District | | | |
| CO2 Intensity (Ib/MWhr) | 590.31 | CH4 Intensity (Ib/MWhr) | 0.029 | N2O Intensity (Ib/MWhr) | 0.006 |

1.3 User Entered Comments & Non-Default Data

Project Characteristics -

Land Use - based on project description

Construction Phase - based on info from applicant

Demolition -

Grading - based on info from applicant

Vehicle Trips - based on info from Transportation Impact Study

Area Mitigation -

Energy Mitigation -

| Table Name | Column Name | Default Value | New Value |
|---------------------------|------------------|---------------|-----------|
| tblConstructionPhase | NumDays | 18.00 | 348.00 |
| tblConstructionPhase | NumDays | 230.00 | 348.00 |
| tblConstructionPhase | NumDays | 20.00 | 44.00 |
| tblConstructionPhase | NumDays | 8.00 | 16.00 |
| tblConstructionPhase | NumDays | 18.00 | 11.00 |
| tblConstructionPhase | PhaseEndDate | 5/16/2019 | 1/29/2018 |
| tblConstructionPhase | PhaseStartDate | 1/16/2018 | 9/29/2016 |
| tblGrading | AcresOfGrading | 8.00 | 2.90 |
| tblGrading | MaterialImported | 0.00 | 2,000.00 |
| tblLandUse | LotAcreage | 0.86 | 0.00 |
| tblLandUse | LotAcreage | 1.79 | 0.00 |
| tblLandUse | LotAcreage | 5.63 | 2.92 |
| tblLandUse | LotAcreage | 7.79 | 2.00 |
| tblLandUse | LotAcreage | 0.14 | 0.00 |
| tblProjectCharacteristics | OperationalYear | 2014 | 2018 |
| tblVehicleTrips | ST_TR | 7.16 | 4.32 |
| tblVehicleTrips | ST_TR | 49.97 | 28.11 |
| tblVehicleTrips | ST_TR | 10.08 | 8.15 |
| tblVehicleTrips | SU_TR | 6.07 | 4.32 |
| tblVehicleTrips | SU_TR | 25.24 | 28.11 |
| tblVehicleTrips | SU_TR | 8.77 | 8.15 |
| tblVehicleTrips | WD_TR | 6.59 | 4.32 |
| tblVehicleTrips | WD_TR | 42.94 | 28.11 |
| tblVehicleTrips | WD_TR | 9.57 | 8.15 |
| | | - | · |

2.0 Emissions Summary

2.1 Overall Construction (Maximum Daily Emission)

Unmitigated Construction

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|-------|---------|----------|----------|--------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------------|-----------------|--------|--------|-----------------|
| Year | | | | | lb/d | day | | | | | | | lb/c | lay | | |
| 2016 | 18.0121 | 54.6972 | 41.9739 | 0.0644 | 18.2032 | 2.9397 | 21.1429 | 9.9670 | 2.7045 | 12.6715 | 0.0000 | 5,965.673 9 | 5,965.673 9 | 1.2331 | 0.0000 | 5,991.569 0 |
| 2017 | 17.4839 | 32.6909 | 36.9047 | 0.0644 | 2.2253 | 2.0195 | 4.2447 | 0.5955 | 1.9060 | 2.5015 | 0.0000 | 5,838.995 4 | 5,838.995 4 | 0.7770 | 0.0000 | 5,855.312 5 |
| 2018 | 16.8411 | 28.9622 | 34.4666 | 0.0643 | 2.2252 | 1.7053 | 3.9305 | 0.5955 | 1.6110 | 2.2065 | 0.0000 | 5,717.237 9 | 5,717.237 9 | 0.7556 | 0.0000 | 5,733.106 2 |
| Total | 52.3371 | 116.3503 | 113.3452 | 0.1931 | 22.6537 | 6.6645 | 29.3182 | 11.1580 | 6.2215 | 17.3796 | 0.0000 | 17,521.90 72 | 17,521.90 72 | 2.7657 | 0.0000 | 17,579.98 76 |

Mitigated Construction

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|-------|---------|----------|----------|--------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------------|-----------------|--------|--------|-----------------|
| Year | | | | | lb/o | day | | | | | | | lb/c | lay | | |
| 2016 | 18.0121 | 54.6972 | 41.9739 | 0.0644 | 18.2032 | 2.9397 | 21.1429 | 9.9670 | 2.7045 | 12.6715 | 0.0000 | 5,965.673 8 | 5,965.673 8 | 1.2331 | 0.0000 | 5,991.569 0 |
| 2017 | 17.4839 | 32.6909 | 36.9047 | 0.0644 | 2.2253 | 2.0195 | 4.2447 | 0.5955 | 1.9060 | 2.5015 | 0.0000 | 5,838.995 4 | 5,838.995 4 | 0.7770 | 0.0000 | 5,855.312 5 |
| 2018 | 16.8411 | 28.9622 | 34.4666 | 0.0643 | 2.2252 | 1.7053 | 3.9305 | 0.5955 | 1.6110 | 2.2065 | 0.0000 | 5,717.237 9 | 5,717.237 9 | 0.7556 | 0.0000 | 5,733.106 2 |
| Total | 52.3371 | 116.3503 | 113.3452 | 0.1931 | 22.6537 | 6.6645 | 29.3182 | 11.1580 | 6.2215 | 17.3796 | 0.0000 | 17,521.90 71 | 17,521.90 71 | 2.7657 | 0.0000 | 17,579.98 76 |

| | ROG | NOx | со | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio-CO2 | Total CO2 | CH4 | N20 | CO2e |
|----------------------|------|------|------|------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------|-----------|------|------|------|
| Percent Reduction | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

2.2 Overall Operational

Unmitigated Operational

| | ROG | NOx | СО | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|---------|--------|---------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|--------|--------|----------------|
| Category | | | | | lb/ | day | | | | | | | lb/c | day | | |
| Area | 9.9410 | 0.2297 | 19.7928 | 1.0400e- 003 | | 0.1080 | 0.1080 | | 0.1080 | 0.1080 | 0.0000 | 35.3948 | 35.3948 | 0.0352 | 0.0000 | 36.1329 |
| Energy | 0.0869 | 0.7430 | 0.3200 | 4.7400e- 003 | | 0.0600 | 0.0600 | | 0.0600 | 0.0600 | | 947.8553 | 947.8553 | 0.0182 | 0.0174 | 953.6238 |
| Mobile | 4.4477 | 7.9851 | 42.6133 | 0.0990 | 6.5850 | 0.1178 | 6.7027 | 1.7591 | 0.1085 | 1.8675 | | 8,018.471 8 | 8,018.471 8 | 0.3017 | | 8,024.807 5 |
| Total | 14.4756 | 8.9578 | 62.7260 | 0.1048 | 6.5850 | 0.2858 | 6.8708 | 1.7591 | 0.2765 | 2.0356 | 0.0000 | 9,001.721 9 | 9,001.721 9 | 0.3550 | 0.0174 | 9,014.564 2 |

Mitigated Operational

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|---------|--------|---------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|--------|--------|----------------|
| Category | | | | | lb/o | day | | | | | | | lb/c | lay | | |
| Area | 9.3337 | 0.2297 | 19.7928 | 1.0400e- 003 | | 0.1080 | 0.1080 | | 0.1080 | 0.1080 | 0.0000 | 35.3948 | 35.3948 | 0.0352 | 0.0000 | 36.1329 |
| Energy | 0.0690 | 0.5898 | 0.2540 | 3.7600e- 003 | | 0.0477 | 0.0477 | | 0.0477 | 0.0477 | | 752.4113 | 752.4113 | 0.0144 | 0.0138 | 756.9904 |
| Mobile | 4.4477 | 7.9851 | 42.6133 | 0.0990 | 6.5850 | 0.1178 | 6.7027 | 1.7591 | 0.1085 | 1.8675 | | 8,018.471 8 | 8,018.471 8 | 0.3017 | | 8,024.807 5 |
| Total | 13.8504 | 8.8046 | 62.6600 | 0.1038 | 6.5850 | 0.2734 | 6.8584 | 1.7591 | 0.2641 | 2.0232 | 0.0000 | 8,806.277 9 | 8,806.277 9 | 0.3513 | 0.0138 | 8,817.930 8 |

| | ROG | NOx | со | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio-CO2 | Total CO2 | CH4 | N20 | CO2e |
|----------------------|------|------|------|------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------|-----------|------|-------|------|
| Percent Reduction | 4.32 | 1.71 | 0.11 | 0.94 | 0.00 | 4.33 | 0.18 | 0.00 | 4.48 | 0.61 | 0.00 | 2.17 | 2.17 | 1.06 | 20.66 | 2.18 |

3.0 Construction Detail

Construction Phase

| Phase Number | Phase Name | Phase Type | Start Date | End Date | Num Days Week | Num Days | Phase Description |
|-----------------|-----------------------|-----------------------|------------|-----------|------------------|----------|-------------------|
| 1 | Demolition | Demolition | 6/1/2016 | 8/1/2016 | 5 | 44 | |
| 2 | Site Preparation | Site Preparation | 8/2/2016 | 8/8/2016 | 5 | 5 | |
| 3 | Grading | Grading | 8/9/2016 | 8/30/2016 | 5 | 16 | |
| 4 | Paving | Paving | 8/31/2016 | 9/14/2016 | 5 | 11 | |
| 5 | Building Construction | Building Construction | 9/15/2016 | 1/15/2018 | 5 | 348 | |
| 6 | Architectural Coating | Architectural Coating | 9/29/2016 | 1/29/2018 | 5 | 348 | |

Acres of Grading (Site Preparation Phase): 0

Acres of Grading (Grading Phase): 2.9

Acres of Paving: 0

Residential Indoor: 520,830; Residential Outdoor: 173,610; Non-Residential Indoor: 127,728; Non-Residential Outdoor: 42,576 (Architectural Coating – sqft)

OffRoad Equipment

| Phase Name | Offroad Equipment Type | Amount | Usage Hours | Horse Power | Load Factor |
|-----------------------|---------------------------|--------|-------------|-------------|-------------|
| Demolition | Concrete/Industrial Saws | 1 | 8.00 | 81 | 0.73 |
| Demolition | Excavators | 3 | 8.00 | 162 | 0.38 |
| Demolition | Rubber Tired Dozers | 2 | 8.00 | 255 | 0.40 |
| Site Preparation | Rubber Tired Dozers | 3 | 8.00 | 255 | 0.40 |
| Site Preparation | Tractors/Loaders/Backhoes | 4 | 8.00 | 97 | 0.37 |
| Grading | Excavators | 1 | 8.00 | 162 | 0.38 |
| Grading | Graders | 1 | 8.00 | 174 | 0.41 |
| Grading | Rubber Tired Dozers | 1 | 8.00 | 255 | 0.40 |
| Grading | Tractors/Loaders/Backhoes | 3 | 8.00 | 97 | 0.37 |
| Paving | Cement and Mortar Mixers | 2 | 6.00 | 9 | 0.56 |
| Paving | Pavers | 1 | 8.00 | 125 | 0.42 |
| Paving | Paving Equipment | 2 | 6.00 | 130 | 0.36 |
| Paving | Rollers | 2 | 6.00 | 80 | 0.38 |
| Paving | Tractors/Loaders/Backhoes | 1 | 8.00 | 97 | 0.37 |
| Building Construction | Cranes | 1 | 7.00 | 226 | 0.29 |
| Building Construction | Forklifts | 3 | 8.00 | 89 | 0.20 |
| Building Construction | Generator Sets | 1 | 8.00 | 84 | 0.74 |
| Building Construction | Tractors/Loaders/Backhoes | 3 | 7.00 | 97 | 0.37 |
| Building Construction | Welders | 1 | 8.00 | 46 | 0.45 |
| Architectural Coating | Air Compressors | 1 | 6.00 | 78 | 0.48 |

Trips and VMT

| Phase Name | Offroad Equipment Count | Worker Trip Number | Vendor Trip Number | Hauling Trip Number | Worker Trip Length | Vendor Trip Length | Hauling Trip Length | Worker Vehicle Class | Vendor Vehicle Class | Hauling Vehicle Class |
|-----------------------|----------------------------|-----------------------|-----------------------|------------------------|-----------------------|-----------------------|------------------------|-------------------------|-------------------------|--------------------------|
| Demolition | 6 | 15.00 | 0.00 | 546.00 | 10.00 | 6.50 | 20.00 | LD_Mix | HDT_Mix | HHDT |
| Site Preparation | 7 | 18.00 | 0.00 | 0.00 | 10.00 | 6.50 | 20.00 | LD_Mix | HDT_Mix | HHDT |
| Grading | 6 | 15.00 | 0.00 | 198.00 | 10.00 | 6.50 | 20.00 | LD_Mix | HDT_Mix | HHDT |
| Paving | 8 | 20.00 | 0.00 | 0.00 | 10.00 | 6.50 | 20.00 | LD_Mix | HDT_Mix | HHDT |
| Building Construction | 9 | 214.00 | 46.00 | 0.00 | 10.00 | 6.50 | 20.00 | LD_Mix | HDT_Mix | HHDT |
| Architectural Coating | 1 | 43.00 | 0.00 | 0.00 | 10.00 | 6.50 | 20.00 | LD_Mix | HDT_Mix | HHDT |

3.1 Mitigation Measures Construction

3.2 Demolition - 2016

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|---------------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|--------|-----|----------------|
| Category | | | | | lb/e | day | | | | | | | lb/c | day | | |
| Fugitive Dust | | | | | 2.7989 | 0.0000 | 2.7989 | 0.4238 | 0.0000 | 0.4238 | - | | 0.0000 | | | 0.0000 |
| Off-Road | 4.2876 | 45.6559 | 35.0303 | 0.0399 | | 2.2921 | 2.2921 | | 2.1365 | 2.1365 | | 4,089.284 1 | 4,089.284 1 | 1.1121 | | 4,112.637 4 |
| Total | 4.2876 | 45.6559 | 35.0303 | 0.0399 | 2.7989 | 2.2921 | 5.0910 | 0.4238 | 2.1365 | 2.5603 | | 4,089.284 1 | 4,089.284 1 | 1.1121 | | 4,112.637 4 |

3.2 Demolition - 2016

Unmitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|-----------------|-----|----------------|
| Category | | | | | lb/o | day | | | | | | | lb/d | lay | | |
| Hauling | 0.2954 | 3.0519 | 3.8938 | 8.9600e- 003 | 0.2151 | 0.0474 | 0.2625 | 0.0589 | 0.0436 | 0.1024 | | 900.0200 | 900.0200 | 6.2800e- 003 | | 900.1520 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Worker | 0.0601 | 0.0541 | 0.7239 | 1.4600e- 003 | 0.1141 | 8.4000e- 004 | 0.1149 | 0.0303 | 7.7000e- 004 | 0.0310 | | 119.9145 | 119.9145 | 5.7900e- 003 | | 120.0362 |
| Total | 0.3555 | 3.1060 | 4.6177 | 0.0104 | 0.3292 | 0.0483 | 0.3775 | 0.0891 | 0.0444 | 0.1335 | | 1,019.934 6 | 1,019.934 6 | 0.0121 | | 1,020.188 2 |

| | ROG | NOx | СО | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|---------------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|--------|-----|----------------|
| Category | | | | | lb/o | day | | | | | | | lb/c | lay | | |
| Fugitive Dust | | | | | 2.7989 | 0.0000 | 2.7989 | 0.4238 | 0.0000 | 0.4238 | | | 0.0000 | | | 0.0000 |
| Off-Road | 4.2876 | 45.6559 | 35.0303 | 0.0399 | | 2.2921 | 2.2921 | | 2.1365 | 2.1365 | 0.0000 | 4,089.284 1 | 4,089.284 1 | 1.1121 | | 4,112.637 4 |
| Total | 4.2876 | 45.6559 | 35.0303 | 0.0399 | 2.7989 | 2.2921 | 5.0910 | 0.4238 | 2.1365 | 2.5603 | 0.0000 | 4,089.284 1 | 4,089.284 1 | 1.1121 | | 4,112.637 4 |

3.2 Demolition - 2016

Mitigated Construction Off-Site

| | ROG | NOx | СО | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|-----------------|-----|----------------|
| Category | | | | | lb/ | day | | | | | | | lb/d | day | | |
| Hauling | 0.2954 | 3.0519 | 3.8938 | 8.9600e- 003 | 0.2151 | 0.0474 | 0.2625 | 0.0589 | 0.0436 | 0.1024 | | 900.0200 | 900.0200 | 6.2800e- 003 | | 900.1520 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Worker | 0.0601 | 0.0541 | 0.7239 | 1.4600e- 003 | 0.1141 | 8.4000e- 004 | 0.1149 | 0.0303 | 7.7000e- 004 | 0.0310 | | 119.9145 | 119.9145 | 5.7900e- 003 | | 120.0362 |
| Total | 0.3555 | 3.1060 | 4.6177 | 0.0104 | 0.3292 | 0.0483 | 0.3775 | 0.0891 | 0.0444 | 0.1335 | | 1,019.934 6 | 1,019.934 6 | 0.0121 | | 1,020.188 2 |

3.3 Site Preparation - 2016

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|---------------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|--------|-----|----------------|
| Category | | | | | lb/d | day | | | | | | | lb/c | lay | | |
| Fugitive Dust | | | | | 18.0663 | 0.0000 | 18.0663 | 9.9307 | 0.0000 | 9.9307 | | | 0.0000 | | | 0.0000 |
| Off-Road | 5.0771 | 54.6323 | 41.1053 | 0.0391 | | 2.9387 | 2.9387 | | 2.7036 | 2.7036 | | 4,065.005 3 | 4,065.005 3 | 1.2262 | | 4,090.754 4 |
| Total | 5.0771 | 54.6323 | 41.1053 | 0.0391 | 18.0663 | 2.9387 | 21.0049 | 9.9307 | 2.7036 | 12.6343 | | 4,065.005 3 | 4,065.005 3 | 1.2262 | | 4,090.754 4 |

3.3 Site Preparation - 2016

Unmitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|-----------------|-----|----------|
| Category | | | | | lb/o | day | | | | | | | lb/c | lay | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Worker | 0.0721 | 0.0649 | 0.8686 | 1.7500e- 003 | 0.1369 | 1.0100e- 003 | 0.1379 | 0.0363 | 9.2000e- 004 | 0.0373 | | 143.8975 | 143.8975 | 6.9500e- 003 | | 144.0434 |
| Total | 0.0721 | 0.0649 | 0.8686 | 1.7500e- 003 | 0.1369 | 1.0100e- 003 | 0.1379 | 0.0363 | 9.2000e- 004 | 0.0373 | | 143.8975 | 143.8975 | 6.9500e- 003 | | 144.0434 |

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|---------------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|--------|-----|----------------|
| Category | | | | | lb/d | day | | | | | | | lb/c | lay | | |
| Fugitive Dust | | | | | 18.0663 | 0.0000 | 18.0663 | 9.9307 | 0.0000 | 9.9307 | | | 0.0000 | | | 0.0000 |
| Off-Road | 5.0771 | 54.6323 | 41.1053 | 0.0391 | | 2.9387 | 2.9387 | | 2.7036 | 2.7036 | 0.0000 | 4,065.005 3 | 4,065.005 3 | 1.2262 | | 4,090.754 4 |
| Total | 5.0771 | 54.6323 | 41.1053 | 0.0391 | 18.0663 | 2.9387 | 21.0049 | 9.9307 | 2.7036 | 12.6343 | 0.0000 | 4,065.005 3 | 4,065.005 3 | 1.2262 | | 4,090.754 4 |

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3.3 Site Preparation - 2016

Mitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|----------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|-----------------|-----|----------|
| Category | | | <u>.</u> | | lb/ | day | | | | | | | lb/c | lay | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | , | 0.0000 |
| Worker | 0.0721 | 0.0649 | 0.8686 | 1.7500e- 003 | 0.1369 | 1.0100e- 003 | 0.1379 | 0.0363 | 9.2000e- 004 | 0.0373 | | 143.8975 | 143.8975 | 6.9500e- 003 | | 144.0434 |
| Total | 0.0721 | 0.0649 | 0.8686 | 1.7500e- 003 | 0.1369 | 1.0100e- 003 | 0.1379 | 0.0363 | 9.2000e- 004 | 0.0373 | | 143.8975 | 143.8975 | 6.9500e- 003 | | 144.0434 |

3.4 Grading - 2016

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|---------------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|--------|-----|----------------|
| Category | | | | | lb/o | day | | | | | | | lb/c | lay | | |
| Fugitive Dust | | | | | 6.2143 | 0.0000 | 6.2143 | 3.3310 | 0.0000 | 3.3310 | | | 0.0000 | | | 0.0000 |
| Off-Road | 3.6669 | 38.4466 | 26.0787 | 0.0298 | | 2.1984 | 2.1984 | | 2.0225 | 2.0225 | | 3,093.788 9 | 3,093.788 9 | 0.9332 | | 3,113.386 0 |
| Total | 3.6669 | 38.4466 | 26.0787 | 0.0298 | 6.2143 | 2.1984 | 8.4127 | 3.3310 | 2.0225 | 5.3535 | | 3,093.788 9 | 3,093.788 9 | 0.9332 | | 3,113.386 0 |

3.4 Grading - 2016

Unmitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|-----------------|-----|----------------|
| Category | | | | | lb/o | day | | | | | | | lb/c | day | | |
| Hauling | 0.2946 | 3.0435 | 3.8831 | 8.9400e- 003 | 0.2145 | 0.0473 | 0.2618 | 0.0587 | 0.0435 | 0.1022 | | 897.5474 | 897.5474 | 6.2700e- 003 | | 897.6790 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Worker | 0.0601 | 0.0541 | 0.7239 | 1.4600e- 003 | 0.1141 | 8.4000e- 004 | 0.1149 | 0.0303 | 7.7000e- 004 | 0.0310 | | 119.9145 | 119.9145 | 5.7900e- 003 | | 120.0362 |
| Total | 0.3547 | 3.0976 | 4.6070 | 0.0104 | 0.3286 | 0.0481 | 0.3768 | 0.0890 | 0.0442 | 0.1332 | | 1,017.462 0 | 1,017.462 0 | 0.0121 | | 1,017.715 2 |

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|---------------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|--------|-----|----------------|
| Category | | | | | lb/d | day | | | | | | | lb/c | lay | | |
| Fugitive Dust | | | | | 6.2143 | 0.0000 | 6.2143 | 3.3310 | 0.0000 | 3.3310 | | | 0.0000 | | | 0.0000 |
| Off-Road | 3.6669 | 38.4466 | 26.0787 | 0.0298 | | 2.1984 | 2.1984 | | 2.0225 | 2.0225 | 0.0000 | 3,093.788 9 | 3,093.788 9 | 0.9332 | | 3,113.386 0 |
| Total | 3.6669 | 38.4466 | 26.0787 | 0.0298 | 6.2143 | 2.1984 | 8.4127 | 3.3310 | 2.0225 | 5.3535 | 0.0000 | 3,093.788 9 | 3,093.788 9 | 0.9332 | | 3,113.386 0 |

3.4 Grading - 2016

Mitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|-----------------|-----|----------------|
| Category | | | | | lb/ | day | | | | | | | lb/d | day | | |
| Hauling | 0.2946 | 3.0435 | 3.8831 | 8.9400e- 003 | 0.2145 | 0.0473 | 0.2618 | 0.0587 | 0.0435 | 0.1022 | | 897.5474 | 897.5474 | 6.2700e- 003 | | 897.6790 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Worker | 0.0601 | 0.0541 | 0.7239 | 1.4600e- 003 | 0.1141 | 8.4000e- 004 | 0.1149 | 0.0303 | 7.7000e- 004 | 0.0310 | | 119.9145 | 119.9145 | 5.7900e- 003 | | 120.0362 |
| Total | 0.3547 | 3.0976 | 4.6070 | 0.0104 | 0.3286 | 0.0481 | 0.3768 | 0.0890 | 0.0442 | 0.1332 | | 1,017.462 0 | 1,017.462 0 | 0.0121 | | 1,017.715 2 |

3.5 Paving - 2016

| | ROG | NOx | со | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|--------|-----|----------------|
| Category | | | | | lb/o | day | | | | | | | lb/c | lay | | |
| Off-Road | 1.7956 | 18.3417 | 12.5623 | 0.0186 | | 1.1065 | 1.1065 | | 1.0198 | 1.0198 | | 1,902.221 2 | 1,902.221 2 | 0.5588 | | 1,913.955 7 |
| Paving | 0.0000 | | | | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | | , | 0.0000 | | | 0.0000 |
| Total | 1.7956 | 18.3417 | 12.5623 | 0.0186 | | 1.1065 | 1.1065 | | 1.0198 | 1.0198 | | 1,902.221 2 | 1,902.221 2 | 0.5588 | | 1,913.955 7 |

3.5 Paving - 2016

Unmitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|-----------------|-----|----------|
| Category | | | | | lb/d | day | | | | | | | lb/c | day | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Worker | 0.0802 | 0.0721 | 0.9651 | 1.9500e- 003 | 0.1521 | 1.1200e- 003 | 0.1533 | 0.0404 | 1.0300e- 003 | 0.0414 | | 159.8861 | 159.8861 | 7.7200e- 003 | | 160.0483 |
| Total | 0.0802 | 0.0721 | 0.9651 | 1.9500e- 003 | 0.1521 | 1.1200e- 003 | 0.1533 | 0.0404 | 1.0300e- 003 | 0.0414 | | 159.8861 | 159.8861 | 7.7200e- 003 | | 160.0483 |

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|--------|-----|----------------|
| Category | | | | | lb/o | day | | | | | | | lb/c | day | | |
| Off-Road | 1.7956 | 18.3417 | 12.5623 | 0.0186 | | 1.1065 | 1.1065 | | 1.0198 | 1.0198 | 0.0000 | 1,902.221 2 | 1,902.221 2 | 0.5588 | | 1,913.955 7 |
| Paving | 0.0000 | | | | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | | | 0.0000 | | | 0.0000 |
| Total | 1.7956 | 18.3417 | 12.5623 | 0.0186 | | 1.1065 | 1.1065 | | 1.0198 | 1.0198 | 0.0000 | 1,902.221 2 | 1,902.221 2 | 0.5588 | | 1,913.955 7 |

3.5 Paving - 2016

Mitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|-----------------|-----|----------|
| Category | | | | | lb/e | day | | | | | | | lb/c | day | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Worker | 0.0802 | 0.0721 | 0.9651 | 1.9500e- 003 | 0.1521 | 1.1200e- 003 | 0.1533 | 0.0404 | 1.0300e- 003 | 0.0414 | | 159.8861 | 159.8861 | 7.7200e- 003 | | 160.0483 |
| Total | 0.0802 | 0.0721 | 0.9651 | 1.9500e- 003 | 0.1521 | 1.1200e- 003 | 0.1533 | 0.0404 | 1.0300e- 003 | 0.0414 | | 159.8861 | 159.8861 | 7.7200e- 003 | | 160.0483 |

3.6 Building Construction - 2016

| | ROG | NOx | СО | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|--------|-----|----------------|
| Category | | | | | lb/e | day | | | | | | | lb/c | lay | | |
| Off-Road | 3.4062 | 28.5063 | 18.5066 | 0.0268 | | 1.9674 | 1.9674 | | 1.8485 | 1.8485 | | 2,669.286 4 | 2,669.286 4 | 0.6620 | | 2,683.189 0 |
| Total | 3.4062 | 28.5063 | 18.5066 | 0.0268 | | 1.9674 | 1.9674 | | 1.8485 | 1.8485 | | 2,669.286 4 | 2,669.286 4 | 0.6620 | | 2,683.189 0 |

Unmitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|---------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|-----------------|-----|----------------|
| Category | | | | | lb/o | day | | | | | | | lb/d | day | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Vendor | 0.5558 | 3.6946 | 6.4823 | 9.6200e- 003 | 0.2702 | 0.0606 | 0.3308 | 0.0769 | 0.0556 | 0.1325 | | 960.4036 | 960.4036 | 7.5600e- 003 | | 960.5623 |
| Worker | 0.8576 | 0.7715 | 10.3270 | 0.0208 | 1.6279 | 0.0120 | 1.6399 | 0.4318 | 0.0110 | 0.4428 | | 1,710.780 8 | 1,710.780 8 | 0.0827 | | 1,712.516 4 |
| Total | 1.4134 | 4.4660 | 16.8093 | 0.0304 | 1.8981 | 0.0725 | 1.9706 | 0.5087 | 0.0666 | 0.5753 | | 2,671.184 4 | 2,671.184 4 | 0.0902 | | 2,673.078 6 |

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|--------|-----|----------------|
| Category | | | | | lb/e | day | | | | | | | lb/c | lay | | |
| Off-Road | 3.4062 | 28.5063 | 18.5066 | 0.0268 | | 1.9674 | 1.9674 | 1 1 1 | 1.8485 | 1.8485 | 0.0000 | 2,669.286 4 | 2,669.286 4 | 0.6620 | | 2,683.189 0 |
| Total | 3.4062 | 28.5063 | 18.5066 | 0.0268 | | 1.9674 | 1.9674 | | 1.8485 | 1.8485 | 0.0000 | 2,669.286 4 | 2,669.286 4 | 0.6620 | | 2,683.189 0 |

Mitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|---------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|-----------------|-----|----------------|
| Category | | | | | lb/o | day | | | | | | | lb/d | day | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Vendor | 0.5558 | 3.6946 | 6.4823 | 9.6200e- 003 | 0.2702 | 0.0606 | 0.3308 | 0.0769 | 0.0556 | 0.1325 | | 960.4036 | 960.4036 | 7.5600e- 003 | | 960.5623 |
| Worker | 0.8576 | 0.7715 | 10.3270 | 0.0208 | 1.6279 | 0.0120 | 1.6399 | 0.4318 | 0.0110 | 0.4428 | | 1,710.780 8 | 1,710.780 8 | 0.0827 | | 1,712.516 4 |
| Total | 1.4134 | 4.4660 | 16.8093 | 0.0304 | 1.8981 | 0.0725 | 1.9706 | 0.5087 | 0.0666 | 0.5753 | | 2,671.184 4 | 2,671.184 4 | 0.0902 | | 2,673.078 6 |

3.6 Building Construction - 2017

| | ROG | NOx | СО | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|--------|-----|----------------|
| Category | | | | | lb/d | day | | | | | | | lb/c | lay | | |
| Off-Road | 3.1024 | 26.4057 | 18.1291 | 0.0268 | | 1.7812 | 1.7812 | | 1.6730 | 1.6730 | | 2,639.805 3 | 2,639.805 3 | 0.6497 | | 2,653.449 0 |
| Total | 3.1024 | 26.4057 | 18.1291 | 0.0268 | | 1.7812 | 1.7812 | | 1.6730 | 1.6730 | | 2,639.805 3 | 2,639.805 3 | 0.6497 | | 2,653.449 0 |

Unmitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|---------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|-----------------|-----|----------------|
| Category | | | | | lb/o | day | | <u>.</u> | | | | | lb/c | day | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Vendor | 0.4793 | 3.2720 | 5.8049 | 9.6000e- 003 | 0.2703 | 0.0510 | 0.3213 | 0.0770 | 0.0469 | 0.1238 | | 944.2413 | 944.2413 | 7.0400e- 003 | | 944.3892 |
| Worker | 0.7647 | 0.6896 | 9.2450 | 0.0208 | 1.6279 | 0.0116 | 1.6395 | 0.4318 | 0.0107 | 0.4425 | | 1,643.304 1 | 1,643.304 1 | 0.0754 | | 1,644.887 4 |
| Total | 1.2439 | 3.9617 | 15.0499 | 0.0304 | 1.8982 | 0.0626 | 1.9608 | 0.5088 | 0.0575 | 0.5663 | | 2,587.545 4 | 2,587.545 4 | 0.0824 | | 2,589.276 6 |

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|--------|-----|----------------|
| Category | | | | | lb/e | day | | | | | | | lb/c | lay | | |
| Off-Road | 3.1024 | 26.4057 | 18.1291 | 0.0268 | | 1.7812 | 1.7812 | | 1.6730 | 1.6730 | 0.0000 | 2,639.805 3 | 2,639.805 3 | 0.6497 | | 2,653.449 0 |
| Total | 3.1024 | 26.4057 | 18.1291 | 0.0268 | | 1.7812 | 1.7812 | | 1.6730 | 1.6730 | 0.0000 | 2,639.805 3 | 2,639.805 3 | 0.6497 | | 2,653.449 0 |

Mitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|---------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|-----------------|-----|----------------|
| Category | | | | | lb/o | day | | | | | | | lb/c | day | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Vendor | 0.4793 | 3.2720 | 5.8049 | 9.6000e- 003 | 0.2703 | 0.0510 | 0.3213 | 0.0770 | 0.0469 | 0.1238 | | 944.2413 | 944.2413 | 7.0400e- 003 | | 944.3892 |
| Worker | 0.7647 | 0.6896 | 9.2450 | 0.0208 | 1.6279 | 0.0116 | 1.6395 | 0.4318 | 0.0107 | 0.4425 | | 1,643.304 1 | 1,643.304 1 | 0.0754 | | 1,644.887 4 |
| Total | 1.2439 | 3.9617 | 15.0499 | 0.0304 | 1.8982 | 0.0626 | 1.9608 | 0.5088 | 0.0575 | 0.5663 | | 2,587.545 4 | 2,587.545 4 | 0.0824 | | 2,589.276 6 |

3.6 Building Construction - 2018

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|--------|-----|----------------|
| Category | | | | | lb/d | day | | | | | | | lb/c | lay | | |
| Off-Road | 2.6687 | 23.2608 | 17.5327 | 0.0268 | | 1.4943 | 1.4943 | | 1.4048 | 1.4048 | | 2,609.939 0 | 2,609.939 0 | 0.6387 | | 2,623.351 7 |
| Total | 2.6687 | 23.2608 | 17.5327 | 0.0268 | | 1.4943 | 1.4943 | | 1.4048 | 1.4048 | | 2,609.939 0 | 2,609.939 0 | 0.6387 | | 2,623.351 7 |

Unmitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|---------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|-----------------|-----|----------------|
| Category | | | | | lb/d | day | | | | | | | lb/d | day | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Vendor | 0.3983 | 2.9494 | 5.0655 | 9.5600e- 003 | 0.2702 | 0.0469 | 0.3171 | 0.0769 | 0.0431 | 0.1200 | | 926.8135 | 926.8135 | 6.8700e- 003 | | 926.9577 |
| Worker | 0.6860 | 0.6213 | 8.3387 | 0.0208 | 1.6279 | 0.0113 | 1.6392 | 0.4318 | 0.0105 | 0.4423 | | 1,581.299 2 | 1,581.299 2 | 0.0694 | | 1,582.756 2 |
| Total | 1.0843 | 3.5708 | 13.4042 | 0.0304 | 1.8981 | 0.0582 | 1.9563 | 0.5087 | 0.0536 | 0.5623 | | 2,508.112 7 | 2,508.112 7 | 0.0763 | | 2,509.713 9 |

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|--------|-----|----------------|
| Category | | | | | lb/e | day | | | | | | | lb/c | lay | | |
| Off-Road | 2.6687 | 23.2608 | 17.5327 | 0.0268 | | 1.4943 | 1.4943 | 1 1 1 | 1.4048 | 1.4048 | 0.0000 | 2,609.938 9 | 2,609.938 9 | 0.6387 | | 2,623.351 7 |
| Total | 2.6687 | 23.2608 | 17.5327 | 0.0268 | | 1.4943 | 1.4943 | | 1.4048 | 1.4048 | 0.0000 | 2,609.938 9 | 2,609.938 9 | 0.6387 | | 2,623.351 7 |

Mitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|---------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|-----------------|-----|----------------|
| Category | | | | | lb/o | day | | | | | | | lb/c | day | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Vendor | 0.3983 | 2.9494 | 5.0655 | 9.5600e- 003 | 0.2702 | 0.0469 | 0.3171 | 0.0769 | 0.0431 | 0.1200 | | 926.8135 | 926.8135 | 6.8700e- 003 | | 926.9577 |
| Worker | 0.6860 | 0.6213 | 8.3387 | 0.0208 | 1.6279 | 0.0113 | 1.6392 | 0.4318 | 0.0105 | 0.4423 | | 1,581.299 2 | 1,581.299 2 | 0.0694 | | 1,582.756 2 |
| Total | 1.0843 | 3.5708 | 13.4042 | 0.0304 | 1.8981 | 0.0582 | 1.9563 | 0.5087 | 0.0536 | 0.5623 | | 2,508.112 7 | 2,508.112 7 | 0.0763 | | 2,509.713 9 |

3.7 Architectural Coating - 2016

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|-----------------|---------|--------|--------|-----------------|------------------|-----------------|---------------|-----------------------|------------------|----------------|----------|-----------|-----------|--------|-----|----------|
| Category | | | | | lb/d | day | | | | | | | lb/c | lay | | |
| Archit. Coating | 12.6516 | | | | | 0.0000 | 0.0000 | - - - - - | 0.0000 | 0.0000 | | | 0.0000 | | | 0.0000 |
| Off-Road | 0.3685 | 2.3722 | 1.8839 | 2.9700e- 003 | | 0.1966 | 0.1966 | | 0.1966 | 0.1966 | | 281.4481 | 281.4481 | 0.0332 | | 282.1449 |
| Total | 13.0201 | 2.3722 | 1.8839 | 2.9700e- 003 | | 0.1966 | 0.1966 | | 0.1966 | 0.1966 | | 281.4481 | 281.4481 | 0.0332 | | 282.1449 |

Unmitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|--------|-----|----------|
| Category | | | | | lb/o | day | | | | | | | lb/c | day | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Worker | 0.1723 | 0.1550 | 2.0751 | 4.1800e- 003 | 0.3271 | 2.4000e- 003 | 0.3295 | 0.0868 | 2.2100e- 003 | 0.0890 | | 343.7550 | 343.7550 | 0.0166 | | 344.1038 |
| Total | 0.1723 | 0.1550 | 2.0751 | 4.1800e- 003 | 0.3271 | 2.4000e- 003 | 0.3295 | 0.0868 | 2.2100e- 003 | 0.0890 | | 343.7550 | 343.7550 | 0.0166 | | 344.1038 |

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|-----------------|---------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|--------|-----|----------|
| Category | | | | | lb/e | day | | | | | | | lb/c | day | | |
| Archit. Coating | 12.6516 | | | | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | | | 0.0000 | | | 0.0000 |
| Off-Road | 0.3685 | 2.3722 | 1.8839 | 2.9700e- 003 | | 0.1966 | 0.1966 | | 0.1966 | 0.1966 | 0.0000 | 281.4481 | 281.4481 | 0.0332 | | 282.1449 |
| Total | 13.0201 | 2.3722 | 1.8839 | 2.9700e- 003 | | 0.1966 | 0.1966 | | 0.1966 | 0.1966 | 0.0000 | 281.4481 | 281.4481 | 0.0332 | | 282.1449 |

Mitigated Construction Off-Site

| | ROG | NOx | СО | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|--------|-----|----------|
| Category | | | | | lb/o | day | | | | | | | lb/d | day | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Worker | 0.1723 | 0.1550 | 2.0751 | 4.1800e- 003 | 0.3271 | 2.4000e- 003 | 0.3295 | 0.0868 | 2.2100e- 003 | 0.0890 | | 343.7550 | 343.7550 | 0.0166 | | 344.1038 |
| Total | 0.1723 | 0.1550 | 2.0751 | 4.1800e- 003 | 0.3271 | 2.4000e- 003 | 0.3295 | 0.0868 | 2.2100e- 003 | 0.0890 | | 343.7550 | 343.7550 | 0.0166 | | 344.1038 |

3.7 Architectural Coating - 2017

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|-----------------|---------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|--------|-----|----------|
| Category | | | | | lb/o | day | | | | | | | lb/c | lay | | |
| Archit. Coating | 12.6516 | | | | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | | | 0.0000 | | | 0.0000 |
| Off-Road | 0.3323 | 2.1850 | 1.8681 | 2.9700e- 003 | | 0.1733 | 0.1733 | | 0.1733 | 0.1733 | | 281.4481 | 281.4481 | 0.0297 | | 282.0721 |
| Total | 12.9839 | 2.1850 | 1.8681 | 2.9700e- 003 | | 0.1733 | 0.1733 | | 0.1733 | 0.1733 | | 281.4481 | 281.4481 | 0.0297 | | 282.0721 |

Unmitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|--------|-----|----------|
| Category | | | | | lb/e | day | | | | | | | lb/c | day | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Worker | 0.1537 | 0.1386 | 1.8576 | 4.1800e- 003 | 0.3271 | 2.3200e- 003 | 0.3294 | 0.0868 | 2.1400e- 003 | 0.0889 | | 330.1966 | 330.1966 | 0.0152 | | 330.5148 |
| Total | 0.1537 | 0.1386 | 1.8576 | 4.1800e- 003 | 0.3271 | 2.3200e- 003 | 0.3294 | 0.0868 | 2.1400e- 003 | 0.0889 | | 330.1966 | 330.1966 | 0.0152 | | 330.5148 |

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|-----------------|---------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|--------|-----|----------|
| Category | | | | | lb/e | day | | | | | | | lb/c | lay | | |
| Archit. Coating | 12.6516 | | | | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | | | 0.0000 | | | 0.0000 |
| Off-Road | 0.3323 | 2.1850 | 1.8681 | 2.9700e- 003 | | 0.1733 | 0.1733 | | 0.1733 | 0.1733 | 0.0000 | 281.4481 | 281.4481 | 0.0297 | | 282.0721 |
| Total | 12.9839 | 2.1850 | 1.8681 | 2.9700e- 003 | | 0.1733 | 0.1733 | | 0.1733 | 0.1733 | 0.0000 | 281.4481 | 281.4481 | 0.0297 | | 282.0721 |

Mitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|--------|-----|----------|
| Category | | | | | lb/o | day | | <u>.</u> | | | | | lb/c | lay | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Worker | 0.1537 | 0.1386 | 1.8576 | 4.1800e- 003 | 0.3271 | 2.3200e- 003 | 0.3294 | 0.0868 | 2.1400e- 003 | 0.0889 | | 330.1966 | 330.1966 | 0.0152 | | 330.5148 |
| Total | 0.1537 | 0.1386 | 1.8576 | 4.1800e- 003 | 0.3271 | 2.3200e- 003 | 0.3294 | 0.0868 | 2.1400e- 003 | 0.0889 | | 330.1966 | 330.1966 | 0.0152 | | 330.5148 |

3.7 Architectural Coating - 2018

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|-----------------|---------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|--------|-----|----------|
| Category | | | | | lb/d | day | | | | | | | lb/c | lay | | |
| Archit. Coating | 12.6516 | | | | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | | | 0.0000 | | | 0.0000 |
| Off-Road | 0.2986 | 2.0058 | 1.8542 | 2.9700e- 003 | | 0.1506 | 0.1506 | | 0.1506 | 0.1506 | | 281.4485 | 281.4485 | 0.0267 | | 282.0102 |
| Total | 12.9503 | 2.0058 | 1.8542 | 2.9700e- 003 | | 0.1506 | 0.1506 | | 0.1506 | 0.1506 | | 281.4485 | 281.4485 | 0.0267 | | 282.0102 |

Unmitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|--------|-----|----------|
| Category | | | | | lb/o | day | | | | | | | lb/d | day | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Worker | 0.1378 | 0.1249 | 1.6755 | 4.1800e- 003 | 0.3271 | 2.2800e- 003 | 0.3294 | 0.0868 | 2.1100e- 003 | 0.0889 | | 317.7377 | 317.7377 | 0.0139 | | 318.0304 |
| Total | 0.1378 | 0.1249 | 1.6755 | 4.1800e- 003 | 0.3271 | 2.2800e- 003 | 0.3294 | 0.0868 | 2.1100e- 003 | 0.0889 | | 317.7377 | 317.7377 | 0.0139 | | 318.0304 |

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|-----------------|---------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|--------|-----|----------|
| Category | | | | | lb/e | day | | | | | | | lb/c | lay | | |
| Archit. Coating | 12.6516 | | | | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | | | 0.0000 | | | 0.0000 |
| Off-Road | 0.2986 | 2.0058 | 1.8542 | 2.9700e- 003 | | 0.1506 | 0.1506 | | 0.1506 | 0.1506 | 0.0000 | 281.4485 | 281.4485 | 0.0267 | | 282.0102 |
| Total | 12.9503 | 2.0058 | 1.8542 | 2.9700e- 003 | | 0.1506 | 0.1506 | | 0.1506 | 0.1506 | 0.0000 | 281.4485 | 281.4485 | 0.0267 | | 282.0102 |

Mitigated Construction Off-Site

| | ROG | NOx | СО | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|--------|-----|----------|
| Category | | | | | lb/o | day | | | | | | | lb/c | day | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Worker | 0.1378 | 0.1249 | 1.6755 | 4.1800e- 003 | 0.3271 | 2.2800e- 003 | 0.3294 | 0.0868 | 2.1100e- 003 | 0.0889 | | 317.7377 | 317.7377 | 0.0139 | | 318.0304 |
| Total | 0.1378 | 0.1249 | 1.6755 | 4.1800e- 003 | 0.3271 | 2.2800e- 003 | 0.3294 | 0.0868 | 2.1100e- 003 | 0.0889 | | 317.7377 | 317.7377 | 0.0139 | | 318.0304 |

4.0 Operational Detail - Mobile

4.1 Mitigation Measures Mobile

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|-------------|--------|--------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|--------|-----|----------------|
| Category | | | - | | lb/o | day | | | | | | - | lb/c | lay | - | |
| Mitigated | 4.4477 | 7.9851 | 42.6133 | 0.0990 | 6.5850 | 0.1178 | 6.7027 | 1.7591 | 0.1085 | 1.8675 | | 8,018.471 8 | 8,018.471 8 | 0.3017 | | 8,024.807 5 |
| Unmitigated | 4.4477 | 7.9851 | 42.6133 | 0.0990 | 6.5850 | 0.1178 | 6.7027 | 1.7591 | 0.1085 | 1.8675 | | 8,018.471 8 | 8,018.471 8 | 0.3017 | | 8,024.807 5 |

4.2 Trip Summary Information

| | Avei | age Daily Trip Ra | ite | Unmitigated | Mitigated |
|----------------------------------|----------|-------------------|----------|-------------|------------|
| Land Use | Weekday | Saturday | Sunday | Annual VMT | Annual VMT |
| Apartments Mid Rise | 924.48 | 924.48 | 924.48 | 2,372,316 | 2,372,316 |
| Parking Lot | 0.00 | 0.00 | 0.00 | | |
| Regional Shopping Center | 168.66 | 168.66 | 168.66 | 235,669 | 235,669 |
| Single Family Housing | 195.60 | 195.60 | 195.60 | 501,931 | 501,931 |
| Unenclosed Parking with Elevator | 0.00 | 0.00 | 0.00 | | |
| Total | 1,288.74 | 1,288.74 | 1,288.74 | 3,109,917 | 3,109,917 |

4.3 Trip Type Information

| | | Miles | | | Trip % | | | Trip Purpos | se % |
|--------------------------|------------|------------|-------------|------------|------------|-------------|---------|-------------|---------|
| Land Use | H-W or C-W | H-S or C-C | H-O or C-NW | H-W or C-W | H-S or C-C | H-O or C-NW | Primary | Diverted | Pass-by |
| Apartments Mid Rise | 10.00 | 5.00 | 6.50 | 46.50 | 12.50 | 41.00 | 86 | 11 | 3 |
| Parking Lot | 10.00 | 5.00 | 6.50 | 0.00 | 0.00 | 0.00 | 0 | 0 | 0 |
| Regional Shopping Center | 10.00 | 5.00 | 6.50 | 16.30 | 64.70 | 19.00 | 54 | 35 | 11 |
| Single Family Housing | 10.00 | 5.00 | 6.50 | 46.50 | 12.50 | 41.00 | 86 | 11 | 3 |
| Unenclosed Parking with | 10.00 | 5.00 | 6.50 | 0.00 | 0.00 | 0.00 | 0 | 0 | 0 |

| LDA | LDT1 | LDT2 | MDV | LHD1 | LHD2 | MHD | HHD | OBUS | UBUS | MCY | SBUS | MH |
|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
| 0.504263 | 0.068212 | 0.178684 | 0.146863 | 0.044671 | 0.006294 | 0.020946 | 0.016568 | 0.002299 | 0.002275 | 0.006187 | 0.000564 | 0.002174 |

5.0 Energy Detail

Historical Energy Use: N

5.1 Mitigation Measures Energy

Exceed Title 24

| | ROG | NOx | со | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|---------------------------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|--------|--------|----------|
| Category | | | | | lb/c | lay | | | | | | | lb/c | day | | |
| NaturalGas Mitigated | 0.0690 | 0.5898 | 0.2540 | 3.7600e- 003 | | 0.0477 | 0.0477 | | 0.0477 | 0.0477 | | 752.4113 | 752.4113 | 0.0144 | 0.0138 | 756.9904 |
| NaturalGas Unmitigated | 0.0869 | 0.7430 | 0.3200 | 4.7400e- 003 | | 0.0600 | 0.0600 | | 0.0600 | 0.0600 | | 947.8553 | 947.8553 | 0.0182 | 0.0174 | 953.6238 |

5.2 Energy by Land Use - NaturalGas

<u>Unmitigated</u>

| | NaturalGa s Use | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|--|--------------------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|-----------------|----------|
| Land Use | kBTU/yr | | | | | lb/d | day | | | | | | | lb/d | day | | |
| Apartments Mid Rise | 5849.8 | 0.0631 | 0.5391 | 0.2294 | 3.4400e- 003 | | 0.0436 | 0.0436 | | 0.0436 | 0.0436 | | 688.2123 | 688.2123 | 0.0132 | 0.0126 | 692.4006 |
| Parking Lot | 0 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Regional Shopping Center | . 52.0707 | 1.0000e- 003 | 9.1100e- 003 | 7.6500e- 003 | 5.0000e- 005 | | 6.9000e- 004 | 6.9000e- 004 | | 6.9000e- 004 | 6.9000e- 004 | | 10.9267 | 10.9267 | 2.1000e- 004 | 2.0000e- 004 | 10.9932 |
| Single Family Housing | 2114.09 | 0.0228 | 0.1948 | 0.0829 | 1.2400e- 003 | | 0.0158 | 0.0158 | | 0.0158 | 0.0158 | | 248.7164 | 248.7164 | 4.7700e- 003 | 4.5600e- 003 | 250.2300 |
| Unenclosed Parking with Elevator | 0 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Total | | 0.0869 | 0.7430 | 0.3200 | 4.7300e- 003 | | 0.0600 | 0.0600 | | 0.0600 | 0.0600 | | 947.8553 | 947.8553 | 0.0182 | 0.0174 | 953.6238 |

5.2 Energy by Land Use - NaturalGas

Mitigated

| | NaturalGa s Use | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|-----------------------------|--------------------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|-----------------|----------|
| Land Use | kBTU/yr | | | | | lb/e | day | | | | | | | lb/c | lay | | |
| Apartments Mid Rise | 4.63891 | 0.0500 | 0.4275 | 0.1819 | 2.7300e- 003 | | 0.0346 | 0.0346 | | 0.0346 | 0.0346 | | 545.7540 | 545.7540 | 0.0105 | 0.0100 | 549.0753 |
| Parking Lot | 0 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Regional Shopping Center | 0.0734795 | 7.9000e- 004 | 7.2000e- 003 | 6.0500e- 003 | 4.0000e- 005 | | 5.5000e- 004 | 5.5000e- 004 | | 5.5000e- 004 | 5.5000e- 004 | | 8.6446 | 8.6446 | 1.7000e- 004 | 1.6000e- 004 | 8.6973 |
| Single Family Housing | 1.68311 | 0.0182 | 0.1551 | 0.0660 | 9.9000e- 004 | | 0.0125 | 0.0125 | | 0.0125 | 0.0125 | | 198.0127 | 198.0127 | 3.8000e- 003 | 3.6300e- 003 | 199.2178 |
| Unenclosed Parking with | 0 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Total | | 0.0690 | 0.5898 | 0.2540 | 3.7600e- 003 | | 0.0477 | 0.0477 | | 0.0477 | 0.0477 | | 752.4113 | 752.4113 | 0.0144 | 0.0138 | 756.9904 |

6.0 Area Detail

6.1 Mitigation Measures Area

Use only Natural Gas Hearths

Use Low VOC Cleaning Supplies

| | ROG | NOx | СО | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|-------------|--------|--------|---------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|--------|--------|---------|
| Category | | | | | lb/ | day | | | | | | | lb/d | day | | |
| Mitigated | 9.3337 | 0.2297 | 19.7928 | 1.0400e- 003 | | 0.1080 | 0.1080 | | 0.1080 | 0.1080 | 0.0000 | 35.3948 | 35.3948 | 0.0352 | 0.0000 | 36.1329 |
| Unmitigated | 9.9410 | 0.2297 | 19.7928 | 1.0400e- 003 | | 0.1080 | 0.1080 | - - - | 0.1080 | 0.1080 | 0.0000 | 35.3948 | 35.3948 | 0.0352 | 0.0000 | 36.1329 |

6.2 Area by SubCategory

<u>Unmitigated</u>

| | ROG | NOx | со | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|-------------|--------|--------|---------|-----------------|------------------|-----------------|---------------|-----------------------|------------------|----------------|----------|-----------|-----------|--------|--------|---------|
| SubCategory | | | | | lb/o | day | | | | | | | lb/d | lay | | |
| Coating | 1.2062 | | | | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | | | 0.0000 | | | 0.0000 |
| | 8.1234 | | | | | 0.0000 | 0.0000 | 1 1 1 1 1 | 0.0000 | 0.0000 | | | 0.0000 | | | 0.0000 |
| Hearth | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 1 1 1 1 1 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Landscaping | 0.6113 | 0.2297 | 19.7928 | 1.0400e- 003 | | 0.1080 | 0.1080 | | 0.1080 | 0.1080 | | 35.3948 | 35.3948 | 0.0352 | | 36.1329 |
| Total | 9.9410 | 0.2297 | 19.7928 | 1.0400e- 003 | | 0.1080 | 0.1080 | | 0.1080 | 0.1080 | 0.0000 | 35.3948 | 35.3948 | 0.0352 | 0.0000 | 36.1329 |

6.2 Area by SubCategory

Mitigated

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|--------------------------|--------|--------|---------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|--------|--------|---------|
| SubCategory | | | | | lb/ | day | | | | | | | lb/d | day | | |
| Architectural Coating | 1.2062 | | | | 1 1 1 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | | | 0.0000 | | | 0.0000 |
| Consumer Products | 7.5161 | | | | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | | | 0.0000 | | | 0.0000 |
| Hearth | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Landscaping | 0.6113 | 0.2297 | 19.7928 | 1.0400e- 003 | | 0.1080 | 0.1080 | | 0.1080 | 0.1080 | | 35.3948 | 35.3948 | 0.0352 | | 36.1329 |
| Total | 9.3337 | 0.2297 | 19.7928 | 1.0400e- 003 | | 0.1080 | 0.1080 | | 0.1080 | 0.1080 | 0.0000 | 35.3948 | 35.3948 | 0.0352 | 0.0000 | 36.1329 |

7.0 Water Detail

7.1 Mitigation Measures Water

8.0 Waste Detail

8.1 Mitigation Measures Waste

9.0 Operational Offroad

| - 1 | | | | | | | |
|-----|----------------|--------|-----------|-----------|-------------|-------------|-----------|
| | Equipment Type | Number | Hours/Day | Days/Year | Horse Power | Load Factor | Fuel Type |

10.0 Vegetation

Stockton & T

Sacramento County, Winter

1.0 Project Characteristics

1.1 Land Usage

| Land Uses | Size | Metric | Lot Acreage | Floor Surface Area | Population |
|----------------------------------|--------|---------------|-------------|--------------------|------------|
| Parking Lot | 96.00 | Space | 0.00 | 38,400.00 | 0 |
| Unenclosed Parking with Elevator | 78.00 | 1000sqft | 0.00 | 78,000.00 | 0 |
| Apartments Mid Rise | 214.00 | Dwelling Unit | 2.92 | 214,000.00 | 571 |
| Single Family Housing | 24.00 | Dwelling Unit | 2.00 | 43,200.00 | 64 |
| Regional Shopping Center | 6.00 | 1000sqft | 0.00 | 6,000.00 | 0 |

1.2 Other Project Characteristics

| Urbanization | Urban | Wind Speed (m/s) | 3.5 | Precipitation Freq (Days) | 58 |
|----------------------------|--------------------------|----------------------------|-------|----------------------------|-------|
| Climate Zone | 6 | | | Operational Year | 2018 |
| Utility Company | Sacramento Municipal Uti | lity District | | | |
| CO2 Intensity (Ib/MWhr) | 590.31 | CH4 Intensity (Ib/MWhr) | 0.029 | N2O Intensity (Ib/MWhr) | 0.006 |

1.3 User Entered Comments & Non-Default Data

Project Characteristics -

Land Use - based on project description

Construction Phase - based on info from applicant

Demolition -

Grading - based on info from applicant

Vehicle Trips - based on info from Transportation Impact Study

Area Mitigation -

Energy Mitigation -

| Table Name | Column Name | Default Value | New Value |
|---------------------------|------------------|---------------|-----------|
| tblConstructionPhase | NumDays | 18.00 | 348.00 |
| tblConstructionPhase | NumDays | 230.00 | 348.00 |
| tblConstructionPhase | NumDays | 20.00 | 44.00 |
| tblConstructionPhase | NumDays | 8.00 | 16.00 |
| tblConstructionPhase | NumDays | 18.00 | 11.00 |
| tblConstructionPhase | PhaseEndDate | 5/16/2019 | 1/29/2018 |
| tblConstructionPhase | PhaseStartDate | 1/16/2018 | 9/29/2016 |
| tblGrading | AcresOfGrading | 8.00 | 2.90 |
| tblGrading | MaterialImported | 0.00 | 2,000.00 |
| tblLandUse | LotAcreage | 0.86 | 0.00 |
| tblLandUse | LotAcreage | 1.79 | 0.00 |
| tblLandUse | LotAcreage | 5.63 | 2.92 |
| tblLandUse | LotAcreage | 7.79 | 2.00 |
| tblLandUse | LotAcreage | 0.14 | 0.00 |
| tblProjectCharacteristics | OperationalYear | 2014 | 2018 |
| tblVehicleTrips | ST_TR | 7.16 | 4.32 |
| tblVehicleTrips | ST_TR | 49.97 | 28.11 |
| tblVehicleTrips | ST_TR | 10.08 | 8.15 |
| tblVehicleTrips | SU_TR | 6.07 | 4.32 |
| tblVehicleTrips | SU_TR | 25.24 | 28.11 |
| tblVehicleTrips | SU_TR | 8.77 | 8.15 |
| tblVehicleTrips | WD_TR | 6.59 | 4.32 |
| tblVehicleTrips | WD_TR | 42.94 | 28.11 |
| tblVehicleTrips | WD_TR | 9.57 | 8.15 |
| | | | • |

2.0 Emissions Summary

2.1 Overall Construction (Maximum Daily Emission)

Unmitigated Construction

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|-------|---------|----------|----------|--------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------------|-----------------|--------|--------|-----------------|
| Year | | | | | lb/d | day | | | | | | | lb/d | day | | |
| 2016 | 18.0564 | 54.7128 | 41.8894 | 0.0613 | 18.2032 | 2.9397 | 21.1429 | 9.9670 | 2.7045 | 12.6715 | 0.0000 | 5,706.628 1 | 5,706.628 1 | 1.2331 | 0.0000 | 5,732.523 2 |
| 2017 | 17.5046 | 33.1227 | 38.7152 | 0.0613 | 2.2253 | 2.0202 | 4.2455 | 0.5955 | 1.9067 | 2.5022 | 0.0000 | 5,589.667 2 | 5,589.667 2 | 0.7772 | 0.0000 | 5,605.989 0 |
| 2018 | 16.8329 | 29.3484 | 36.3649 | 0.0612 | 2.2252 | 1.7060 | 3.9312 | 0.5955 | 1.6117 | 2.2072 | 0.0000 | 5,476.966 6 | 5,476.966 6 | 0.7559 | 0.0000 | 5,492.839 7 |
| Total | 52.3940 | 117.1839 | 116.9695 | 0.1838 | 22.6537 | 6.6659 | 29.3196 | 11.1580 | 6.2229 | 17.3809 | 0.0000 | 16,773.26 18 | 16,773.26 18 | 2.7662 | 0.0000 | 16,831.35 19 |

Mitigated Construction

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|-------|---------|----------|----------|--------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------------|-----------------|--------|--------|-----------------|
| Year | | | | | lb/d | day | | | | | | | lb/c | lay | | |
| 2016 | 18.0564 | 54.7128 | 41.8894 | 0.0613 | 18.2032 | 2.9397 | 21.1429 | 9.9670 | 2.7045 | 12.6715 | 0.0000 | 5,706.628 1 | 5,706.628 1 | 1.2331 | 0.0000 | 5,732.523 2 |
| 2017 | 17.5046 | 33.1227 | 38.7152 | 0.0613 | 2.2253 | 2.0202 | 4.2455 | 0.5955 | 1.9067 | 2.5022 | 0.0000 | 5,589.667 2 | 5,589.667 2 | 0.7772 | 0.0000 | 5,605.989 0 |
| 2018 | 16.8329 | 29.3484 | 36.3649 | 0.0612 | 2.2252 | 1.7060 | 3.9312 | 0.5955 | 1.6117 | 2.2072 | 0.0000 | 5,476.966 6 | 5,476.966 6 | 0.7559 | 0.0000 | 5,492.839 7 |
| Total | 52.3940 | 117.1839 | 116.9695 | 0.1838 | 22.6537 | 6.6659 | 29.3196 | 11.1580 | 6.2229 | 17.3809 | 0.0000 | 16,773.26 18 | 16,773.26 18 | 2.7662 | 0.0000 | 16,831.35 19 |

| | ROG | NOx | со | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio-CO2 | Total CO2 | CH4 | N20 | CO2e |
|----------------------|------|------|------|------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------|-----------|------|------|------|
| Percent Reduction | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

2.2 Overall Operational

Unmitigated Operational

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|---------|---------|---------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|--------|--------|----------------|
| Category | | | | | lb/o | day | | | | | | | lb/c | lay | | |
| Area | 9.9410 | 0.2297 | 19.7928 | 1.0400e- 003 | | 0.1080 | 0.1080 | | 0.1080 | 0.1080 | 0.0000 | 35.3948 | 35.3948 | 0.0352 | 0.0000 | 36.1329 |
| Energy | 0.0869 | 0.7430 | 0.3200 | 4.7400e- 003 | | 0.0600 | 0.0600 | | 0.0600 | 0.0600 | | 947.8553 | 947.8553 | 0.0182 | 0.0174 | 953.6238 |
| Mobile | 4.1197 | 9.0919 | 44.5722 | 0.0893 | 6.5850 | 0.1185 | 6.7035 | 1.7591 | 0.1092 | 1.8683 | | 7,263.001 6 | 7,263.001 6 | 0.3020 | | 7,269.342 6 |
| Total | 14.1476 | 10.0646 | 64.6849 | 0.0951 | 6.5850 | 0.2865 | 6.8715 | 1.7591 | 0.2772 | 2.0363 | 0.0000 | 8,246.251 8 | 8,246.251 8 | 0.3553 | 0.0174 | 8,259.099 3 |

Mitigated Operational

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|---------|--------|---------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|--------|--------|----------------|
| Category | | | | | lb/e | day | | | | | | | lb/c | lay | | |
| Area | 9.3337 | 0.2297 | 19.7928 | 1.0400e- 003 | | 0.1080 | 0.1080 | | 0.1080 | 0.1080 | 0.0000 | 35.3948 | 35.3948 | 0.0352 | 0.0000 | 36.1329 |
| Energy | 0.0690 | 0.5898 | 0.2540 | 3.7600e- 003 | | 0.0477 | 0.0477 | | 0.0477 | 0.0477 | | 752.4113 | 752.4113 | 0.0144 | 0.0138 | 756.9904 |
| Mobile | 4.1197 | 9.0919 | 44.5722 | 0.0893 | 6.5850 | 0.1185 | 6.7035 | 1.7591 | 0.1092 | 1.8683 | | 7,263.001 6 | 7,263.001 6 | 0.3020 | | 7,269.342 6 |
| Total | 13.5223 | 9.9114 | 64.6189 | 0.0941 | 6.5850 | 0.2742 | 6.8591 | 1.7591 | 0.2648 | 2.0239 | 0.0000 | 8,050.807 8 | 8,050.807 8 | 0.3515 | 0.0138 | 8,062.465 9 |

| | ROG | NOx | со | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio-CO2 | Total CO2 | CH4 | N20 | CO2e |
|----------------------|------|------|------|------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------|-----------|------|-------|------|
| Percent Reduction | 4.42 | 1.52 | 0.10 | 1.03 | 0.00 | 4.32 | 0.18 | 0.00 | 4.47 | 0.61 | 0.00 | 2.37 | 2.37 | 1.06 | 20.66 | 2.38 |

3.0 Construction Detail

Construction Phase

| Phase Number | Phase Name | Phase Type | Start Date | End Date | Num Days Week | Num Days | Phase Description |
|-----------------|-----------------------|-----------------------|------------|-----------|------------------|----------|-------------------|
| 1 | Demolition | Demolition | 6/1/2016 | 8/1/2016 | 5 | 44 | |
| 2 | Site Preparation | Site Preparation | 8/2/2016 | 8/8/2016 | 5 | 5 | |
| 3 | Grading | Grading | 8/9/2016 | 8/30/2016 | 5 | 16 | |
| 4 | Paving | Paving | 8/31/2016 | 9/14/2016 | 5 | 11 | |
| 5 | Building Construction | Building Construction | 9/15/2016 | 1/15/2018 | 5 | 348 | |
| 6 | Architectural Coating | Architectural Coating | 9/29/2016 | 1/29/2018 | 5 | 348 | |

Acres of Grading (Site Preparation Phase): 0

Acres of Grading (Grading Phase): 2.9

Acres of Paving: 0

Residential Indoor: 520,830; Residential Outdoor: 173,610; Non-Residential Indoor: 127,728; Non-Residential Outdoor: 42,576 (Architectural Coating – sqft)

OffRoad Equipment

| Phase Name | Offroad Equipment Type | Amount | Usage Hours | Horse Power | Load Factor |
|-----------------------|---------------------------|--------|-------------|-------------|-------------|
| Demolition | Concrete/Industrial Saws | 1 | 8.00 | 81 | 0.73 |
| Demolition | Excavators | 3 | 8.00 | 162 | 0.38 |
| Demolition | Rubber Tired Dozers | 2 | 8.00 | 255 | 0.40 |
| Site Preparation | Rubber Tired Dozers | 3 | 8.00 | 255 | 0.40 |
| Site Preparation | Tractors/Loaders/Backhoes | 4 | 8.00 | 97 | 0.37 |
| Grading | Excavators | 1 | 8.00 | 162 | 0.38 |
| Grading | Graders | 1 | 8.00 | 174 | 0.41 |
| Grading | Rubber Tired Dozers | 1 | 8.00 | 255 | 0.40 |
| Grading | Tractors/Loaders/Backhoes | 3 | 8.00 | 97 | 0.37 |
| Paving | Cement and Mortar Mixers | 2 | 6.00 | 9 | 0.56 |
| Paving | Pavers | 1 | 8.00 | 125 | 0.42 |
| Paving | Paving Equipment | 2 | 6.00 | 130 | 0.36 |
| Paving | Rollers | 2 | 6.00 | 80 | 0.38 |
| Paving | Tractors/Loaders/Backhoes | 1 | 8.00 | 97 | 0.37 |
| Building Construction | Cranes | 1 | 7.00 | 226 | 0.29 |
| Building Construction | Forklifts | 3 | 8.00 | 89 | 0.20 |
| Building Construction | Generator Sets | 1 | 8.00 | 84 | 0.74 |
| Building Construction | Tractors/Loaders/Backhoes | 3 | 7.00 | 97 | 0.37 |
| Building Construction | Welders | 1 | 8.00 | 46 | 0.45 |
| Architectural Coating | Air Compressors | 1 | 6.00 | 78 | 0.48 |

Trips and VMT

| Phase Name | Offroad Equipment Count | Worker Trip Number | Vendor Trip Number | Hauling Trip Number | Worker Trip Length | Vendor Trip Length | Hauling Trip Length | Worker Vehicle Class | Vendor Vehicle Class | Hauling Vehicle Class |
|-----------------------|----------------------------|-----------------------|-----------------------|------------------------|-----------------------|-----------------------|------------------------|-------------------------|-------------------------|--------------------------|
| Demolition | 6 | 15.00 | 0.00 | 546.00 | 10.00 | 6.50 | 20.00 | LD_Mix | HDT_Mix | HHDT |
| Site Preparation | 7 | 18.00 | 0.00 | 0.00 | 10.00 | 6.50 | 20.00 | LD_Mix | HDT_Mix | HHDT |
| Grading | 6 | 15.00 | 0.00 | 198.00 | 10.00 | 6.50 | 20.00 | LD_Mix | HDT_Mix | HHDT |
| Paving | 8 | 20.00 | 0.00 | 0.00 | 10.00 | 6.50 | 20.00 | LD_Mix | HDT_Mix | HHDT |
| Building Construction | 9 | 214.00 | 46.00 | 0.00 | 10.00 | 6.50 | 20.00 | LD_Mix | HDT_Mix | HHDT |
| Architectural Coating | 1 | 43.00 | 0.00 | 0.00 | 10.00 | 6.50 | 20.00 | LD_Mix | HDT_Mix | HHDT |

3.1 Mitigation Measures Construction

3.2 Demolition - 2016

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|---------------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|--------|-----|----------------|
| Category | | | | | lb/d | day | | | | | | | lb/c | day | | |
| Fugitive Dust | | | | | 2.7989 | 0.0000 | 2.7989 | 0.4238 | 0.0000 | 0.4238 | - | | 0.0000 | | | 0.0000 |
| Off-Road | 4.2876 | 45.6559 | 35.0303 | 0.0399 | | 2.2921 | 2.2921 | | 2.1365 | 2.1365 | | 4,089.284 1 | 4,089.284 1 | 1.1121 | | 4,112.637 4 |
| Total | 4.2876 | 45.6559 | 35.0303 | 0.0399 | 2.7989 | 2.2921 | 5.0910 | 0.4238 | 2.1365 | 2.5603 | | 4,089.284 1 | 4,089.284 1 | 1.1121 | | 4,112.637 4 |

3.2 Demolition - 2016

Unmitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|-----------------|-----|----------------|
| Category | | | | | lb/e | day | | | | | | | lb/d | day | | |
| Hauling | 0.3668 | 3.3239 | 5.0754 | 8.9600e- 003 | 0.2151 | 0.0476 | 0.2627 | 0.0589 | 0.0437 | 0.1026 | | 897.8296 | 897.8296 | 6.3700e- 003 | | 897.9634 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Worker | 0.0524 | 0.0671 | 0.6534 | 1.2800e- 003 | 0.1141 | 8.4000e- 004 | 0.1149 | 0.0303 | 7.7000e- 004 | 0.0310 | | 105.2835 | 105.2835 | 5.7900e- 003 | | 105.4052 |
| Total | 0.4192 | 3.3909 | 5.7288 | 0.0102 | 0.3292 | 0.0484 | 0.3776 | 0.0891 | 0.0445 | 0.1336 | | 1,003.113 1 | 1,003.113 1 | 0.0122 | | 1,003.368 6 |

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|---------------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|--------|-----|----------------|
| Category | | | | | lb/o | day | | | | | | | lb/c | lay | | |
| Fugitive Dust | | | | | 2.7989 | 0.0000 | 2.7989 | 0.4238 | 0.0000 | 0.4238 | | | 0.0000 | | | 0.0000 |
| Off-Road | 4.2876 | 45.6559 | 35.0303 | 0.0399 | | 2.2921 | 2.2921 | | 2.1365 | 2.1365 | 0.0000 | 4,089.284 1 | 4,089.284 1 | 1.1121 | | 4,112.637 4 |
| Total | 4.2876 | 45.6559 | 35.0303 | 0.0399 | 2.7989 | 2.2921 | 5.0910 | 0.4238 | 2.1365 | 2.5603 | 0.0000 | 4,089.284 1 | 4,089.284 1 | 1.1121 | | 4,112.637 4 |

3.2 Demolition - 2016

Mitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|-----------------|-----|----------------|
| Category | | | | | lb/o | day | | | | | | | lb/d | day | | |
| Hauling | 0.3668 | 3.3239 | 5.0754 | 8.9600e- 003 | 0.2151 | 0.0476 | 0.2627 | 0.0589 | 0.0437 | 0.1026 | | 897.8296 | 897.8296 | 6.3700e- 003 | | 897.9634 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Worker | 0.0524 | 0.0671 | 0.6534 | 1.2800e- 003 | 0.1141 | 8.4000e- 004 | 0.1149 | 0.0303 | 7.7000e- 004 | 0.0310 | | 105.2835 | 105.2835 | 5.7900e- 003 | | 105.4052 |
| Total | 0.4192 | 3.3909 | 5.7288 | 0.0102 | 0.3292 | 0.0484 | 0.3776 | 0.0891 | 0.0445 | 0.1336 | | 1,003.113 1 | 1,003.113 1 | 0.0122 | | 1,003.368 6 |

3.3 Site Preparation - 2016

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|---------------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|--------|-----|----------------|
| Category | | | | | lb/d | day | | | | | | | lb/c | lay | | |
| Fugitive Dust | | | | | 18.0663 | 0.0000 | 18.0663 | 9.9307 | 0.0000 | 9.9307 | | | 0.0000 | | | 0.0000 |
| Off-Road | 5.0771 | 54.6323 | 41.1053 | 0.0391 | | 2.9387 | 2.9387 | | 2.7036 | 2.7036 | | 4,065.005 3 | 4,065.005 3 | 1.2262 | | 4,090.754 4 |
| Total | 5.0771 | 54.6323 | 41.1053 | 0.0391 | 18.0663 | 2.9387 | 21.0049 | 9.9307 | 2.7036 | 12.6343 | | 4,065.005 3 | 4,065.005 3 | 1.2262 | | 4,090.754 4 |

3.3 Site Preparation - 2016

Unmitigated Construction Off-Site

| | ROG | NOx | СО | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|-----------------|-----|----------|
| Category | | | | | lb/o | day | | | | | | | lb/d | lay | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Worker | 0.0629 | 0.0805 | 0.7841 | 1.5400e- 003 | 0.1369 | 1.0100e- 003 | 0.1379 | 0.0363 | 9.2000e- 004 | 0.0373 | | 126.3402 | 126.3402 | 6.9500e- 003 | | 126.4862 |
| Total | 0.0629 | 0.0805 | 0.7841 | 1.5400e- 003 | 0.1369 | 1.0100e- 003 | 0.1379 | 0.0363 | 9.2000e- 004 | 0.0373 | | 126.3402 | 126.3402 | 6.9500e- 003 | | 126.4862 |

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|---------------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|--------|-----|----------------|
| Category | | | | | lb/d | day | | | | | | | lb/c | lay | | |
| Fugitive Dust | | | | | 18.0663 | 0.0000 | 18.0663 | 9.9307 | 0.0000 | 9.9307 | | | 0.0000 | | | 0.0000 |
| Off-Road | 5.0771 | 54.6323 | 41.1053 | 0.0391 | | 2.9387 | 2.9387 | | 2.7036 | 2.7036 | 0.0000 | 4,065.005 3 | 4,065.005 3 | 1.2262 | | 4,090.754 4 |
| Total | 5.0771 | 54.6323 | 41.1053 | 0.0391 | 18.0663 | 2.9387 | 21.0049 | 9.9307 | 2.7036 | 12.6343 | 0.0000 | 4,065.005 3 | 4,065.005 3 | 1.2262 | | 4,090.754 4 |

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3.3 Site Preparation - 2016

Mitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|-----------------|-----|----------|
| Category | | | | | lb/ | day | | | | | | | lb/d | day | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Worker | 0.0629 | 0.0805 | 0.7841 | 1.5400e- 003 | 0.1369 | 1.0100e- 003 | 0.1379 | 0.0363 | 9.2000e- 004 | 0.0373 | | 126.3402 | 126.3402 | 6.9500e- 003 | | 126.4862 |
| Total | 0.0629 | 0.0805 | 0.7841 | 1.5400e- 003 | 0.1369 | 1.0100e- 003 | 0.1379 | 0.0363 | 9.2000e- 004 | 0.0373 | | 126.3402 | 126.3402 | 6.9500e- 003 | | 126.4862 |

3.4 Grading - 2016

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|---------------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|--------|-----|----------------|
| Category | | | | | lb/o | day | | | | | | | lb/c | lay | | |
| Fugitive Dust | | | | | 6.2143 | 0.0000 | 6.2143 | 3.3310 | 0.0000 | 3.3310 | | | 0.0000 | | | 0.0000 |
| Off-Road | 3.6669 | 38.4466 | 26.0787 | 0.0298 | | 2.1984 | 2.1984 | | 2.0225 | 2.0225 | | 3,093.788 9 | 3,093.788 9 | 0.9332 | | 3,113.386 0 |
| Total | 3.6669 | 38.4466 | 26.0787 | 0.0298 | 6.2143 | 2.1984 | 8.4127 | 3.3310 | 2.0225 | 5.3535 | | 3,093.788 9 | 3,093.788 9 | 0.9332 | | 3,113.386 0 |

3.4 Grading - 2016

Unmitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|-----------------|-----|----------------|
| Category | | | | | lb/e | day | | | | | | | lb/c | day | | |
| Hauling | 0.3658 | 3.3147 | 5.0614 | 8.9400e- 003 | 0.2145 | 0.0475 | 0.2620 | 0.0587 | 0.0436 | 0.1023 | | 895.3630 | 895.3630 | 6.3600e- 003 | | 895.4965 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Worker | 0.0524 | 0.0671 | 0.6534 | 1.2800e- 003 | 0.1141 | 8.4000e- 004 | 0.1149 | 0.0303 | 7.7000e- 004 | 0.0310 | | 105.2835 | 105.2835 | 5.7900e- 003 | | 105.4052 |
| Total | 0.4182 | 3.3818 | 5.7148 | 0.0102 | 0.3286 | 0.0483 | 0.3769 | 0.0890 | 0.0444 | 0.1333 | | 1,000.646 6 | 1,000.646 6 | 0.0122 | | 1,000.901 7 |

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|---------------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|--------|-----|----------------|
| Category | | | | | lb/o | day | | | | | | | lb/c | lay | | |
| Fugitive Dust | | | | | 6.2143 | 0.0000 | 6.2143 | 3.3310 | 0.0000 | 3.3310 | | | 0.0000 | | | 0.0000 |
| Off-Road | 3.6669 | 38.4466 | 26.0787 | 0.0298 | | 2.1984 | 2.1984 | | 2.0225 | 2.0225 | 0.0000 | 3,093.788 9 | 3,093.788 9 | 0.9332 | | 3,113.386 0 |
| Total | 3.6669 | 38.4466 | 26.0787 | 0.0298 | 6.2143 | 2.1984 | 8.4127 | 3.3310 | 2.0225 | 5.3535 | 0.0000 | 3,093.788 9 | 3,093.788 9 | 0.9332 | | 3,113.386 0 |

3.4 Grading - 2016

Mitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|-----------------|-----|----------------|
| Category | | | | | lb/o | day | | | | | | | lb/d | day | | |
| Hauling | 0.3658 | 3.3147 | 5.0614 | 8.9400e- 003 | 0.2145 | 0.0475 | 0.2620 | 0.0587 | 0.0436 | 0.1023 | | 895.3630 | 895.3630 | 6.3600e- 003 | | 895.4965 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Worker | 0.0524 | 0.0671 | 0.6534 | 1.2800e- 003 | 0.1141 | 8.4000e- 004 | 0.1149 | 0.0303 | 7.7000e- 004 | 0.0310 | | 105.2835 | 105.2835 | 5.7900e- 003 | | 105.4052 |
| Total | 0.4182 | 3.3818 | 5.7148 | 0.0102 | 0.3286 | 0.0483 | 0.3769 | 0.0890 | 0.0444 | 0.1333 | | 1,000.646 6 | 1,000.646 6 | 0.0122 | | 1,000.901 7 |

3.5 Paving - 2016

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|--------|-----|----------------|
| Category | | | | | lb/o | day | | | | | | | lb/c | lay | | |
| | 1.7956 | 18.3417 | 12.5623 | 0.0186 | | 1.1065 | 1.1065 | | 1.0198 | 1.0198 | | 1,902.221 2 | 1,902.221 2 | 0.5588 | | 1,913.955 7 |
| Paving | 0.0000 | | | | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | | , | 0.0000 | | | 0.0000 |
| Total | 1.7956 | 18.3417 | 12.5623 | 0.0186 | | 1.1065 | 1.1065 | | 1.0198 | 1.0198 | | 1,902.221 2 | 1,902.221 2 | 0.5588 | | 1,913.955 7 |

3.5 Paving - 2016

Unmitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|-----------------|-----|----------|
| Category | | | | | lb/d | day | | | | | | | lb/c | lay | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Worker | 0.0699 | 0.0895 | 0.8712 | 1.7100e- 003 | 0.1521 | 1.1200e- 003 | 0.1533 | 0.0404 | 1.0300e- 003 | 0.0414 | | 140.3780 | 140.3780 | 7.7200e- 003 | | 140.5402 |
| Total | 0.0699 | 0.0895 | 0.8712 | 1.7100e- 003 | 0.1521 | 1.1200e- 003 | 0.1533 | 0.0404 | 1.0300e- 003 | 0.0414 | | 140.3780 | 140.3780 | 7.7200e- 003 | | 140.5402 |

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|--------|-----|----------------|
| Category | | | | | lb/o | day | | | | | | | lb/c | day | | |
| Off-Road | 1.7956 | 18.3417 | 12.5623 | 0.0186 | | 1.1065 | 1.1065 | | 1.0198 | 1.0198 | 0.0000 | 1,902.221 2 | 1,902.221 2 | 0.5588 | | 1,913.955 7 |
| Paving | 0.0000 | | | | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | | | 0.0000 | | | 0.0000 |
| Total | 1.7956 | 18.3417 | 12.5623 | 0.0186 | | 1.1065 | 1.1065 | | 1.0198 | 1.0198 | 0.0000 | 1,902.221 2 | 1,902.221 2 | 0.5588 | | 1,913.955 7 |

3.5 Paving - 2016

Mitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|-----------------|-----|----------|
| Category | | | | | lb/o | day | | <u>.</u> | | | | | lb/c | lay | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Worker | 0.0699 | 0.0895 | 0.8712 | 1.7100e- 003 | 0.1521 | 1.1200e- 003 | 0.1533 | 0.0404 | 1.0300e- 003 | 0.0414 | | 140.3780 | 140.3780 | 7.7200e- 003 | | 140.5402 |
| Total | 0.0699 | 0.0895 | 0.8712 | 1.7100e- 003 | 0.1521 | 1.1200e- 003 | 0.1533 | 0.0404 | 1.0300e- 003 | 0.0414 | | 140.3780 | 140.3780 | 7.7200e- 003 | | 140.5402 |

3.6 Building Construction - 2016

| | ROG | NOx | СО | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|--------|-----|----------------|
| Category | | | | | lb/e | day | | | | | | | lb/c | lay | | |
| Off-Road | 3.4062 | 28.5063 | 18.5066 | 0.0268 | | 1.9674 | 1.9674 | | 1.8485 | 1.8485 | | 2,669.286 4 | 2,669.286 4 | 0.6620 | | 2,683.189 0 |
| Total | 3.4062 | 28.5063 | 18.5066 | 0.0268 | | 1.9674 | 1.9674 | | 1.8485 | 1.8485 | | 2,669.286 4 | 2,669.286 4 | 0.6620 | | 2,683.189 0 |

Unmitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|---------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|-----------------|-----|----------------|
| Category | | | | | lb/o | day | | | | | | | lb/d | day | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Vendor | 0.7316 | 3.9611 | 9.4631 | 9.5900e- 003 | 0.2702 | 0.0615 | 0.3317 | 0.0769 | 0.0564 | 0.1334 | | 952.0359 | 952.0359 | 7.7800e- 003 | | 952.1994 |
| Worker | 0.7482 | 0.9572 | 9.3220 | 0.0183 | 1.6279 | 0.0120 | 1.6399 | 0.4318 | 0.0110 | 0.4428 | | 1,502.044 9 | 1,502.044 9 | 0.0827 | | 1,503.780 5 |
| Total | 1.4798 | 4.9184 | 18.7851 | 0.0279 | 1.8981 | 0.0734 | 1.9715 | 0.5087 | 0.0674 | 0.5762 | | 2,454.080 9 | 2,454.080 9 | 0.0904 | | 2,455.979 8 |

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|--------|-----|----------------|
| Category | | | | | lb/e | day | | | | | | | lb/c | lay | | |
| Off-Road | 3.4062 | 28.5063 | 18.5066 | 0.0268 | | 1.9674 | 1.9674 | 1 1 1 | 1.8485 | 1.8485 | 0.0000 | 2,669.286 4 | 2,669.286 4 | 0.6620 | | 2,683.189 0 |
| Total | 3.4062 | 28.5063 | 18.5066 | 0.0268 | | 1.9674 | 1.9674 | | 1.8485 | 1.8485 | 0.0000 | 2,669.286 4 | 2,669.286 4 | 0.6620 | | 2,683.189 0 |

Mitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|---------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|-----------------|-----|----------------|
| Category | | | | | lb/d | day | | | | | | | lb/c | day | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Vendor | 0.7316 | 3.9611 | 9.4631 | 9.5900e- 003 | 0.2702 | 0.0615 | 0.3317 | 0.0769 | 0.0564 | 0.1334 | | 952.0359 | 952.0359 | 7.7800e- 003 | | 952.1994 |
| Worker | 0.7482 | 0.9572 | 9.3220 | 0.0183 | 1.6279 | 0.0120 | 1.6399 | 0.4318 | 0.0110 | 0.4428 | | 1,502.044 9 | 1,502.044 9 | 0.0827 | | 1,503.780 5 |
| Total | 1.4798 | 4.9184 | 18.7851 | 0.0279 | 1.8981 | 0.0734 | 1.9715 | 0.5087 | 0.0674 | 0.5762 | | 2,454.080 9 | 2,454.080 9 | 0.0904 | | 2,455.979 8 |

3.6 Building Construction - 2017

| | ROG | NOx | СО | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|--------|-----|----------------|
| Category | | | | | lb/d | day | | | | | | | lb/c | lay | | |
| Off-Road | 3.1024 | 26.4057 | 18.1291 | 0.0268 | | 1.7812 | 1.7812 | | 1.6730 | 1.6730 | | 2,639.805 3 | 2,639.805 3 | 0.6497 | | 2,653.449 0 |
| Total | 3.1024 | 26.4057 | 18.1291 | 0.0268 | | 1.7812 | 1.7812 | | 1.6730 | 1.6730 | | 2,639.805 3 | 2,639.805 3 | 0.6497 | | 2,653.449 0 |

Unmitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|---------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|-----------------|-----|----------------|
| Category | | | | | lb/d | day | | | | | | | lb/d | day | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Vendor | 0.6250 | 3.5054 | 8.7737 | 9.5600e- 003 | 0.2703 | 0.0518 | 0.3221 | 0.0770 | 0.0476 | 0.1245 | | 935.9820 | 935.9820 | 7.2700e- 003 | | 936.1346 |
| Worker | 0.6606 | 0.8548 | 8.2805 | 0.0183 | 1.6279 | 0.0116 | 1.6395 | 0.4318 | 0.0107 | 0.4425 | | 1,442.569 7 | 1,442.569 7 | 0.0754 | | 1,444.153 0 |
| Total | 1.2856 | 4.3603 | 17.0542 | 0.0278 | 1.8982 | 0.0634 | 1.9615 | 0.5088 | 0.0582 | 0.5670 | | 2,378.551 7 | 2,378.551 7 | 0.0827 | | 2,380.287 6 |

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|--------|-----|----------------|
| Category | | | | | lb/e | day | | | | | | | lb/c | lay | | |
| Off-Road | 3.1024 | 26.4057 | 18.1291 | 0.0268 | | 1.7812 | 1.7812 | | 1.6730 | 1.6730 | 0.0000 | 2,639.805 3 | 2,639.805 3 | 0.6497 | | 2,653.449 0 |
| Total | 3.1024 | 26.4057 | 18.1291 | 0.0268 | | 1.7812 | 1.7812 | | 1.6730 | 1.6730 | 0.0000 | 2,639.805 3 | 2,639.805 3 | 0.6497 | | 2,653.449 0 |

Mitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|---------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|-----------------|-----|----------------|
| Category | | | | | lb/o | day | | | | | | | lb/c | lay | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Vendor | 0.6250 | 3.5054 | 8.7737 | 9.5600e- 003 | 0.2703 | 0.0518 | 0.3221 | 0.0770 | 0.0476 | 0.1245 | | 935.9820 | 935.9820 | 7.2700e- 003 | | 936.1346 |
| Worker | 0.6606 | 0.8548 | 8.2805 | 0.0183 | 1.6279 | 0.0116 | 1.6395 | 0.4318 | 0.0107 | 0.4425 | | 1,442.569 7 | 1,442.569 7 | 0.0754 | | 1,444.153 0 |
| Total | 1.2856 | 4.3603 | 17.0542 | 0.0278 | 1.8982 | 0.0634 | 1.9615 | 0.5088 | 0.0582 | 0.5670 | | 2,378.551 7 | 2,378.551 7 | 0.0827 | | 2,380.287 6 |

3.6 Building Construction - 2018

| | ROG | NOx | СО | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|--------|-----|----------------|
| Category | | | | | lb/o | day | | | | | | | lb/c | lay | | |
| Off-Road | 2.6687 | 23.2608 | 17.5327 | 0.0268 | | 1.4943 | 1.4943 | 1 1 1 | 1.4048 | 1.4048 | | 2,609.939 0 | 2,609.939 0 | 0.6387 | | 2,623.351 7 |
| Total | 2.6687 | 23.2608 | 17.5327 | 0.0268 | | 1.4943 | 1.4943 | | 1.4048 | 1.4048 | | 2,609.939 0 | 2,609.939 0 | 0.6387 | | 2,623.351 7 |

Unmitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|---------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|-----------------|-----|----------------|
| Category | | | | | lb/d | day | | | | | | | lb/d | day | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Vendor | 0.5091 | 3.1578 | 8.0808 | 9.5200e- 003 | 0.2702 | 0.0476 | 0.3178 | 0.0769 | 0.0437 | 0.1207 | | 918.6739 | 918.6739 | 7.1000e- 003 | | 918.8230 |
| Worker | 0.5869 | 0.7694 | 7.4086 | 0.0183 | 1.6279 | 0.0113 | 1.6392 | 0.4318 | 0.0105 | 0.4423 | | 1,388.006 6 | 1,388.006 6 | 0.0694 | | 1,389.463 6 |
| Total | 1.0961 | 3.9272 | 15.4894 | 0.0278 | 1.8981 | 0.0589 | 1.9570 | 0.5087 | 0.0542 | 0.5630 | | 2,306.680 6 | 2,306.680 6 | 0.0765 | | 2,308.286 6 |

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|---------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|--------|-----|----------------|
| Category | | | | | lb/e | day | | | | | | | lb/c | lay | | |
| Off-Road | 2.6687 | 23.2608 | 17.5327 | 0.0268 | | 1.4943 | 1.4943 | 1 1 1 | 1.4048 | 1.4048 | 0.0000 | 2,609.938 9 | 2,609.938 9 | 0.6387 | | 2,623.351 7 |
| Total | 2.6687 | 23.2608 | 17.5327 | 0.0268 | | 1.4943 | 1.4943 | | 1.4048 | 1.4048 | 0.0000 | 2,609.938 9 | 2,609.938 9 | 0.6387 | | 2,623.351 7 |

Mitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|---------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|-----------------|-----|----------------|
| Category | | | | | lb/o | day | | | | | | | lb/c | day | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Vendor | 0.5091 | 3.1578 | 8.0808 | 9.5200e- 003 | 0.2702 | 0.0476 | 0.3178 | 0.0769 | 0.0437 | 0.1207 | | 918.6739 | 918.6739 | 7.1000e- 003 | | 918.8230 |
| Worker | 0.5869 | 0.7694 | 7.4086 | 0.0183 | 1.6279 | 0.0113 | 1.6392 | 0.4318 | 0.0105 | 0.4423 | | 1,388.006 6 | 1,388.006 6 | 0.0694 | | 1,389.463 6 |
| Total | 1.0961 | 3.9272 | 15.4894 | 0.0278 | 1.8981 | 0.0589 | 1.9570 | 0.5087 | 0.0542 | 0.5630 | | 2,306.680 6 | 2,306.680 6 | 0.0765 | | 2,308.286 6 |

3.7 Architectural Coating - 2016

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|-----------------|---------|--------|--------|-----------------|------------------|-----------------|---------------|-----------------------|------------------|----------------|----------|-----------|-----------|--------|-----|----------|
| Category | | | | | lb/d | day | | | | | | | lb/c | day | | |
| Archit. Coating | 12.6516 | | | | | 0.0000 | 0.0000 | - - - - - | 0.0000 | 0.0000 | | | 0.0000 | | | 0.0000 |
| Off-Road | 0.3685 | 2.3722 | 1.8839 | 2.9700e- 003 | | 0.1966 | 0.1966 | | 0.1966 | 0.1966 | | 281.4481 | 281.4481 | 0.0332 | | 282.1449 |
| Total | 13.0201 | 2.3722 | 1.8839 | 2.9700e- 003 | | 0.1966 | 0.1966 | | 0.1966 | 0.1966 | | 281.4481 | 281.4481 | 0.0332 | | 282.1449 |

Unmitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|--------|-----|----------|
| Category | | | | | lb/o | day | | | | | | | lb/c | day | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Worker | 0.1503 | 0.1923 | 1.8731 | 3.6700e- 003 | 0.3271 | 2.4000e- 003 | 0.3295 | 0.0868 | 2.2100e- 003 | 0.0890 | | 301.8128 | 301.8128 | 0.0166 | | 302.1615 |
| Total | 0.1503 | 0.1923 | 1.8731 | 3.6700e- 003 | 0.3271 | 2.4000e- 003 | 0.3295 | 0.0868 | 2.2100e- 003 | 0.0890 | | 301.8128 | 301.8128 | 0.0166 | | 302.1615 |

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|-----------------|---------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|--------|-----|----------|
| Category | | | | | lb/e | day | | | | | | | lb/c | day | | |
| Archit. Coating | 12.6516 | | | | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | | | 0.0000 | | | 0.0000 |
| Off-Road | 0.3685 | 2.3722 | 1.8839 | 2.9700e- 003 | | 0.1966 | 0.1966 | | 0.1966 | 0.1966 | 0.0000 | 281.4481 | 281.4481 | 0.0332 | | 282.1449 |
| Total | 13.0201 | 2.3722 | 1.8839 | 2.9700e- 003 | | 0.1966 | 0.1966 | | 0.1966 | 0.1966 | 0.0000 | 281.4481 | 281.4481 | 0.0332 | | 282.1449 |

Mitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|--------|-----|----------|
| Category | | | | | lb/o | day | | | | | | | lb/d | day | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Worker | 0.1503 | 0.1923 | 1.8731 | 3.6700e- 003 | 0.3271 | 2.4000e- 003 | 0.3295 | 0.0868 | 2.2100e- 003 | 0.0890 | | 301.8128 | 301.8128 | 0.0166 | | 302.1615 |
| Total | 0.1503 | 0.1923 | 1.8731 | 3.6700e- 003 | 0.3271 | 2.4000e- 003 | 0.3295 | 0.0868 | 2.2100e- 003 | 0.0890 | | 301.8128 | 301.8128 | 0.0166 | | 302.1615 |

3.7 Architectural Coating - 2017

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|-----------------|---------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|--------|-----|----------|
| Category | | | | | lb/d | day | | | | | | | lb/c | day | | |
| Archit. Coating | 12.6516 | | | | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | | | 0.0000 | | | 0.0000 |
| Off-Road | 0.3323 | 2.1850 | 1.8681 | 2.9700e- 003 | | 0.1733 | 0.1733 | | 0.1733 | 0.1733 | | 281.4481 | 281.4481 | 0.0297 | | 282.0721 |
| Total | 12.9839 | 2.1850 | 1.8681 | 2.9700e- 003 | | 0.1733 | 0.1733 | | 0.1733 | 0.1733 | | 281.4481 | 281.4481 | 0.0297 | | 282.0721 |

Unmitigated Construction Off-Site

| | ROG | NOx | СО | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|--------|-----|----------|
| Category | | | | | lb/o | day | | | | | | | lb/c | day | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Worker | 0.1327 | 0.1718 | 1.6638 | 3.6700e- 003 | 0.3271 | 2.3200e- 003 | 0.3294 | 0.0868 | 2.1400e- 003 | 0.0889 | | 289.8621 | 289.8621 | 0.0152 | | 290.1803 |
| Total | 0.1327 | 0.1718 | 1.6638 | 3.6700e- 003 | 0.3271 | 2.3200e- 003 | 0.3294 | 0.0868 | 2.1400e- 003 | 0.0889 | | 289.8621 | 289.8621 | 0.0152 | | 290.1803 |

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|-----------------|---------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|--------|-----|----------|
| Category | | | | | lb/e | day | | | | | | | lb/c | day | | |
| Archit. Coating | 12.6516 | | | | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | | | 0.0000 | | | 0.0000 |
| Off-Road | 0.3323 | 2.1850 | 1.8681 | 2.9700e- 003 | | 0.1733 | 0.1733 | | 0.1733 | 0.1733 | 0.0000 | 281.4481 | 281.4481 | 0.0297 | | 282.0721 |
| Total | 12.9839 | 2.1850 | 1.8681 | 2.9700e- 003 | | 0.1733 | 0.1733 | | 0.1733 | 0.1733 | 0.0000 | 281.4481 | 281.4481 | 0.0297 | | 282.0721 |

Mitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|--------|-----|----------|
| Category | | | | | lb/o | day | | | | | | | lb/c | day | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Worker | 0.1327 | 0.1718 | 1.6638 | 3.6700e- 003 | 0.3271 | 2.3200e- 003 | 0.3294 | 0.0868 | 2.1400e- 003 | 0.0889 | | 289.8621 | 289.8621 | 0.0152 | | 290.1803 |
| Total | 0.1327 | 0.1718 | 1.6638 | 3.6700e- 003 | 0.3271 | 2.3200e- 003 | 0.3294 | 0.0868 | 2.1400e- 003 | 0.0889 | | 289.8621 | 289.8621 | 0.0152 | | 290.1803 |

3.7 Architectural Coating - 2018

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|-----------------|---------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|--------|-----|----------|
| Category | | | | | lb/d | day | | | | | | | lb/c | lay | | |
| Archit. Coating | 12.6516 | | | | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | | | 0.0000 | | | 0.0000 |
| Off-Road | 0.2986 | 2.0058 | 1.8542 | 2.9700e- 003 | | 0.1506 | 0.1506 | | 0.1506 | 0.1506 | | 281.4485 | 281.4485 | 0.0267 | | 282.0102 |
| Total | 12.9503 | 2.0058 | 1.8542 | 2.9700e- 003 | | 0.1506 | 0.1506 | | 0.1506 | 0.1506 | | 281.4485 | 281.4485 | 0.0267 | | 282.0102 |

Unmitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|--------|-----|----------|
| Category | | | | | lb/o | day | | | | | | | lb/d | lay | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Worker | 0.1179 | 0.1546 | 1.4886 | 3.6700e- 003 | 0.3271 | 2.2800e- 003 | 0.3294 | 0.0868 | 2.1100e- 003 | 0.0889 | | 278.8985 | 278.8985 | 0.0139 | | 279.1913 |
| Total | 0.1179 | 0.1546 | 1.4886 | 3.6700e- 003 | 0.3271 | 2.2800e- 003 | 0.3294 | 0.0868 | 2.1100e- 003 | 0.0889 | | 278.8985 | 278.8985 | 0.0139 | | 279.1913 |

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|---------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|--------|-----|----------|
| Category | | | | | lb/e | day | | | | | | | lb/c | day | | |
| J J | 12.6516 | | | | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | | | 0.0000 | | | 0.0000 |
| Off-Road | 0.2986 | 2.0058 | 1.8542 | 2.9700e- 003 | | 0.1506 | 0.1506 | | 0.1506 | 0.1506 | 0.0000 | 281.4485 | 281.4485 | 0.0267 | | 282.0102 |
| Total | 12.9503 | 2.0058 | 1.8542 | 2.9700e- 003 | | 0.1506 | 0.1506 | | 0.1506 | 0.1506 | 0.0000 | 281.4485 | 281.4485 | 0.0267 | | 282.0102 |

Mitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|--------|-----|----------|
| Category | | | | | lb/ | day | | | | | | | lb/c | day | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | | 0.0000 |
| Worker | 0.1179 | 0.1546 | 1.4886 | 3.6700e- 003 | 0.3271 | 2.2800e- 003 | 0.3294 | 0.0868 | 2.1100e- 003 | 0.0889 | | 278.8985 | 278.8985 | 0.0139 | | 279.1913 |
| Total | 0.1179 | 0.1546 | 1.4886 | 3.6700e- 003 | 0.3271 | 2.2800e- 003 | 0.3294 | 0.0868 | 2.1100e- 003 | 0.0889 | | 278.8985 | 278.8985 | 0.0139 | | 279.1913 |

4.0 Operational Detail - Mobile

4.1 Mitigation Measures Mobile

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|-------------|--------|--------|---------|--------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|--------|-----|----------------|
| Category | | | | | lb/o | day | | | | | | | lb/c | lay | | |
| Mitigated | 4.1197 | 9.0919 | 44.5722 | 0.0893 | 6.5850 | 0.1185 | 6.7035 | 1.7591 | 0.1092 | 1.8683 | | 7,263.001 6 | 7,263.001 6 | 0.3020 | | 7,269.342 6 |
| Unmitigated | 4.1197 | 9.0919 | 44.5722 | 0.0893 | 6.5850 | 0.1185 | 6.7035 | 1.7591 | 0.1092 | 1.8683 | | 7,263.001 6 | 7,263.001 6 | 0.3020 | | 7,269.342 6 |

4.2 Trip Summary Information

| | Avei | age Daily Trip Ra | ite | Unmitigated | Mitigated |
|----------------------------------|----------|-------------------|----------|-------------|------------|
| Land Use | Weekday | Saturday | Sunday | Annual VMT | Annual VMT |
| Apartments Mid Rise | 924.48 | 924.48 | 924.48 | 2,372,316 | 2,372,316 |
| Parking Lot | 0.00 | 0.00 | 0.00 | | |
| Regional Shopping Center | 168.66 | 168.66 | 168.66 | 235,669 | 235,669 |
| Single Family Housing | 195.60 | 195.60 | 195.60 | 501,931 | 501,931 |
| Unenclosed Parking with Elevator | 0.00 | 0.00 | 0.00 | | |
| Total | 1,288.74 | 1,288.74 | 1,288.74 | 3,109,917 | 3,109,917 |

4.3 Trip Type Information

| | | Miles | | | Trip % | | | Trip Purpos | е% |
|--------------------------|------------|------------|-------------|------------|------------|-------------|---------|-------------|---------|
| Land Use | H-W or C-W | H-S or C-C | H-O or C-NW | H-W or C-W | H-S or C-C | H-O or C-NW | Primary | Diverted | Pass-by |
| Apartments Mid Rise | 10.00 | 5.00 | 6.50 | 46.50 | 12.50 | 41.00 | 86 | 11 | 3 |
| Parking Lot | 10.00 | 5.00 | 6.50 | 0.00 | 0.00 | 0.00 | 0 | 0 | 0 |
| Regional Shopping Center | 10.00 | 5.00 | 6.50 | 16.30 | 64.70 | 19.00 | 54 | 35 | 11 |
| Single Family Housing | 10.00 | 5.00 | 6.50 | 46.50 | 12.50 | 41.00 | 86 | 11 | 3 |
| Unenclosed Parking with | 10.00 | 5.00 | 6.50 | 0.00 | 0.00 | 0.00 | 0 | 0 | 0 |

| LDA | LDT1 | LDT2 | MDV | LHD1 | LHD2 | MHD | HHD | OBUS | UBUS | MCY | SBUS | MH |
|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
| 0.504263 | 0.068212 | 0.178684 | 0.146863 | 0.044671 | 0.006294 | 0.020946 | 0.016568 | 0.002299 | 0.002275 | 0.006187 | 0.000564 | 0.002174 |

5.0 Energy Detail

Historical Energy Use: N

5.1 Mitigation Measures Energy

Exceed Title 24

| | ROG | NOx | со | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|---------------------------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|--------|--------|----------|
| Category | | | | | lb/c | lay | | | | | | | lb/c | day | | |
| NaturalGas Mitigated | 0.0690 | 0.5898 | 0.2540 | 3.7600e- 003 | | 0.0477 | 0.0477 | | 0.0477 | 0.0477 | | 752.4113 | 752.4113 | 0.0144 | 0.0138 | 756.9904 |
| NaturalGas Unmitigated | 0.0869 | 0.7430 | 0.3200 | 4.7400e- 003 | | 0.0600 | 0.0600 | | 0.0600 | 0.0600 | | 947.8553 | 947.8553 | 0.0182 | 0.0174 | 953.6238 |

5.2 Energy by Land Use - NaturalGas

<u>Unmitigated</u>

| | NaturalGa s Use | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|--|--------------------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|-----------------|----------|
| Land Use | kBTU/yr | | | | | lb/d | day | | | | | | | lb/d | day | | |
| Apartments Mid Rise | 5849.8 | 0.0631 | 0.5391 | 0.2294 | 3.4400e- 003 | | 0.0436 | 0.0436 | | 0.0436 | 0.0436 | | 688.2123 | 688.2123 | 0.0132 | 0.0126 | 692.4006 |
| Parking Lot | 0 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Regional Shopping Center | . 52.0707 | 1.0000e- 003 | 9.1100e- 003 | 7.6500e- 003 | 5.0000e- 005 | | 6.9000e- 004 | 6.9000e- 004 | | 6.9000e- 004 | 6.9000e- 004 | | 10.9267 | 10.9267 | 2.1000e- 004 | 2.0000e- 004 | 10.9932 |
| Single Family Housing | 2114.09 | 0.0228 | 0.1948 | 0.0829 | 1.2400e- 003 | | 0.0158 | 0.0158 | | 0.0158 | 0.0158 | | 248.7164 | 248.7164 | 4.7700e- 003 | 4.5600e- 003 | 250.2300 |
| Unenclosed Parking with Elevator | 0 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Total | | 0.0869 | 0.7430 | 0.3200 | 4.7300e- 003 | | 0.0600 | 0.0600 | | 0.0600 | 0.0600 | | 947.8553 | 947.8553 | 0.0182 | 0.0174 | 953.6238 |

5.2 Energy by Land Use - NaturalGas

Mitigated

| | NaturalGa s Use | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|-----------------------------|--------------------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|-----------------|----------|
| Land Use | kBTU/yr | | | | | lb/e | day | | | | | | | lb/c | lay | | |
| Apartments Mid Rise | 4.63891 | 0.0500 | 0.4275 | 0.1819 | 2.7300e- 003 | | 0.0346 | 0.0346 | | 0.0346 | 0.0346 | | 545.7540 | 545.7540 | 0.0105 | 0.0100 | 549.0753 |
| Parking Lot | 0 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Regional Shopping Center | 0.0734795 | 7.9000e- 004 | 7.2000e- 003 | 6.0500e- 003 | 4.0000e- 005 | | 5.5000e- 004 | 5.5000e- 004 | | 5.5000e- 004 | 5.5000e- 004 | | 8.6446 | 8.6446 | 1.7000e- 004 | 1.6000e- 004 | 8.6973 |
| Single Family Housing | 1.68311 | 0.0182 | 0.1551 | 0.0660 | 9.9000e- 004 | | 0.0125 | 0.0125 | | 0.0125 | 0.0125 | | 198.0127 | 198.0127 | 3.8000e- 003 | 3.6300e- 003 | 199.2178 |
| Unenclosed Parking with | 0 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Total | | 0.0690 | 0.5898 | 0.2540 | 3.7600e- 003 | | 0.0477 | 0.0477 | | 0.0477 | 0.0477 | | 752.4113 | 752.4113 | 0.0144 | 0.0138 | 756.9904 |

6.0 Area Detail

6.1 Mitigation Measures Area

Use only Natural Gas Hearths

Use Low VOC Cleaning Supplies

| | ROG | NOx | со | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|-------------|--------|--------|---------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|--------|--------|---------|
| Category | | | | | lb/e | day | | | | | | | lb/d | day | | |
| Mitigated | 9.3337 | 0.2297 | 19.7928 | 1.0400e- 003 | | 0.1080 | 0.1080 | | 0.1080 | 0.1080 | 0.0000 | 35.3948 | 35.3948 | 0.0352 | 0.0000 | 36.1329 |
| Unmitigated | 9.9410 | 0.2297 | 19.7928 | 1.0400e- 003 | | 0.1080 | 0.1080 | | 0.1080 | 0.1080 | 0.0000 | 35.3948 | 35.3948 | 0.0352 | 0.0000 | 36.1329 |

6.2 Area by SubCategory

<u>Unmitigated</u>

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|--------------------------|--------|--------|---------|-----------------|------------------|-----------------|---------------|-----------------------|------------------|----------------|----------|-----------|-----------|--------|--------|---------|
| SubCategory | | | | | lb/ | day | | | | | | | lb/d | day | | |
| Architectural Coating | 1.2062 | | | | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | | | 0.0000 | | | 0.0000 |
| Consumer Products | 8.1234 | | , | | | 0.0000 | 0.0000 | 1 1 1 1 1 | 0.0000 | 0.0000 | | | 0.0000 | | , | 0.0000 |
| Hearth | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Landscaping | 0.6113 | 0.2297 | 19.7928 | 1.0400e- 003 | | 0.1080 | 0.1080 | 1 1 1 1 1 | 0.1080 | 0.1080 | | 35.3948 | 35.3948 | 0.0352 | 1 | 36.1329 |
| Total | 9.9410 | 0.2297 | 19.7928 | 1.0400e- 003 | | 0.1080 | 0.1080 | | 0.1080 | 0.1080 | 0.0000 | 35.3948 | 35.3948 | 0.0352 | 0.0000 | 36.1329 |

6.2 Area by SubCategory

Mitigated

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|--------------------------|--------|--------|---------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|--------|--------|---------|
| SubCategory | | | | | lb/ | day | | | | | | | lb/d | day | | |
| Architectural Coating | 1.2062 | | | | 1 1 1 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | | | 0.0000 | | | 0.0000 |
| Consumer Products | 7.5161 | | | | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | | | 0.0000 | | | 0.0000 |
| Hearth | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Landscaping | 0.6113 | 0.2297 | 19.7928 | 1.0400e- 003 | | 0.1080 | 0.1080 | | 0.1080 | 0.1080 | | 35.3948 | 35.3948 | 0.0352 | | 36.1329 |
| Total | 9.3337 | 0.2297 | 19.7928 | 1.0400e- 003 | | 0.1080 | 0.1080 | | 0.1080 | 0.1080 | 0.0000 | 35.3948 | 35.3948 | 0.0352 | 0.0000 | 36.1329 |

7.0 Water Detail

7.1 Mitigation Measures Water

8.0 Waste Detail

8.1 Mitigation Measures Waste

9.0 Operational Offroad

| - 1 | | | | | | | |
|-----|----------------|--------|-----------|-----------|-------------|-------------|-----------|
| | Equipment Type | Number | Hours/Day | Days/Year | Horse Power | Load Factor | Fuel Type |

10.0 Vegetation

Stockton & T

Sacramento County, Annual

1.0 Project Characteristics

1.1 Land Usage

| Land Uses | Size | Metric | Lot Acreage | Floor Surface Area | Population |
|----------------------------------|--------|---------------|-------------|--------------------|------------|
| Parking Lot | 96.00 | Space | 0.00 | 38,400.00 | 0 |
| Unenclosed Parking with Elevator | 78.00 | 1000sqft | 0.00 | 78,000.00 | 0 |
| Apartments Mid Rise | 214.00 | Dwelling Unit | 2.92 | 214,000.00 | 571 |
| Single Family Housing | 24.00 | Dwelling Unit | 2.00 | 43,200.00 | 64 |
| Regional Shopping Center | 6.00 | 1000sqft | 0.00 | 6,000.00 | 0 |

1.2 Other Project Characteristics

| Urbanization | Urban | Wind Speed (m/s) | 3.5 | Precipitation Freq (Days) | 58 |
|----------------------------|--------------------------|----------------------------|-------|----------------------------|-------|
| Climate Zone | 6 | | | Operational Year | 2018 |
| Utility Company | Sacramento Municipal Uti | lity District | | | |
| CO2 Intensity (Ib/MWhr) | 590.31 | CH4 Intensity (Ib/MWhr) | 0.029 | N2O Intensity (Ib/MWhr) | 0.006 |

1.3 User Entered Comments & Non-Default Data

Project Characteristics -

Land Use - based on project description

Construction Phase - based on info from applicant

Demolition -

Grading - based on info from applicant

Vehicle Trips - based on info from Transportation Impact Study

Area Mitigation -

Energy Mitigation -

| Table Name | Column Name | Default Value | New Value |
|---------------------------|------------------|---------------|-----------|
| tblConstructionPhase | NumDays | 18.00 | 348.00 |
| tblConstructionPhase | NumDays | 230.00 | 348.00 |
| tblConstructionPhase | NumDays | 20.00 | 44.00 |
| tblConstructionPhase | NumDays | 8.00 | 16.00 |
| tblConstructionPhase | NumDays | 18.00 | 11.00 |
| tblConstructionPhase | PhaseEndDate | 5/16/2019 | 1/29/2018 |
| tblConstructionPhase | PhaseStartDate | 1/16/2018 | 9/29/2016 |
| tblGrading | AcresOfGrading | 8.00 | 2.90 |
| tblGrading | MaterialImported | 0.00 | 2,000.00 |
| tblLandUse | LotAcreage | 0.86 | 0.00 |
| tblLandUse | LotAcreage | 1.79 | 0.00 |
| tblLandUse | LotAcreage | 5.63 | 2.92 |
| tblLandUse | LotAcreage | 7.79 | 2.00 |
| tblLandUse | LotAcreage | 0.14 | 0.00 |
| tblProjectCharacteristics | OperationalYear | 2014 | 2018 |
| tblVehicleTrips | ST_TR | 7.16 | 4.32 |
| tblVehicleTrips | ST_TR | 49.97 | 28.11 |
| tblVehicleTrips | ST_TR | 10.08 | 8.15 |
| tblVehicleTrips | SU_TR | 6.07 | 4.32 |
| tblVehicleTrips | SU_TR | 25.24 | 28.11 |
| tblVehicleTrips | SU_TR | 8.77 | 8.15 |
| tblVehicleTrips | WD_TR | 6.59 | 4.32 |
| tblVehicleTrips | WD_TR | 42.94 | 28.11 |
| tblVehicleTrips | WD_TR | 9.57 | 8.15 |

2.0 Emissions Summary

2.1 Overall Construction

Unmitigated Construction

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|-------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|-----------------|--------|----------------|
| Year | | | | | ton | s/yr | | | | | | | МТ | /yr | | |
| 2016 | 0.7813 | 3.0150 | 2.7789 | 3.9900e- 003 | 0.2483 | 0.1681 | 0.4165 | 0.0855 | 0.1573 | 0.2428 | 0.0000 | 349.8431 | 349.8431 | 0.0627 | 0.0000 | 351.1600 |
| 2017 | 2.2593 | 4.2842 | 4.7503 | 8.0500e- 003 | 0.2795 | 0.2626 | 0.5421 | 0.0750 | 0.2478 | 0.3228 | 0.0000 | 665.7887 | 665.7887 | 0.0917 | 0.0000 | 667.7133 |
| 2018 | 0.1574 | 0.1713 | 0.2050 | 3.7000e- 004 | 0.0134 | 0.0102 | 0.0236 | 3.5900e- 003 | 9.6300e- 003 | 0.0132 | 0.0000 | 30.1748 | 30.1748 | 3.9600e- 003 | 0.0000 | 30.2579 |
| Total | 3.1979 | 7.4705 | 7.7342 | 0.0124 | 0.5412 | 0.4408 | 0.9821 | 0.1641 | 0.4147 | 0.5788 | 0.0000 | 1,045.806 6 | 1,045.806 6 | 0.1583 | 0.0000 | 1,049.131 2 |

Mitigated Construction

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|-------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|-----------------|--------|----------------|
| Year | | | | | ton | s/yr | | | | | | | MT | /yr | | |
| 2016 | 0.7813 | 3.0150 | 2.7789 | 3.9900e- 003 | 0.2483 | 0.1681 | 0.4165 | 0.0855 | 0.1573 | 0.2428 | 0.0000 | 349.8428 | 349.8428 | 0.0627 | 0.0000 | 351.1597 |
| 2017 | 2.2593 | 4.2842 | 4.7503 | 8.0500e- 003 | 0.2795 | 0.2626 | 0.5421 | 0.0750 | 0.2478 | 0.3228 | 0.0000 | 665.7883 | 665.7883 | 0.0917 | 0.0000 | 667.7129 |
| 2018 | 0.1574 | 0.1713 | 0.2050 | 3.7000e- 004 | 0.0134 | 0.0102 | 0.0236 | 3.5900e- 003 | 9.6300e- 003 | 0.0132 | 0.0000 | 30.1748 | 30.1748 | 3.9600e- 003 | 0.0000 | 30.2579 |
| Total | 3.1979 | 7.4705 | 7.7342 | 0.0124 | 0.5412 | 0.4408 | 0.9821 | 0.1641 | 0.4147 | 0.5788 | 0.0000 | 1,045.805 9 | 1,045.805 9 | 0.1583 | 0.0000 | 1,049.130 5 |

| | ROG | NOx | со | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio-CO2 | Total CO2 | CH4 | N20 | CO2e |
|----------------------|------|------|------|------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------|-----------|------|------|------|
| Percent Reduction | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

2.2 Overall Operational

Unmitigated Operational

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|-----------------|-----------------|----------------|
| Category | | | | | ton | s/yr | | | | | | | MT | /yr | | |
| Area | 1.7791 | 0.0287 | 2.4741 | 1.3000e- 004 | | 0.0135 | 0.0135 | | 0.0135 | 0.0135 | 0.0000 | 4.0137 | 4.0137 | 3.9900e- 003 | 0.0000 | 4.0974 |
| Energy | 0.0159 | 0.1356 | 0.0584 | 8.6000e- 004 | | 0.0110 | 0.0110 | | 0.0110 | 0.0110 | 0.0000 | 500.8399 | 500.8399 | 0.0199 | 6.3700e- 003 | 503.2333 |
| Mobile | 0.7132 | 1.5654 | 7.3537 | 0.0166 | 1.1576 | 0.0215 | 1.1791 | 0.3101 | 0.0198 | 0.3299 | 0.0000 | 1,224.656 2 | 1,224.656 2 | 0.0498 | 0.0000 | 1,225.701 4 |
| Waste | | | | | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 25.9382 | 0.0000 | 25.9382 | 1.5329 | 0.0000 | 58.1291 |
| Water | ,, | | | | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 5.6435 | 30.6979 | 36.3414 | 0.0209 | 0.0126 | 40.6823 |
| Total | 2.5082 | 1.7297 | 9.8862 | 0.0176 | 1.1576 | 0.0459 | 1.2036 | 0.3101 | 0.0442 | 0.3544 | 31.5817 | 1,760.207 7 | 1,791.789 4 | 1.6275 | 0.0190 | 1,831.843 6 |

2.2 Overall Operational

Mitigated Operational

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|---------------------|--------|----------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|----------------|----------------|-----------------|-----------------|----------------|
| Category | | | <u>.</u> | | ton | s/yr | <u> </u> | | | | | | MT | /yr | | |
| Area | 1.6682 | 0.0287 | 2.4741 | 1.3000e- 004 | | 0.0135 | 0.0135 | | 0.0135 | 0.0135 | 0.0000 | 4.0137 | 4.0137 | 3.9900e- 003 | 0.0000 | 4.0974 |
| Energy | 0.0126 | 0.1076 | 0.0464 | 6.9000e- 004 | | 8.7000e- 003 | 8.7000e- 003 | | 8.7000e- 003 | 8.7000e- 003 | 0.0000 | 461.0917 | 461.0917 | 0.0189 | 5.7000e- 003 | 463.2573 |
| Mobile | 0.7132 | 1.5654 | 7.3537 | 0.0166 | 1.1576 | 0.0215 | 1.1791 | 0.3101 | 0.0198 | 0.3299 | 0.0000 | 1,224.656 2 | 1,224.656 2 | 0.0498 | 0.0000 | 1,225.701 4 |
| Waste | n 11 11 11 | | | | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 25.9382 | 0.0000 | 25.9382 | 1.5329 | 0.0000 | 58.1291 |
| Water | n | | | | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 5.6435 | 30.6979 | 36.3414 | 0.0210 | 0.0126 | 40.6886 |
| Total | 2.3941 | 1.7018 | 9.8742 | 0.0174 | 1.1576 | 0.0437 | 1.2013 | 0.3101 | 0.0420 | 0.3521 | 31.5817 | 1,720.459 5 | 1,752.041 2 | 1.6266 | 0.0183 | 1,791.873 9 |

| | | ROG | NOx | со | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio-CO2 | Total CO2 | CH4 | N20 | CO2e |
|---|----------------------|------|------|------|------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------|-----------|------|------|------|
| ſ | Percent Reduction | 4.55 | 1.62 | 0.12 | 0.97 | 0.00 | 4.92 | 0.19 | 0.00 | 5.11 | 0.64 | 0.00 | 2.26 | 2.22 | 0.06 | 3.43 | 2.18 |

3.0 Construction Detail

Construction Phase

| Phase Number | Phase Name | Phase Type | Start Date | End Date | Num Days Week | Num Days | Phase Description |
|-----------------|-----------------------|-----------------------|------------|-----------|------------------|----------|-------------------|
| 1 | Demolition | Demolition | 6/1/2016 | 8/1/2016 | 5 | 44 | |
| 2 | Site Preparation | Site Preparation | 8/2/2016 | 8/8/2016 | 5 | 5 | |
| 3 | Grading | Grading | 8/9/2016 | 8/30/2016 | 5 | 16 | |
| 4 | Paving | Paving | 8/31/2016 | 9/14/2016 | 5 | 11 | |
| 5 | Building Construction | Building Construction | 9/15/2016 | 1/15/2018 | 5 | 348 | |
| 6 | Architectural Coating | Architectural Coating | 9/29/2016 | 1/29/2018 | 5 | 348 | |

Acres of Grading (Site Preparation Phase): 0

Acres of Grading (Grading Phase): 2.9

Acres of Paving: 0

Residential Indoor: 520,830; Residential Outdoor: 173,610; Non-Residential Indoor: 127,728; Non-Residential Outdoor: 42,576 (Architectural Coating – sqft)

OffRoad Equipment

| Phase Name | Offroad Equipment Type | Amount | Usage Hours | Horse Power | Load Factor |
|-----------------------|---------------------------|--------|-------------|-------------|-------------|
| Demolition | Concrete/Industrial Saws | 1 | 8.00 | 81 | 0.73 |
| Demolition | Excavators | 3 | 8.00 | 162 | 0.38 |
| Demolition | Rubber Tired Dozers | 2 | 8.00 | 255 | 0.40 |
| Site Preparation | Rubber Tired Dozers | 3 | 8.00 | 255 | 0.40 |
| Site Preparation | Tractors/Loaders/Backhoes | 4 | 8.00 | 97 | 0.37 |
| Grading | Excavators | 1 | 8.00 | 162 | 0.38 |
| Grading | Graders | 1 | 8.00 | 174 | 0.41 |
| Grading | Rubber Tired Dozers | 1 | 8.00 | 255 | 0.40 |
| Grading | Tractors/Loaders/Backhoes | 3 | 8.00 | 97 | 0.37 |
| Paving | Cement and Mortar Mixers | 2 | 6.00 | 9 | 0.56 |
| Paving | Pavers | 1 | 8.00 | 125 | 0.42 |
| Paving | Paving Equipment | 2 | 6.00 | 130 | 0.36 |
| Paving | Rollers | 2 | 6.00 | 80 | 0.38 |
| Paving | Tractors/Loaders/Backhoes | 1 | 8.00 | 97 | 0.37 |
| Building Construction | Cranes | 1 | 7.00 | 226 | 0.29 |
| Building Construction | Forklifts | 3 | 8.00 | 89 | 0.20 |
| Building Construction | Generator Sets | 1 | 8.00 | 84 | 0.74 |
| Building Construction | Tractors/Loaders/Backhoes | 3 | 7.00 | 97 | 0.37 |
| Building Construction | Welders | 1 | 8.00 | 46 | 0.45 |
| Architectural Coating | Air Compressors | 1 | 6.00 | 78 | 0.48 |

Trips and VMT

| Phase Name | Offroad Equipment Count | Worker Trip Number | Vendor Trip Number | Hauling Trip Number | Worker Trip Length | Vendor Trip Length | Hauling Trip Length | Worker Vehicle Class | Vendor Vehicle Class | Hauling Vehicle Class |
|-----------------------|----------------------------|-----------------------|-----------------------|------------------------|-----------------------|-----------------------|------------------------|-------------------------|-------------------------|--------------------------|
| Demolition | 6 | 15.00 | 0.00 | 546.00 | 10.00 | 6.50 | 20.00 | LD_Mix | HDT_Mix | HHDT |
| Site Preparation | 7 | 18.00 | 0.00 | 0.00 | 10.00 | 6.50 | 20.00 | LD_Mix | HDT_Mix | HHDT |
| Grading | 6 | 15.00 | 0.00 | 198.00 | 10.00 | 6.50 | 20.00 | LD_Mix | HDT_Mix | HHDT |
| Paving | 8 | 20.00 | 0.00 | 0.00 | 10.00 | 6.50 | 20.00 | LD_Mix | HDT_Mix | HHDT |
| Building Construction | 9 | 214.00 | 46.00 | 0.00 | 10.00 | 6.50 | 20.00 | LD_Mix | HDT_Mix | HHDT |
| Architectural Coating | 1 | 43.00 | 0.00 | 0.00 | 10.00 | 6.50 | 20.00 | LD_Mix | HDT_Mix | HHDT |

3.1 Mitigation Measures Construction

3.2 Demolition - 2016

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|---------------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|-----------------|----------|-----------|-----------|--------|--------|---------|
| Category | | | | | ton | s/yr | | | | | | | МТ | '/yr | | |
| Fugitive Dust | | | | | 0.0616 | 0.0000 | 0.0616 | 9.3200e- 003 | 0.0000 | 9.3200e- 003 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Off-Road | 0.0943 | 1.0044 | 0.7707 | 8.8000e- 004 | | 0.0504 | 0.0504 | | 0.0470 | 0.0470 | 0.0000 | 81.6142 | 81.6142 | 0.0222 | 0.0000 | 82.0803 |
| Total | 0.0943 | 1.0044 | 0.7707 | 8.8000e- 004 | 0.0616 | 0.0504 | 0.1120 | 9.3200e- 003 | 0.0470 | 0.0563 | 0.0000 | 81.6142 | 81.6142 | 0.0222 | 0.0000 | 82.0803 |

3.2 Demolition - 2016

Unmitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|-----------------|-----------------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|---------|
| Category | | | | | ton | s/yr | | | | | | | MT | '/yr | | |
| Hauling | 7.0300e- 003 | 0.0715 | 0.0947 | 2.0000e- 004 | 4.5900e- 003 | 1.0400e- 003 | 5.6300e- 003 | 1.2600e- 003 | 9.6000e- 004 | 2.2200e- 003 | 0.0000 | 17.9443 | 17.9443 | 1.3000e- 004 | 0.0000 | 17.9470 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker | 1.1100e- 003 | 1.3200e- 003 | 0.0138 | 3.0000e- 005 | 2.4200e- 003 | 2.0000e- 005 | 2.4400e- 003 | 6.4000e- 004 | 2.0000e- 005 | 6.6000e- 004 | 0.0000 | 2.1630 | 2.1630 | 1.2000e- 004 | 0.0000 | 2.1654 |
| Total | 8.1400e- 003 | 0.0729 | 0.1085 | 2.3000e- 004 | 7.0100e- 003 | 1.0600e- 003 | 8.0700e- 003 | 1.9000e- 003 | 9.8000e- 004 | 2.8800e- 003 | 0.0000 | 20.1073 | 20.1073 | 2.5000e- 004 | 0.0000 | 20.1124 |

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|---------------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|-----------------|----------|-----------|-----------|--------|--------|---------|
| Category | | | | | ton | s/yr | | | | | | | МТ | /yr | | |
| r ughtvo Buot | | | | | 0.0616 | 0.0000 | 0.0616 | 9.3200e- 003 | 0.0000 | 9.3200e- 003 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Off-Road | 0.0943 | 1.0044 | 0.7707 | 8.8000e- 004 | | 0.0504 | 0.0504 | | 0.0470 | 0.0470 | 0.0000 | 81.6141 | 81.6141 | 0.0222 | 0.0000 | 82.0802 |
| Total | 0.0943 | 1.0044 | 0.7707 | 8.8000e- 004 | 0.0616 | 0.0504 | 0.1120 | 9.3200e- 003 | 0.0470 | 0.0563 | 0.0000 | 81.6141 | 81.6141 | 0.0222 | 0.0000 | 82.0802 |

3.2 Demolition - 2016

Mitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|-----------------|-----------------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|---------|
| Category | | | | | ton | s/yr | | | | | | | МТ | /yr | | |
| Hauling | 7.0300e- 003 | 0.0715 | 0.0947 | 2.0000e- 004 | 4.5900e- 003 | 1.0400e- 003 | 5.6300e- 003 | 1.2600e- 003 | 9.6000e- 004 | 2.2200e- 003 | 0.0000 | 17.9443 | 17.9443 | 1.3000e- 004 | 0.0000 | 17.9470 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker | 1.1100e- 003 | 1.3200e- 003 | 0.0138 | 3.0000e- 005 | 2.4200e- 003 | 2.0000e- 005 | 2.4400e- 003 | 6.4000e- 004 | 2.0000e- 005 | 6.6000e- 004 | 0.0000 | 2.1630 | 2.1630 | 1.2000e- 004 | 0.0000 | 2.1654 |
| Total | 8.1400e- 003 | 0.0729 | 0.1085 | 2.3000e- 004 | 7.0100e- 003 | 1.0600e- 003 | 8.0700e- 003 | 1.9000e- 003 | 9.8000e- 004 | 2.8800e- 003 | 0.0000 | 20.1073 | 20.1073 | 2.5000e- 004 | 0.0000 | 20.1124 |

3.3 Site Preparation - 2016

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------------|--------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|--------|
| Category | | | | | ton | s/yr | | | | | | | МТ | /yr | | |
| r ugilive Dust | | | | | 0.0452 | 0.0000 | 0.0452 | 0.0248 | 0.0000 | 0.0248 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Off-Road | 0.0127 | 0.1366 | 0.1028 | 1.0000e- 004 | | 7.3500e- 003 | 7.3500e- 003 | | 6.7600e- 003 | 6.7600e- 003 | 0.0000 | 9.2193 | 9.2193 | 2.7800e- 003 | 0.0000 | 9.2777 |
| Total | 0.0127 | 0.1366 | 0.1028 | 1.0000e- 004 | 0.0452 | 7.3500e- 003 | 0.0525 | 0.0248 | 6.7600e- 003 | 0.0316 | 0.0000 | 9.2193 | 9.2193 | 2.7800e- 003 | 0.0000 | 9.2777 |

3.3 Site Preparation - 2016

Unmitigated Construction Off-Site

| | ROG | NOx | СО | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|-----------------|-----------------|-----------------|--------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|--------|
| Category | | | | | ton | s/yr | | | | | | | MT | /yr | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker | 1.5000e- 004 | 1.8000e- 004 | 1.8900e- 003 | 0.0000 | 3.3000e- 004 | 0.0000 | 3.3000e- 004 | 9.0000e- 005 | 0.0000 | 9.0000e- 005 | 0.0000 | 0.2950 | 0.2950 | 2.0000e- 005 | 0.0000 | 0.2953 |
| Total | 1.5000e- 004 | 1.8000e- 004 | 1.8900e- 003 | 0.0000 | 3.3000e- 004 | 0.0000 | 3.3000e- 004 | 9.0000e- 005 | 0.0000 | 9.0000e- 005 | 0.0000 | 0.2950 | 0.2950 | 2.0000e- 005 | 0.0000 | 0.2953 |

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------------|--------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|--------|
| Category | | | | | ton | s/yr | | | | | | | МТ | /yr | | |
| r ugilivo Buot | | | | | 0.0452 | 0.0000 | 0.0452 | 0.0248 | 0.0000 | 0.0248 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Off-Road | 0.0127 | 0.1366 | 0.1028 | 1.0000e- 004 | | 7.3500e- 003 | 7.3500e- 003 | | 6.7600e- 003 | 6.7600e- 003 | 0.0000 | 9.2193 | 9.2193 | 2.7800e- 003 | 0.0000 | 9.2777 |
| Total | 0.0127 | 0.1366 | 0.1028 | 1.0000e- 004 | 0.0452 | 7.3500e- 003 | 0.0525 | 0.0248 | 6.7600e- 003 | 0.0316 | 0.0000 | 9.2193 | 9.2193 | 2.7800e- 003 | 0.0000 | 9.2777 |

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3.3 Site Preparation - 2016

Mitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|-----------------|-----------------|-----------------|--------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|--------|
| Category | | | | | ton | s/yr | | | | | | | МТ | /yr | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker | 1.5000e- 004 | 1.8000e- 004 | 1.8900e- 003 | 0.0000 | 3.3000e- 004 | 0.0000 | 3.3000e- 004 | 9.0000e- 005 | 0.0000 | 9.0000e- 005 | 0.0000 | 0.2950 | 0.2950 | 2.0000e- 005 | 0.0000 | 0.2953 |
| Total | 1.5000e- 004 | 1.8000e- 004 | 1.8900e- 003 | 0.0000 | 3.3000e- 004 | 0.0000 | 3.3000e- 004 | 9.0000e- 005 | 0.0000 | 9.0000e- 005 | 0.0000 | 0.2950 | 0.2950 | 2.0000e- 005 | 0.0000 | 0.2953 |

3.4 Grading - 2016

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|---------------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|-----------------|--------|---------|
| Category | | | | | ton | s/yr | | | | | | | MT | /yr | | |
| r ugiavo Euor | | | | | 0.0497 | 0.0000 | 0.0497 | 0.0267 | 0.0000 | 0.0267 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Off-Road | 0.0293 | 0.3076 | 0.2086 | 2.4000e- 004 | | 0.0176 | 0.0176 | | 0.0162 | 0.0162 | 0.0000 | 22.4531 | 22.4531 | 6.7700e- 003 | 0.0000 | 22.5953 |
| Total | 0.0293 | 0.3076 | 0.2086 | 2.4000e- 004 | 0.0497 | 0.0176 | 0.0673 | 0.0267 | 0.0162 | 0.0428 | 0.0000 | 22.4531 | 22.4531 | 6.7700e- 003 | 0.0000 | 22.5953 |

3.4 Grading - 2016

Unmitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|--------|
| Category | | | | | ton | s/yr | | | | | | | MT | /yr | | |
| Hauling | 2.5500e- 003 | 0.0259 | 0.0343 | 7.0000e- 005 | 1.6600e- 003 | 3.8000e- 004 | 2.0400e- 003 | 4.6000e- 004 | 3.5000e- 004 | 8.0000e- 004 | 0.0000 | 6.5073 | 6.5073 | 5.0000e- 005 | 0.0000 | 6.5082 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker | 4.0000e- 004 | 4.8000e- 004 | 5.0300e- 003 | 1.0000e- 005 | 8.8000e- 004 | 1.0000e- 005 | 8.9000e- 004 | 2.3000e- 004 | 1.0000e- 005 | 2.4000e- 004 | 0.0000 | 0.7866 | 0.7866 | 4.0000e- 005 | 0.0000 | 0.7874 |
| Total | 2.9500e- 003 | 0.0264 | 0.0394 | 8.0000e- 005 | 2.5400e- 003 | 3.9000e- 004 | 2.9300e- 003 | 6.9000e- 004 | 3.6000e- 004 | 1.0400e- 003 | 0.0000 | 7.2938 | 7.2938 | 9.0000e- 005 | 0.0000 | 7.2957 |

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|---------------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|-----------------|--------|---------|
| Category | | | | | ton | s/yr | | | | | | | MT | /yr | | |
| r ughtvo Buot | | | | | 0.0497 | 0.0000 | 0.0497 | 0.0267 | 0.0000 | 0.0267 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Off-Road | 0.0293 | 0.3076 | 0.2086 | 2.4000e- 004 | | 0.0176 | 0.0176 | | 0.0162 | 0.0162 | 0.0000 | 22.4531 | 22.4531 | 6.7700e- 003 | 0.0000 | 22.5953 |
| Total | 0.0293 | 0.3076 | 0.2086 | 2.4000e- 004 | 0.0497 | 0.0176 | 0.0673 | 0.0267 | 0.0162 | 0.0428 | 0.0000 | 22.4531 | 22.4531 | 6.7700e- 003 | 0.0000 | 22.5953 |

3.4 Grading - 2016

Mitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|--------|
| Category | | | | | ton | s/yr | | | | | | | MT | /yr | | |
| Hauling | 2.5500e- 003 | 0.0259 | 0.0343 | 7.0000e- 005 | 1.6600e- 003 | 3.8000e- 004 | 2.0400e- 003 | 4.6000e- 004 | 3.5000e- 004 | 8.0000e- 004 | 0.0000 | 6.5073 | 6.5073 | 5.0000e- 005 | 0.0000 | 6.5082 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker | 4.0000e- 004 | 4.8000e- 004 | 5.0300e- 003 | 1.0000e- 005 | 8.8000e- 004 | 1.0000e- 005 | 8.9000e- 004 | 2.3000e- 004 | 1.0000e- 005 | 2.4000e- 004 | 0.0000 | 0.7866 | 0.7866 | 4.0000e- 005 | 0.0000 | 0.7874 |
| Total | 2.9500e- 003 | 0.0264 | 0.0394 | 8.0000e- 005 | 2.5400e- 003 | 3.9000e- 004 | 2.9300e- 003 | 6.9000e- 004 | 3.6000e- 004 | 1.0400e- 003 | 0.0000 | 7.2938 | 7.2938 | 9.0000e- 005 | 0.0000 | 7.2957 |

3.5 Paving - 2016

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|--------|
| Category | | | | | ton | s/yr | | | | | | | МТ | /yr | | |
| Off-Road | 9.8800e- 003 | 0.1009 | 0.0691 | 1.0000e- 004 | | 6.0900e- 003 | 6.0900e- 003 | | 5.6100e- 003 | 5.6100e- 003 | 0.0000 | 9.4912 | 9.4912 | 2.7900e- 003 | 0.0000 | 9.5497 |
| Paving | 0.0000 | | | | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Total | 9.8800e- 003 | 0.1009 | 0.0691 | 1.0000e- 004 | | 6.0900e- 003 | 6.0900e- 003 | | 5.6100e- 003 | 5.6100e- 003 | 0.0000 | 9.4912 | 9.4912 | 2.7900e- 003 | 0.0000 | 9.5497 |

3.5 Paving - 2016

Unmitigated Construction Off-Site

| | ROG | NOx | со | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|--------|
| Category | | | | | ton | s/yr | | | | | | | МТ | /yr | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker | 3.7000e- 004 | 4.4000e- 004 | 4.6100e- 003 | 1.0000e- 005 | 8.1000e- 004 | 1.0000e- 005 | 8.1000e- 004 | 2.1000e- 004 | 1.0000e- 005 | 2.2000e- 004 | 0.0000 | 0.7210 | 0.7210 | 4.0000e- 005 | 0.0000 | 0.7218 |
| Total | 3.7000e- 004 | 4.4000e- 004 | 4.6100e- 003 | 1.0000e- 005 | 8.1000e- 004 | 1.0000e- 005 | 8.1000e- 004 | 2.1000e- 004 | 1.0000e- 005 | 2.2000e- 004 | 0.0000 | 0.7210 | 0.7210 | 4.0000e- 005 | 0.0000 | 0.7218 |

| | ROG | NOx | СО | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|--------|
| Category | | | | | ton | s/yr | | | | | | | MT | /yr | | |
| Off-Road | 9.8800e- 003 | 0.1009 | 0.0691 | 1.0000e- 004 | | 6.0900e- 003 | 6.0900e- 003 | | 5.6100e- 003 | 5.6100e- 003 | 0.0000 | 9.4912 | 9.4912 | 2.7900e- 003 | 0.0000 | 9.5497 |
| Paving | 0.0000 | | | | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Total | 9.8800e- 003 | 0.1009 | 0.0691 | 1.0000e- 004 | | 6.0900e- 003 | 6.0900e- 003 | | 5.6100e- 003 | 5.6100e- 003 | 0.0000 | 9.4912 | 9.4912 | 2.7900e- 003 | 0.0000 | 9.5497 |

3.5 Paving - 2016

Mitigated Construction Off-Site

| | ROG | NOx | СО | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|--------|
| Category | | | | | ton | s/yr | | | | | | | MT | /yr | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker | 3.7000e- 004 | 4.4000e- 004 | 4.6100e- 003 | 1.0000e- 005 | 8.1000e- 004 | 1.0000e- 005 | 8.1000e- 004 | 2.1000e- 004 | 1.0000e- 005 | 2.2000e- 004 | 0.0000 | 0.7210 | 0.7210 | 4.0000e- 005 | 0.0000 | 0.7218 |
| Total | 3.7000e- 004 | 4.4000e- 004 | 4.6100e- 003 | 1.0000e- 005 | 8.1000e- 004 | 1.0000e- 005 | 8.1000e- 004 | 2.1000e- 004 | 1.0000e- 005 | 2.2000e- 004 | 0.0000 | 0.7210 | 0.7210 | 4.0000e- 005 | 0.0000 | 0.7218 |

3.6 Building Construction - 2016

| | ROG | NOx | СО | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|--------|--------|---------|
| Category | | | | | ton | s/yr | | | | | | | MT | /yr | | |
| Off-Road | 0.1311 | 1.0975 | 0.7125 | 1.0300e- 003 | | 0.0757 | 0.0757 | | 0.0712 | 0.0712 | 0.0000 | 93.2291 | 93.2291 | 0.0231 | 0.0000 | 93.7147 |
| Total | 0.1311 | 1.0975 | 0.7125 | 1.0300e- 003 | | 0.0757 | 0.0757 | | 0.0712 | 0.0712 | 0.0000 | 93.2291 | 93.2291 | 0.0231 | 0.0000 | 93.7147 |

Unmitigated Construction Off-Site

| | ROG | NOx | СО | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|---------|
| Category | | | | | ton | s/yr | | | | | | | МТ | /yr | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor | 0.0237 | 0.1500 | 0.2918 | 3.7000e- 004 | 0.0101 | 2.3500e- 003 | 0.0125 | 2.8900e- 003 | 2.1500e- 003 | 5.0400e- 003 | 0.0000 | 33.4209 | 33.4209 | 2.7000e- 004 | 0.0000 | 33.4265 |
| Worker | 0.0276 | 0.0330 | 0.3455 | 7.2000e- 004 | 0.0605 | 4.6000e- 004 | 0.0610 | 0.0161 | 4.2000e- 004 | 0.0165 | 0.0000 | 54.0030 | 54.0030 | 2.8900e- 003 | 0.0000 | 54.0636 |
| Total | 0.0513 | 0.1829 | 0.6373 | 1.0900e- 003 | 0.0706 | 2.8100e- 003 | 0.0734 | 0.0190 | 2.5700e- 003 | 0.0216 | 0.0000 | 87.4239 | 87.4239 | 3.1600e- 003 | 0.0000 | 87.4901 |

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|--------|--------|---------|
| Category | | | | | ton | s/yr | | | | | | | МТ | /yr | | |
| | 0.1311 | 1.0975 | 0.7125 | 1.0300e- 003 | | 0.0757 | 0.0757 | | 0.0712 | 0.0712 | 0.0000 | 93.2290 | 93.2290 | 0.0231 | 0.0000 | 93.7146 |
| Total | 0.1311 | 1.0975 | 0.7125 | 1.0300e- 003 | | 0.0757 | 0.0757 | | 0.0712 | 0.0712 | 0.0000 | 93.2290 | 93.2290 | 0.0231 | 0.0000 | 93.7146 |

Mitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|---------|
| Category | | | | | ton | s/yr | | | | | | | МТ | /yr | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor | 0.0237 | 0.1500 | 0.2918 | 3.7000e- 004 | 0.0101 | 2.3500e- 003 | 0.0125 | 2.8900e- 003 | 2.1500e- 003 | 5.0400e- 003 | 0.0000 | 33.4209 | 33.4209 | 2.7000e- 004 | 0.0000 | 33.4265 |
| Worker | 0.0276 | 0.0330 | 0.3455 | 7.2000e- 004 | 0.0605 | 4.6000e- 004 | 0.0610 | 0.0161 | 4.2000e- 004 | 0.0165 | 0.0000 | 54.0030 | 54.0030 | 2.8900e- 003 | 0.0000 | 54.0636 |
| Total | 0.0513 | 0.1829 | 0.6373 | 1.0900e- 003 | 0.0706 | 2.8100e- 003 | 0.0734 | 0.0190 | 2.5700e- 003 | 0.0216 | 0.0000 | 87.4239 | 87.4239 | 3.1600e- 003 | 0.0000 | 87.4901 |

3.6 Building Construction - 2017

| | ROG | NOx | СО | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|--------|--------|----------|
| Category | | | | | ton | s/yr | | | | | | | МТ | /yr | | |
| Off-Road | 0.4033 | 3.4327 | 2.3568 | 3.4900e- 003 | | 0.2316 | 0.2316 | 1 1 1 | 0.2175 | 0.2175 | 0.0000 | 311.3228 | 311.3228 | 0.0766 | 0.0000 | 312.9319 |
| Total | 0.4033 | 3.4327 | 2.3568 | 3.4900e- 003 | | 0.2316 | 0.2316 | | 0.2175 | 0.2175 | 0.0000 | 311.3228 | 311.3228 | 0.0766 | 0.0000 | 312.9319 |

Unmitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|-----------------|--------|----------|
| Category | | | | | ton | s/yr | | | | | | | МТ | /yr | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor | 0.0687 | 0.4481 | 0.9010 | 1.2500e- 003 | 0.0341 | 6.6800e- 003 | 0.0408 | 9.7500e- 003 | 6.1300e- 003 | 0.0159 | 0.0000 | 110.9491 | 110.9491 | 8.4000e- 004 | 0.0000 | 110.9667 |
| Worker | 0.0827 | 0.0994 | 1.0406 | 2.4400e- 003 | 0.2043 | 1.5000e- 003 | 0.2058 | 0.0543 | 1.3900e- 003 | 0.0557 | 0.0000 | 175.1340 | 175.1340 | 8.8900e- 003 | 0.0000 | 175.3208 |
| Total | 0.1514 | 0.5475 | 1.9416 | 3.6900e- 003 | 0.2384 | 8.1800e- 003 | 0.2466 | 0.0641 | 7.5200e- 003 | 0.0716 | 0.0000 | 286.0831 | 286.0831 | 9.7300e- 003 | 0.0000 | 286.2875 |

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|--------|--------|----------|
| Category | | | | | ton | s/yr | | | | | | | MT | /yr | | |
| Off-Road | 0.4033 | 3.4327 | 2.3568 | 3.4900e- 003 | | 0.2316 | 0.2316 | | 0.2175 | 0.2175 | 0.0000 | 311.3225 | 311.3225 | 0.0766 | 0.0000 | 312.9315 |
| Total | 0.4033 | 3.4327 | 2.3568 | 3.4900e- 003 | | 0.2316 | 0.2316 | | 0.2175 | 0.2175 | 0.0000 | 311.3225 | 311.3225 | 0.0766 | 0.0000 | 312.9315 |

Mitigated Construction Off-Site

| | ROG | NOx | СО | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|-----------------|--------|----------|
| Category | | | | | ton | is/yr | | | | | | | МТ | /yr | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor | 0.0687 | 0.4481 | 0.9010 | 1.2500e- 003 | 0.0341 | 6.6800e- 003 | 0.0408 | 9.7500e- 003 | 6.1300e- 003 | 0.0159 | 0.0000 | 110.9491 | 110.9491 | 8.4000e- 004 | 0.0000 | 110.9667 |
| Worker | 0.0827 | 0.0994 | 1.0406 | 2.4400e- 003 | 0.2043 | 1.5000e- 003 | 0.2058 | 0.0543 | 1.3900e- 003 | 0.0557 | 0.0000 | 175.1340 | 175.1340 | 8.8900e- 003 | 0.0000 | 175.3208 |
| Total | 0.1514 | 0.5475 | 1.9416 | 3.6900e- 003 | 0.2384 | 8.1800e- 003 | 0.2466 | 0.0641 | 7.5200e- 003 | 0.0716 | 0.0000 | 286.0831 | 286.0831 | 9.7300e- 003 | 0.0000 | 286.2875 |

3.6 Building Construction - 2018

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|---------|
| Category | | | | | ton | s/yr | | | | | | | MT | /yr | | |
| | 0.0147 | 0.1279 | 0.0964 | 1.5000e- 004 | | 8.2200e- 003 | 8.2200e- 003 | 1 1 1 | 7.7300e- 003 | 7.7300e- 003 | 0.0000 | 13.0223 | 13.0223 | 3.1900e- 003 | 0.0000 | 13.0893 |
| Total | 0.0147 | 0.1279 | 0.0964 | 1.5000e- 004 | | 8.2200e- 003 | 8.2200e- 003 | | 7.7300e- 003 | 7.7300e- 003 | 0.0000 | 13.0223 | 13.0223 | 3.1900e- 003 | 0.0000 | 13.0893 |

Unmitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|-----------------|-----------------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|---------|
| Category | | | | | ton | s/yr | | | | | | | МТ | /yr | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor | 2.4000e- 003 | 0.0171 | 0.0344 | 5.0000e- 005 | 1.4400e- 003 | 2.6000e- 004 | 1.7000e- 003 | 4.1000e- 004 | 2.4000e- 004 | 6.5000e- 004 | 0.0000 | 4.6073 | 4.6073 | 3.0000e- 005 | 0.0000 | 4.6080 |
| Worker | 3.1200e- 003 | 3.7800e- 003 | 0.0396 | 1.0000e- 004 | 8.6400e- 003 | 6.0000e- 005 | 8.7100e- 003 | 2.3000e- 003 | 6.0000e- 005 | 2.3600e- 003 | 0.0000 | 7.1294 | 7.1294 | 3.5000e- 004 | 0.0000 | 7.1367 |
| Total | 5.5200e- 003 | 0.0209 | 0.0739 | 1.5000e- 004 | 0.0101 | 3.2000e- 004 | 0.0104 | 2.7100e- 003 | 3.0000e- 004 | 3.0100e- 003 | 0.0000 | 11.7367 | 11.7367 | 3.8000e- 004 | 0.0000 | 11.7447 |

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|---------|
| Category | | | | | ton | s/yr | | | | | | | МТ | /yr | | |
| | 0.0147 | 0.1279 | 0.0964 | 1.5000e- 004 | | 8.2200e- 003 | 8.2200e- 003 | 1 | 7.7300e- 003 | 7.7300e- 003 | 0.0000 | 13.0223 | 13.0223 | 3.1900e- 003 | 0.0000 | 13.0892 |
| Total | 0.0147 | 0.1279 | 0.0964 | 1.5000e- 004 | | 8.2200e- 003 | 8.2200e- 003 | | 7.7300e- 003 | 7.7300e- 003 | 0.0000 | 13.0223 | 13.0223 | 3.1900e- 003 | 0.0000 | 13.0892 |

Mitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|-----------------|-----------------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|---------|
| Category | | | | | ton | s/yr | | | | | | | МТ | /yr | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor | 2.4000e- 003 | 0.0171 | 0.0344 | 5.0000e- 005 | 1.4400e- 003 | 2.6000e- 004 | 1.7000e- 003 | 4.1000e- 004 | 2.4000e- 004 | 6.5000e- 004 | 0.0000 | 4.6073 | 4.6073 | 3.0000e- 005 | 0.0000 | 4.6080 |
| Worker | 3.1200e- 003 | 3.7800e- 003 | 0.0396 | 1.0000e- 004 | 8.6400e- 003 | 6.0000e- 005 | 8.7100e- 003 | 2.3000e- 003 | 6.0000e- 005 | 2.3600e- 003 | 0.0000 | 7.1294 | 7.1294 | 3.5000e- 004 | 0.0000 | 7.1367 |
| Total | 5.5200e- 003 | 0.0209 | 0.0739 | 1.5000e- 004 | 0.0101 | 3.2000e- 004 | 0.0104 | 2.7100e- 003 | 3.0000e- 004 | 3.0100e- 003 | 0.0000 | 11.7367 | 11.7367 | 3.8000e- 004 | 0.0000 | 11.7447 |

3.7 Architectural Coating - 2016

| | ROG | NOx | СО | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|-----------------|--------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|--------|
| Category | | | | | ton | s/yr | | | | | | | MT | /yr | | |
| Archit. Coating | 0.4238 | | | | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Off-Road | 0.0123 | 0.0795 | 0.0631 | 1.0000e- 004 | | 6.5900e- 003 | 6.5900e- 003 | | 6.5900e- 003 | 6.5900e- 003 | 0.0000 | 8.5534 | 8.5534 | 1.0100e- 003 | 0.0000 | 8.5746 |
| Total | 0.4362 | 0.0795 | 0.0631 | 1.0000e- 004 | | 6.5900e- 003 | 6.5900e- 003 | | 6.5900e- 003 | 6.5900e- 003 | 0.0000 | 8.5534 | 8.5534 | 1.0100e- 003 | 0.0000 | 8.5746 |

Unmitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|-----------------|-----------------|----------|-----------------|------------------|-----------------|---------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|--------|
| Category | | | <u>.</u> | | ton | s/yr | | | | | | | МТ | /yr | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker | 4.8300e- 003 | 5.7600e- 003 | 0.0604 | 1.3000e- 004 | 0.0106 | 8.0000e- 005 | 0.0107 | 2.8100e- 003 | 7.0000e- 005 | 2.8900e- 003 | 0.0000 | 9.4418 | 9.4418 | 5.0000e- 004 | 0.0000 | 9.4524 |
| Total | 4.8300e- 003 | 5.7600e- 003 | 0.0604 | 1.3000e- 004 | 0.0106 | 8.0000e- 005 | 0.0107 | 2.8100e- 003 | 7.0000e- 005 | 2.8900e- 003 | 0.0000 | 9.4418 | 9.4418 | 5.0000e- 004 | 0.0000 | 9.4524 |

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|-----------------|--------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|--------|
| Category | | | | | ton | s/yr | | | | | | | МТ | '/yr | | |
| Archit. Coating | 0.4238 | | | | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Off-Road | 0.0123 | 0.0795 | 0.0631 | 1.0000e- 004 | | 6.5900e- 003 | 6.5900e- 003 | | 6.5900e- 003 | 6.5900e- 003 | 0.0000 | 8.5534 | 8.5534 | 1.0100e- 003 | 0.0000 | 8.5746 |
| Total | 0.4362 | 0.0795 | 0.0631 | 1.0000e- 004 | | 6.5900e- 003 | 6.5900e- 003 | | 6.5900e- 003 | 6.5900e- 003 | 0.0000 | 8.5534 | 8.5534 | 1.0100e- 003 | 0.0000 | 8.5746 |

Mitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|-----------------|-----------------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|--------|
| Category | | | | | ton | s/yr | | | | | | | МТ | /yr | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker | 4.8300e- 003 | 5.7600e- 003 | 0.0604 | 1.3000e- 004 | 0.0106 | 8.0000e- 005 | 0.0107 | 2.8100e- 003 | 7.0000e- 005 | 2.8900e- 003 | 0.0000 | 9.4418 | 9.4418 | 5.0000e- 004 | 0.0000 | 9.4524 |
| Total | 4.8300e- 003 | 5.7600e- 003 | 0.0604 | 1.3000e- 004 | 0.0106 | 8.0000e- 005 | 0.0107 | 2.8100e- 003 | 7.0000e- 005 | 2.8900e- 003 | 0.0000 | 9.4418 | 9.4418 | 5.0000e- 004 | 0.0000 | 9.4524 |

3.7 Architectural Coating - 2017

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|-----------------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|-----------------|--------|---------|
| Category | | | | | ton | s/yr | | | | | | | МТ | /yr | | |
| Archit. Coating | 1.6447 | | | | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Off-Road | 0.0432 | 0.2841 | 0.2429 | 3.9000e- 004 | | 0.0225 | 0.0225 | | 0.0225 | 0.0225 | 0.0000 | 33.1923 | 33.1923 | 3.5000e- 003 | 0.0000 | 33.2659 |
| Total | 1.6879 | 0.2841 | 0.2429 | 3.9000e- 004 | | 0.0225 | 0.0225 | | 0.0225 | 0.0225 | 0.0000 | 33.1923 | 33.1923 | 3.5000e- 003 | 0.0000 | 33.2659 |

Unmitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|-----------------|--------|---------|
| Category | | | | | ton | s/yr | | | | | | | МТ | /yr | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker | 0.0166 | 0.0200 | 0.2091 | 4.9000e- 004 | 0.0411 | 3.0000e- 004 | 0.0414 | 0.0109 | 2.8000e- 004 | 0.0112 | 0.0000 | 35.1905 | 35.1905 | 1.7900e- 003 | 0.0000 | 35.2280 |
| Total | 0.0166 | 0.0200 | 0.2091 | 4.9000e- 004 | 0.0411 | 3.0000e- 004 | 0.0414 | 0.0109 | 2.8000e- 004 | 0.0112 | 0.0000 | 35.1905 | 35.1905 | 1.7900e- 003 | 0.0000 | 35.2280 |

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|---------------------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|-----------------|--------|---------|
| Category | | | | | ton | s/yr | | | | | | | MT | '/yr | | |
| , a china c coa mig | 1.6447 | | | | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Off-Road | 0.0432 | 0.2841 | 0.2429 | 3.9000e- 004 | | 0.0225 | 0.0225 | | 0.0225 | 0.0225 | 0.0000 | 33.1923 | 33.1923 | 3.5000e- 003 | 0.0000 | 33.2659 |
| Total | 1.6879 | 0.2841 | 0.2429 | 3.9000e- 004 | | 0.0225 | 0.0225 | | 0.0225 | 0.0225 | 0.0000 | 33.1923 | 33.1923 | 3.5000e- 003 | 0.0000 | 33.2659 |

Mitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|--------|----------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|-----------------|--------|---------|
| Category | | <u>.</u> | | | ton | s/yr | | <u>.</u> | | | | | МТ | /yr | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker | 0.0166 | 0.0200 | 0.2091 | 4.9000e- 004 | 0.0411 | 3.0000e- 004 | 0.0414 | 0.0109 | 2.8000e- 004 | 0.0112 | 0.0000 | 35.1905 | 35.1905 | 1.7900e- 003 | 0.0000 | 35.2280 |
| Total | 0.0166 | 0.0200 | 0.2091 | 4.9000e- 004 | 0.0411 | 3.0000e- 004 | 0.0414 | 0.0109 | 2.8000e- 004 | 0.0112 | 0.0000 | 35.1905 | 35.1905 | 1.7900e- 003 | 0.0000 | 35.2280 |

3.7 Architectural Coating - 2018

| | ROG | NOx | СО | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|-----------------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|--------|
| Category | | | | | ton | s/yr | | | | | | | MT | /yr | | |
| Archit. Coating | 0.1328 | | | | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Off-Road | 3.1400e- 003 | 0.0211 | 0.0195 | 3.0000e- 005 | | 1.5800e- 003 | 1.5800e- 003 | | 1.5800e- 003 | 1.5800e- 003 | 0.0000 | 2.6809 | 2.6809 | 2.5000e- 004 | 0.0000 | 2.6863 |
| Total | 0.1360 | 0.0211 | 0.0195 | 3.0000e- 005 | | 1.5800e- 003 | 1.5800e- 003 | | 1.5800e- 003 | 1.5800e- 003 | 0.0000 | 2.6809 | 2.6809 | 2.5000e- 004 | 0.0000 | 2.6863 |

Unmitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|-----------------|-----------------|----------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|--------|
| Category | | | <u>.</u> | | ton | s/yr | | <u>.</u> | | | | | МТ | /yr | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker | 1.2000e- 003 | 1.4500e- 003 | 0.0152 | 4.0000e- 005 | 3.3200e- 003 | 2.0000e- 005 | 3.3400e- 003 | 8.8000e- 004 | 2.0000e- 005 | 9.0000e- 004 | 0.0000 | 2.7349 | 2.7349 | 1.3000e- 004 | 0.0000 | 2.7377 |
| Total | 1.2000e- 003 | 1.4500e- 003 | 0.0152 | 4.0000e- 005 | 3.3200e- 003 | 2.0000e- 005 | 3.3400e- 003 | 8.8000e- 004 | 2.0000e- 005 | 9.0000e- 004 | 0.0000 | 2.7349 | 2.7349 | 1.3000e- 004 | 0.0000 | 2.7377 |

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|---------------------|-----------------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|--------|
| Category | | | | | ton | s/yr | | | | | | | MT | /yr | | |
| , a of the obdating | 0.1328 | | | | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| | 3.1400e- 003 | 0.0211 | 0.0195 | 3.0000e- 005 | | 1.5800e- 003 | 1.5800e- 003 | | 1.5800e- 003 | 1.5800e- 003 | 0.0000 | 2.6809 | 2.6809 | 2.5000e- 004 | 0.0000 | 2.6863 |
| Total | 0.1360 | 0.0211 | 0.0195 | 3.0000e- 005 | | 1.5800e- 003 | 1.5800e- 003 | | 1.5800e- 003 | 1.5800e- 003 | 0.0000 | 2.6809 | 2.6809 | 2.5000e- 004 | 0.0000 | 2.6863 |

Mitigated Construction Off-Site

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------|-----------------|-----------------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|--------|--------|
| Category | | | | | ton | s/yr | | | | | | | МТ | /yr | | |
| Hauling | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Vendor | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Worker | 1.2000e- 003 | 1.4500e- 003 | 0.0152 | 4.0000e- 005 | 3.3200e- 003 | 2.0000e- 005 | 3.3400e- 003 | 8.8000e- 004 | 2.0000e- 005 | 9.0000e- 004 | 0.0000 | 2.7349 | 2.7349 | 1.3000e- 004 | 0.0000 | 2.7377 |
| Total | 1.2000e- 003 | 1.4500e- 003 | 0.0152 | 4.0000e- 005 | 3.3200e- 003 | 2.0000e- 005 | 3.3400e- 003 | 8.8000e- 004 | 2.0000e- 005 | 9.0000e- 004 | 0.0000 | 2.7349 | 2.7349 | 1.3000e- 004 | 0.0000 | 2.7377 |

4.0 Operational Detail - Mobile

4.1 Mitigation Measures Mobile

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|-------------|--------|--------|--------|--------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|----------------|----------------|--------|--------|----------------|
| Category | | | | | ton | s/yr | | | | | | | MT | /yr | | |
| Mitigated | 0.7132 | 1.5654 | 7.3537 | 0.0166 | 1.1576 | 0.0215 | 1.1791 | 0.3101 | 0.0198 | 0.3299 | 0.0000 | 1,224.656 2 | 1,224.656 2 | 0.0498 | 0.0000 | 1,225.701 4 |
| Unmitigated | 0.7132 | 1.5654 | 7.3537 | 0.0166 | 1.1576 | 0.0215 | 1.1791 | 0.3101 | 0.0198 | 0.3299 | 0.0000 | 1,224.656 2 | 1,224.656 2 | 0.0498 | 0.0000 | 1,225.701 4 |

4.2 Trip Summary Information

| | Avei | age Daily Trip Ra | ite | Unmitigated | Mitigated |
|----------------------------------|----------|-------------------|----------|-------------|------------|
| Land Use | Weekday | Saturday | Sunday | Annual VMT | Annual VMT |
| Apartments Mid Rise | 924.48 | 924.48 | 924.48 | 2,372,316 | 2,372,316 |
| Parking Lot | 0.00 | 0.00 | 0.00 | | |
| Regional Shopping Center | 168.66 | 168.66 | 168.66 | 235,669 | 235,669 |
| Single Family Housing | 195.60 | 195.60 | 195.60 | 501,931 | 501,931 |
| Unenclosed Parking with Elevator | 0.00 | 0.00 | 0.00 | | |
| Total | 1,288.74 | 1,288.74 | 1,288.74 | 3,109,917 | 3,109,917 |

4.3 Trip Type Information

| | | Miles | | | Trip % | | | Trip Purpos | е% |
|--------------------------|------------|------------|-------------|------------|------------|-------------|---------|-------------|---------|
| Land Use | H-W or C-W | H-S or C-C | H-O or C-NW | H-W or C-W | H-S or C-C | H-O or C-NW | Primary | Diverted | Pass-by |
| Apartments Mid Rise | 10.00 | 5.00 | 6.50 | 46.50 | 12.50 | 41.00 | 86 | 11 | 3 |
| Parking Lot | 10.00 | 5.00 | 6.50 | 0.00 | 0.00 | 0.00 | 0 | 0 | 0 |
| Regional Shopping Center | 10.00 | 5.00 | 6.50 | 16.30 | 64.70 | 19.00 | 54 | 35 | 11 |
| Single Family Housing | 10.00 | 5.00 | 6.50 | 46.50 | 12.50 | 41.00 | 86 | 11 | 3 |
| Unenclosed Parking with | 10.00 | 5.00 | 6.50 | 0.00 | 0.00 | 0.00 | 0 | 0 | 0 |

| LDA | LDT1 | LDT2 | MDV | LHD1 | LHD2 | MHD | HHD | OBUS | UBUS | MCY | SBUS | MH |
|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
| 0.504263 | 0.068212 | 0.178684 | 0.146863 | 0.044671 | 0.006294 | 0.020946 | 0.016568 | 0.002299 | 0.002275 | 0.006187 | 0.000564 | 0.002174 |

5.0 Energy Detail

Historical Energy Use: N

5.1 Mitigation Measures Energy

Exceed Title 24

| | ROG | NOx | со | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|----------------------------|--------|--------|--------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|-----------------|----------|
| Category | | | | | ton | s/yr | | | | | | | МТ | /yr | | |
| Electricity Mitigated | | | | | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | 336.5215 | 336.5215 | 0.0165 | 3.4200e- 003 | 337.9290 |
| Electricity Unmitigated | n | | | | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | 343.9118 | 343.9118 | 0.0169 | 3.5000e- 003 | 345.3502 |
| NaturalGas Mitigated | 0.0126 | 0.1076 | 0.0464 | 6.9000e- 004 | | 8.7000e- 003 | 8.7000e- 003 | | 8.7000e- 003 | 8.7000e- 003 | 0.0000 | 124.5701 | 124.5701 | 2.3900e- 003 | 2.2800e- 003 | 125.3283 |
| NaturalGas Unmitigated | 0.0159 | 0.1356 | 0.0584 | 8.6000e- 004 | | 0.0110 | 0.0110 | | 0.0110 | 0.0110 | 0.0000 | 156.9281 | 156.9281 | 3.0100e- 003 | 2.8800e- 003 | 157.8831 |

5.2 Energy by Land Use - NaturalGas

<u>Unmitigated</u>

| | NaturalGa s Use | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|--|--------------------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|-----------------|----------|
| Land Use | kBTU/yr | | | | | ton | s/yr | | | | | | | МТ | /yr | | |
| Apartments Mid Rise | 2.13518e +006 | 0.0115 | 0.0984 | 0.0419 | 6.3000e- 004 | | 7.9500e- 003 | 7.9500e- 003 | | 7.9500e- 003 | 7.9500e- 003 | 0.0000 | 113.9413 | 113.9413 | 2.1800e- 003 | 2.0900e- 003 | 114.6347 |
| Parking Lot | 0 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Regional Shopping Center | 33900 | 1.8000e- 004 | 1.6600e- 003 | 1.4000e- 003 | 1.0000e- 005 | | 1.3000e- 004 | 1.3000e- 004 | | 1.3000e- 004 | 1.3000e- 004 | 0.0000 | 1.8090 | 1.8090 | 3.0000e- 005 | 3.0000e- 005 | 1.8200 |
| Single Family Housing | 771642 | 4.1600e- 003 | 0.0356 | 0.0151 | 2.3000e- 004 | | 2.8700e- 003 | 2.8700e- 003 | | 2.8700e- 003 | 2.8700e- 003 | 0.0000 | 41.1778 | 41.1778 | 7.9000e- 004 | 7.5000e- 004 | 41.4284 |
| Unenclosed Parking with Elevator | 0 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Total | | 0.0159 | 0.1356 | 0.0584 | 8.7000e- 004 | | 0.0110 | 0.0110 | | 0.0110 | 0.0110 | 0.0000 | 156.9281 | 156.9281 | 3.0000e- 003 | 2.8700e- 003 | 157.8831 |

5.2 Energy by Land Use - NaturalGas

Mitigated

| | NaturalGa s Use | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|--|--------------------|-----------------|-----------------|-----------------|-----------------|------------------|-----------------|-----------------|-------------------|------------------|-----------------|----------|-----------|-----------|-----------------|-----------------|----------|
| Land Use | kBTU/yr | | | | | ton | s/yr | | | | | | | MT | /yr | | |
| Parking Lot | 0 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 1 1 1 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Regional Shopping Center | 26820 | 1.4000e- 004 | 1.3100e- 003 | 1.1000e- 003 | 1.0000e- 005 | | 1.0000e- 004 | 1.0000e- 004 | | 1.0000e- 004 | 1.0000e- 004 | 0.0000 | 1.4312 | 1.4312 | 3.0000e- 005 | 3.0000e- 005 | 1.4399 |
| Single Family Housing | 614334 | 3.3100e- 003 | 0.0283 | 0.0121 | 1.8000e- 004 | | 2.2900e- 003 | 2.2900e- 003 | | 2.2900e- 003 | 2.2900e- 003 | 0.0000 | 32.7832 | 32.7832 | 6.3000e- 004 | 6.0000e- 004 | 32.9827 |
| Unenclosed Parking with Elevator | 0 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Apartments Mid Rise | 1.6932e +006 | 9.1300e- 003 | 0.0780 | 0.0332 | 5.0000e- 004 | | 6.3100e- 003 | 6.3100e- 003 | | 6.3100e- 003 | 6.3100e- 003 | 0.0000 | 90.3557 | 90.3557 | 1.7300e- 003 | 1.6600e- 003 | 90.9056 |
| Total | | 0.0126 | 0.1076 | 0.0464 | 6.9000e- 004 | | 8.7000e- 003 | 8.7000e- 003 | | 8.7000e- 003 | 8.7000e- 003 | 0.0000 | 124.5701 | 124.5701 | 2.3900e- 003 | 2.2900e- 003 | 125.3283 |

5.3 Energy by Land Use - Electricity

<u>Unmitigated</u>

| | Electricity Use | Total CO2 | CH4 | N2O | CO2e |
|--|--------------------|-----------|-----------------|-----------------|----------|
| Land Use | kWh/yr | | МТ | 7/yr | |
| Apartments Mid Rise | 774335 | 207.3362 | 0.0102 | 2.1100e- 003 | 208.2033 |
| Parking Lot | 33792 | 9.0482 | 4.4000e- 004 | 9.0000e- 005 | 9.0860 |
| Regional Shopping Center | 77820 | 20.8371 | 1.0200e- 003 | 2.1000e- 004 | 20.9242 |
| Single Family Housing | 178495 | 47.7939 | 2.3500e- 003 | 4.9000e- 004 | 47.9938 |
| Unenclosed Parking with Elevator | 219960 | 58.8965 | 2.8900e- 003 | 6.0000e- 004 | 59.1429 |
| Total | | 343.9118 | 0.0169 | 3.5000e- 003 | 345.3502 |

5.3 Energy by Land Use - Electricity <u>Mitigated</u>

Total CO2 CH4 CO2e Electricity N2O Use Land Use kWh/yr MT/yr 2.0600e-003 203.5644 Apartments Mid 757083 202.7166 9.9600e-Rise 003 33792 9.0482 4.4000e-9.0000e-9.0860 Parking Lot 004 005 71850 19.2386 2.0000e-19.3190 9.5000e-Regional . 004 Shopping Center 004 Single Family 174117 1 46.6217 2.2900e-4.7000e-46.8167 Housing 003 004 219960 58.8965 6.0000e-59.1429 Unenclosed ÷. 2.8900e-. Parking with 004 003 337.9290 336.5215 3.4200e-Total 0.0165 003

6.0 Area Detail

6.1 Mitigation Measures Area

Use only Natural Gas Hearths

Use Low VOC Cleaning Supplies

| | ROG | NOx | со | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|-------------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|-----------------|--------|--------|
| Category | | | | | ton | s/yr | | | | | | | ΜT | Г/yr | | |
| Mitigated | 1.6682 | 0.0287 | 2.4741 | 1.3000e- 004 | | 0.0135 | 0.0135 | | 0.0135 | 0.0135 | 0.0000 | 4.0137 | 4.0137 | 3.9900e- 003 | 0.0000 | 4.0974 |
| Unmitigated | 1.7791 | 0.0287 | 2.4741 | 1.3000e- 004 | | 0.0135 | 0.0135 | | 0.0135 | 0.0135 | 0.0000 | 4.0137 | 4.0137 | 3.9900e- 003 | 0.0000 | 4.0974 |

6.2 Area by SubCategory

<u>Unmitigated</u>

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|--------------------------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|-----------------|--------|--------|
| SubCategory | | | | | ton | s/yr | | | | | | | МТ | /yr | | |
| Architectural Coating | 0.2201 | | | | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Consumer Products | 1.4825 | | | | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Hearth | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Landscaping | 0.0764 | 0.0287 | 2.4741 | 1.3000e- 004 | | 0.0135 | 0.0135 | | 0.0135 | 0.0135 | 0.0000 | 4.0137 | 4.0137 | 3.9900e- 003 | 0.0000 | 4.0974 |
| Total | 1.7791 | 0.0287 | 2.4741 | 1.3000e- 004 | | 0.0135 | 0.0135 | | 0.0135 | 0.0135 | 0.0000 | 4.0137 | 4.0137 | 3.9900e- 003 | 0.0000 | 4.0974 |

6.2 Area by SubCategory

Mitigated

| | ROG | NOx | CO | SO2 | Fugitive PM10 | Exhaust PM10 | PM10 Total | Fugitive PM2.5 | Exhaust PM2.5 | PM2.5 Total | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|--------------------------|--------|--------|--------|-----------------|------------------|-----------------|---------------|-------------------|------------------|----------------|----------|-----------|-----------|-----------------|--------|--------|
| SubCategory | | | | | ton | s/yr | | | | | | | МТ | ī/yr | | |
| Architectural Coating | 0.2201 | | | | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Consumer Products | 1.3717 | | | | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Hearth | 0.0000 | 0.0000 | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Landscaping | 0.0764 | 0.0287 | 2.4741 | 1.3000e- 004 | | 0.0135 | 0.0135 | | 0.0135 | 0.0135 | 0.0000 | 4.0137 | 4.0137 | 3.9900e- 003 | 0.0000 | 4.0974 |
| Total | 1.6682 | 0.0287 | 2.4741 | 1.3000e- 004 | | 0.0135 | 0.0135 | | 0.0135 | 0.0135 | 0.0000 | 4.0137 | 4.0137 | 3.9900e- 003 | 0.0000 | 4.0974 |

7.0 Water Detail

7.1 Mitigation Measures Water

| | Total CO2 | CH4 | N2O | CO2e | |
|-------------|-----------|--------|--------|---------|--|
| Category | MT/yr | | | | |
| | 36.3414 | 0.0210 | 0.0126 | 40.6886 | |
| Chiningutou | 36.3414 | 0.0209 | 0.0126 | 40.6823 | |

7.2 Water by Land Use

<u>Unmitigated</u>

| | Indoor/Out door Use | Total CO2 | CH4 | N2O | CO2e | |
|-----------------------------|------------------------|-----------|-----------------|-----------------|---------|--|
| Land Use | Mgal | MT/yr | | | | |
| Apartments Mid Rise | 13.943 / 8.79013 | 31.7727 | 0.0183 | 0.0110 | 35.5671 | |
| Parking Lot | 0/0 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | |
| Regional Shopping Center | 0.444435/ 0.272396 | 1.0055 | 5.8000e- 004 | 3.5000e- 004 | 1.1264 | |
| Single Family Housing | 1.5637 / 0.985809 | 3.5633 | 2.0500e- 003 | 1.2300e- 003 | 3.9888 | |
| Unenclosed Parking with | 0/0 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | |
| Total | | 36.3414 | 0.0209 | 0.0126 | 40.6823 | |

7.2 Water by Land Use

Mitigated

| | Indoor/Out door Use | Total CO2 | CH4 | N2O | CO2e |
|--|------------------------|-----------|-----------------|-----------------|---------|
| Land Use | Mgal | MT/yr | | | |
| Apartments Mid Rise | 13.943 / 8.79013 | 31.7727 | 0.0184 | 0.0110 | 35.5726 |
| Parking Lot | 0/0 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Regional Shopping Center | 0.444435/ 0.272396 | | 5.8000e- 004 | 3.5000e- 004 | 1.1266 |
| Single Family Housing | 1.5637 / 0.985809 | 3.5633 | 2.0600e- 003 | 1.2400e- 003 | 3.9895 |
| Unenclosed Parking with Elevator | 0/0 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Total | | 36.3414 | 0.0210 | 0.0126 | 40.6886 |

8.0 Waste Detail

8.1 Mitigation Measures Waste

Category/Year

| | Total CO2 | CH4 | N2O | CO2e | | |
|-------------|-----------|--------|--------|---------|--|--|
| | MT/yr | | | | | |
| Willigutou | 25.9382 | 1.5329 | 0.0000 | 58.1291 | | |
| Grinnigutou | 25.9382 | 1.5329 | 0.0000 | 58.1291 | | |

8.2 Waste by Land Use

<u>Unmitigated</u>

| | Waste Disposed | Total CO2 | CH4 | N2O | CO2e |
|--|-------------------|-----------|--------|--------|---------|
| Land Use | tons | MT/yr | | | |
| Apartments Mid Rise | 98.44 | 19.9824 | 1.1809 | 0.0000 | 44.7819 |
| Parking Lot | 0 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Regional Shopping Center | 6.3 | 1.2788 | 0.0756 | 0.0000 | 2.8660 |
| Single Family Housing | 23.04 | 4.6769 | 0.2764 | 0.0000 | 10.4813 |
| Unenclosed Parking with Elevator | 0 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Total | | 25.9382 | 1.5329 | 0.0000 | 58.1291 |

8.2 Waste by Land Use

Mitigated

| | Waste Disposed | Total CO2 | CH4 | N2O | CO2e |
|-----------------------------|-------------------|-----------|--------|--------|---------|
| Land Use | tons | | МТ | /yr | |
| Apartments Mid Rise | 98.44 | 19.9824 | 1.1809 | 0.0000 | 44.7819 |
| Parking Lot | 0 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Regional Shopping Center | 6.3 | 1.2788 | 0.0756 | 0.0000 | 2.8660 |
| Single Family Housing | 23.04 | 4.6769 | 0.2764 | 0.0000 | 10.4813 |
| Unenclosed Parking with | 0 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| Total | | 25.9382 | 1.5329 | 0.0000 | 58.1291 |

9.0 Operational Offroad

| Equipment Type | Number | Hours/Day | Days/Year | Horse Power | Load Factor | Fuel Type |
|----------------|--------|-----------|-----------|-------------|-------------|-----------|

10.0 Vegetation

Stockton & T

Sacramento County, Mitigation Report

Construction Mitigation Summary

| Phase | ROG | NOx | со | SO2 | Exhaust PM10 | Exhaust PM2.5 | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|-----------------------|------|------|------|------|-----------------|------------------|----------|--------------|-----------|------|------|------|
| Percent Reduction | | | | | | | | | | | | |
| Architectural Coating | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Building Construction | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Demolition | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Grading | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Paving | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Site Preparation | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

OFFROAD Equipment Mitigation

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Date: 1/21/2015 4:41 PM

| Equipment Type | Fuel Type | Tier | Number Mitigated | Total Number of Equipment | DPF | Oxidation Catalyst |
|---------------------------|-----------|-----------|------------------|---------------------------|-----------|--------------------|
| Air Compressors | Diesel | No Change | 0 | 1 | No Change | 0.00 |
| Cement and Mortar Mixers | Diesel | No Change | 0 | 2 | No Change | 0.00 |
| Concrete/Industrial Saws | Diesel | No Change | 0 | 1 | No Change | 0.00 |
| Cranes | Diesel | No Change | 0 | 1 | No Change | 0.00 |
| Excavators | Diesel | No Change | 0 | 4 | No Change | 0.00 |
| Forklifts | Diesel | No Change | 0 | 3 | No Change | 0.00 |
| Generator Sets | Diesel | No Change | 0 | 1 | No Change | 0.00 |
| Graders | Diesel | No Change | 0 | 1 | No Change | 0.00 |
| Pavers | Diesel | No Change | 0 | 1 | No Change | 0.00 |
| Paving Equipment | Diesel | No Change | 0 | 2 | No Change | 0.00 |
| Rollers | Diesel | No Change | 0 | 2 | No Change | 0.00 |
| Rubber Tired Dozers | Diesel | No Change | 0 | 6 | No Change | 0.00 |
| Tractors/Loaders/Backhoes | Diesel | No Change | 0 | 11 | No Change | 0.00 |
| Welders | Diesel | No Change | 0 | 1 | No Change | 0.00 |

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| Equipment Type | ROG | NOx | со | SO2 | Exhaust PM10 | Exhaust PM2.5 | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e | | |
|-------------------------------|--------------|--------------|-------------------|--------------|--------------|---------------|-------------------|--------------|--------------|--------------|--------------|--------------|--|--|
| | | Ur | mitigated tons/yr | | | | Unmitigated mt/yr | | | | | | | |
| Air Compressors | 5.86800E-002 | 3.84580E-001 | 3.25430E-001 | 5.20000E-004 | 3.07000E-002 | 3.07000E-002 | 0.00000E+000 | 4.44266E+001 | 4.44266E+001 | 4.77000E-003 | 0.00000E+000 | 4.45267E+001 | | |
| Cement and Mortar Mixers | 4.90000E-004 | 3.05000E-003 | 2.54000E-003 | 1.00000E-005 | 1.20000E-004 | 1.20000E-004 | 0.00000E+000 | 3.78080E-001 | 3.78080E-001 | 4.00000E-005 | 0.00000E+000 | 3.78900E-001 | | |
| Concrete/Industria I Saws | 1.42200E-002 | 1.01680E-001 | 8.30500E-002 | 1.40000E-004 | 7.64000E-003 | 7.64000E-003 | 0.00000E+000 | 1.18285E+001 | 1.18285E+001 | 1.14000E-003 | 0.00000E+000 | 1.18525E+001 | | |
| Cranes | 1.00650E-001 | 1.19460E+000 | 4.25960E-001 | 8.60000E-004 | 5.34400E-002 | 4.91700E-002 | 0.00000E+000 | 7.99622E+001 | 7.99622E+001 | 2.44300E-002 | 0.00000E+000 | 8.04752E+001 | | |
| Excavators | 2.87300E-002 | 3.27880E-001 | 2.53700E-001 | 3.90000E-004 | 1.61300E-002 | 1.48400E-002 | 0.00000E+000 | 3.69169E+001 | 3.69169E+001 | 1.11400E-002 | 0.00000E+000 | 3.71508E+001 | | |
| Forklifts | 1.11420E-001 | 9.63880E-001 | 6.53010E-001 | 8.00000E-004 | 7.97000E-002 | 7.33300E-002 | 0.00000E+000 | 7.42161E+001 | 7.42161E+001 | 2.26700E-002 | 0.00000E+000 | 7.46922E+001 | | |
| Generator Sets | 1.01500E-001 | 7.89110E-001 | 6.57590E-001 | 1.14000E-003 | 5.35300E-002 | 5.35300E-002 | 0.00000E+000 | 9.83461E+001 | 9.83461E+001 | 8.16000E-003 | 0.00000E+000 | 9.85175E+001 | | |
| Graders | 8.15000E-003 | 8.30400E-002 | 3.94200E-002 | 5.00000E-005 | 4.67000E-003 | 4.29000E-003 | 0.00000E+000 | 4.71306E+000 | 4.71306E+000 | 1.42000E-003 | 0.00000E+000 | 4.74291E+000 | | |
| Pavers | 2.21000E-003 | 2.48200E-002 | 1.56900E-002 | 2.00000E-005 | 1.23000E-003 | 1.13000E-003 | 0.00000E+000 | 2.34022E+000 | 2.34022E+000 | 7.10000E-004 | 0.00000E+000 | 2.35504E+000 | | |
| Paving Equipment | 2.53000E-003 | 2.94300E-002 | 2.09800E-002 | 3.00000E-005 | 1.46000E-003 | 1.34000E-003 | 0.00000E+000 | 3.11858E+000 | 3.11858E+000 | 9.40000E-004 | 0.00000E+000 | 3.13833E+000 | | |
| Rollers | 2.78000E-003 | 2.56800E-002 | 1.66100E-002 | 2.00000E-005 | 1.89000E-003 | 1.74000E-003 | 0.00000E+000 | 2.03930E+000 | 2.03930E+000 | 6.20000E-004 | 0.00000E+000 | 2.05222E+000 | | |
| Rubber Tired Dozers | 7.36800E-002 | 8.25310E-001 | 6.23850E-001 | 5.30000E-004 | 3.84000E-002 | 3.53300E-002 | 0.00000E+000 | 4.98446E+001 | 4.98446E+001 | 1.50300E-002 | 0.00000E+000 | 5.01603E+001 | | |
| Tractors/Loaders/ Backhoes | 1.59820E-001 | 1.53423E+000 | 1.18976E+000 | 1.54000E-003 | 1.16040E-001 | 1.06750E-001 | 0.00000E+000 | 1.43898E+002 | 1.43898E+002 | 4.39100E-002 | 0.00000E+000 | 1.44820E+002 | | |
| Welders | 8.91900E-002 | 3.04920E-001 | 3.34700E-001 | 4.40000E-004 | 2.27000E-002 | 2.27000E-002 | 0.00000E+000 | 3.27504E+001 | 3.27504E+001 | 7.25000E-003 | 0.00000E+000 | 3.29027E+001 | | |

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| Equipment Type | ROG | NOx | со | SO2 | Exhaust BM10 | Exhaust PM2.5 | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|-------------------------------|--------------|--------------|------------------|--------------|----------------|-----------------|--------------|--------------|--------------|--------------|--------------|--------------|
| Equipment Type | ROG | _ | itigated tons/yr | 302 | EXHAUST FIVITU | EXHAUST PIVI2.5 | BI0- CO2 | INDIO- CO2 | | ed mt/yr | IN2O | COZE |
| Air Compressors | 5 86800E-002 | | | 5.20000E-004 | 3 07000E-002 | 3 07000E-002 | 0.00000E+000 | 4 44266F+001 | | | 0.00000E+000 | 4 45267E+001 |
| | | | | | | | | , | | | | |
| Cement and Mortar Mixers | 4.90000E-004 | 3.05000E-003 | 2.54000E-003 | 1.00000E-005 | 1.20000E-004 | 1.20000E-004 | 0.00000E+000 | 3.78080E-001 | 3.78080E-001 | 4.00000E-005 | 0.00000E+000 | 3.78900E-001 |
| Concrete/Industrial Saws | 1.42200E-002 | 1.01680E-001 | 8.30500E-002 | 1.40000E-004 | 7.64000E-003 | 7.64000E-003 | 0.00000E+000 | 1.18285E+001 | 1.18285E+001 | 1.14000E-003 | 0.00000E+000 | 1.18525E+001 |
| Cranes | 1.00650E-001 | 1.19460E+000 | 4.25960E-001 | 8.60000E-004 | 5.34400E-002 | 4.91700E-002 | 0.00000E+000 | 7.99621E+001 | 7.99621E+001 | 2.44300E-002 | 0.00000E+000 | 8.04751E+001 |
| Excavators | 2.87300E-002 | 3.27880E-001 | 2.53700E-001 | 3.90000E-004 | 1.61300E-002 | 1.48400E-002 | 0.00000E+000 | 3.69169E+001 | 3.69169E+001 | 1.11400E-002 | 0.00000E+000 | 3.71507E+001 |
| Forklifts | 1.11420E-001 | 9.63880E-001 | 6.53010E-001 | 8.00000E-004 | 7.97000E-002 | 7.33300E-002 | 0.00000E+000 | 7.42160E+001 | 7.42160E+001 | 2.26700E-002 | 0.00000E+000 | 7.46921E+001 |
| Generator Sets | 1.01500E-001 | 7.89110E-001 | 6.57590E-001 | 1.14000E-003 | 5.35300E-002 | 5.35300E-002 | 0.00000E+000 | 9.83460E+001 | 9.83460E+001 | 8.16000E-003 | 0.00000E+000 | 9.85174E+001 |
| Graders | 8.15000E-003 | 8.30400E-002 | 3.94200E-002 | 5.00000E-005 | 4.67000E-003 | 4.29000E-003 | 0.00000E+000 | 4.71305E+000 | 4.71305E+000 | 1.42000E-003 | 0.00000E+000 | 4.74290E+000 |
| Pavers | 2.21000E-003 | 2.48200E-002 | 1.56900E-002 | 2.00000E-005 | 1.23000E-003 | 1.13000E-003 | 0.00000E+000 | 2.34021E+000 | 2.34021E+000 | 7.10000E-004 | 0.00000E+000 | 2.35504E+000 |
| Paving Equipment | 2.53000E-003 | 2.94300E-002 | 2.09800E-002 | 3.00000E-005 | 1.46000E-003 | 1.34000E-003 | 0.00000E+000 | 3.11857E+000 | 3.11857E+000 | 9.40000E-004 | 0.00000E+000 | 3.13833E+000 |
| Rollers | 2.78000E-003 | 2.56800E-002 | 1.66100E-002 | 2.00000E-005 | 1.89000E-003 | 1.74000E-003 | 0.00000E+000 | 2.03930E+000 | 2.03930E+000 | 6.20000E-004 | 0.00000E+000 | 2.05221E+000 |
| Rubber Tired Dozers | 7.36800E-002 | 8.25310E-001 | 6.23850E-001 | 5.30000E-004 | 3.84000E-002 | 3.53300E-002 | 0.00000E+000 | 4.98445E+001 | 4.98445E+001 | 1.50300E-002 | 0.00000E+000 | 5.01602E+001 |
| Tractors/Loaders/Ba ckhoes | 1.59820E-001 | 1.53422E+000 | 1.18976E+000 | 1.54000E-003 | 1.16030E-001 | 1.06750E-001 | 0.00000E+000 | 1.43898E+002 | 1.43898E+002 | 4.39100E-002 | 0.00000E+000 | 1.44820E+002 |
| Welders | 8.91900E-002 | 3.04920E-001 | 3.34700E-001 | 4.40000E-004 | 2.27000E-002 | 2.27000E-002 | 0.00000E+000 | 3.27504E+001 | 3.27504E+001 | 7.25000E-003 | 0.00000E+000 | 3.29027E+001 |

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| Equipment Type | ROG | NOx | СО | SO2 | Exhaust PM10 | Exhaust PM2.5 | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|-------------------------------|--------------|--------------|--------------|--------------|--------------|-----------------|--------------|--------------|--------------|--------------|--------------|--------------|
| | | | | | Pe | rcent Reduction | | | | | | |
| Air Compressors | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 1.12545E-006 | 1.12545E-006 | 0.00000E+000 | 0.00000E+000 | 1.12292E-006 |
| Cement and Mortar Mixers | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 |
| Concrete/Industrial Saws | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 8.45419E-007 | 8.45419E-007 | 0.00000E+000 | 0.00000E+000 | 8.43704E-007 |
| Cranes | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 1.25059E-006 | 1.25059E-006 | 0.00000E+000 | 0.00000E+000 | 1.24262E-006 |
| Excavators | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 1.08351E-006 | 1.08351E-006 | 0.00000E+000 | 0.00000E+000 | 1.34587E-006 |
| Forklifts | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 1.21268E-006 | 1.21268E-006 | 0.00000E+000 | 0.00000E+000 | 1.20495E-006 |
| Generator Sets | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 1.22018E-006 | 1.22018E-006 | 0.00000E+000 | 0.00000E+000 | 1.21806E-006 |
| Graders | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 2.12176E-006 | 2.12176E-006 | 0.00000E+000 | 0.00000E+000 | 2.10841E-006 |
| Pavers | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 4.27310E-006 | 4.27310E-006 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 |
| Paving Equipment | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 3.20659E-006 | 3.20659E-006 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 |
| Rollers | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 4.87277E-006 |
| Rubber Tired Dozers | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 1.20374E-006 | 1.20374E-006 | 0.00000E+000 | 0.00000E+000 | 1.19617E-006 |
| Tractors/Loaders/Ba ckhoes | 0.00000E+000 | 6.51793E-006 | 0.00000E+000 | 0.00000E+000 | 8.61772E-005 | 0.00000E+000 | 0.00000E+000 | 1.18139E-006 | 1.18139E-006 | 0.00000E+000 | 0.00000E+000 | 1.24292E-006 |
| Welders | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 0.00000E+000 | 1.22136E-006 | 1.22136E-006 | 0.00000E+000 | 0.00000E+000 | 1.21570E-006 |

Fugitive Dust Mitigation

| | Yes/No | Mitigation Measure | Mitigation Input | Mitigation Input | Mitigation Input |
|---|--------|---|------------------|------------------|------------------------|
| Γ | | Soil Stabilizer for unpaved Roads | PM10 Reduction | PM2.5 Reduction | |
| ľ | | Replace Ground Cover of Area Disturbed | ····· | PM2.5 Reduction | |
| | No | Water Exposed Area | PM10 Reduction | PM2.5 Reduction | Frequency (per day) |

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|-------|-------------------------------------|-------------------------|--------------------|--------|------------------------|-------------------------|--|--|--|
| ١ | No | Unpaved Road Mitigation | Moisture Content % | | Vehicle Speed (mph) | | | | |
| ١ | No | Clean Paved Road | % PM Reduction | 0.00 | | | | | |

| | | Unmi | itigated | Mit | tigated | Percent R | eduction |
|-----------------------|---------------|------------|----------|------|---------|-----------|----------|
| Phase | Source | PM10 PM2.5 | | PM10 | PM2.5 | PM10 | PM2.5 |
| Architectural Coating | Fugitive Dust | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Architectural Coating | Roads | 0.05 | 0.01 | 0.05 | 0.01 | 0.00 | 0.00 |
| Building Construction | Fugitive Dust | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Building Construction | Roads | 0.32 | 0.09 | 0.32 | 0.09 | 0.00 | 0.00 |
| Demolition | Fugitive Dust | 0.06 | 0.01 | 0.06 | 0.01 | 0.00 | 0.00 |
| Demolition | Roads | 0.01 | 0.00 | 0.01 | 0.00 | 0.00 | 0.00 |
| Grading | Fugitive Dust | 0.05 | 0.03 | 0.05 | 0.03 | 0.00 | 0.00 |
| Grading | Roads | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Paving | Fugitive Dust | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Paving | Roads | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Site Preparation | Fugitive Dust | 0.05 | 0.02 | 0.05 | 0.02 | 0.00 | 0.00 |
| Site Preparation | Roads | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

Operational Percent Reduction Summary

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| Category | ROG | NOx | со | SO2 | Exhaust PM10 | Exhaust PM2.5 | Bio- CO2 | NBio- CO2 | Total CO2 | CH4 | N2O | CO2e |
|-----------------------|-------|-------|-------|-------|-----------------|------------------|----------|--------------|-----------|-------|-------|-------|
| Percent Reduction | | | | | | | | | | | | |
| Architectural Coating | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Consumer Products | 7.48 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Electricity | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 2.15 | 2.15 | 2.13 | 2.29 | 2.15 |
| Hearth | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Landscaping | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Mobile | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Natural Gas | 20.63 | 20.63 | 20.63 | 20.69 | 20.55 | 20.55 | 0.00 | 20.62 | 20.62 | 20.33 | 20.21 | 20.62 |
| Water Indoor | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | -0.33 | -0.16 | -0.02 |
| Water Outdoor | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

Operational Mobile Mitigation

Project Setting:

| Mitigation | Category | Measure | % Reduction | Input Value 1 | Input Value 2 | Input Value |
|------------|----------|-------------------------------------|-------------|---------------|---------------|-------------|
| No | Land Use | Increase Density | 0.00 | 8 | | |
| No | Land Use | Increase Diversity | 0.17 | 0.43 | | |
| No | Land Use | Improve Walkability Design | 0.00 | | | |
| No | Land Use | Improve Destination Accessibility | 0.00 | | | |
| No | Land Use | Increase Transit Accessibility | 0.25 | | | |
| No | Land Use | Integrate Below Market Rate Housing | 0.00 | | | |
| [| Land Use | Land Use SubTotal | 0.00 | | | |

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|-------------------------------------|--|---|------|-------------------------|--|
| No | Neighborhood Enhancements | Improve Pedestrian Network | | | |
| No | Neighborhood Enhancements | Provide Traffic Calming Measures | | | |
| No | Neighborhood Enhancements | Implement NEV Network | 0.00 | | |
| | Neighborhood Enhancements | Neighborhood Enhancements Subtotal | 0.00 | | |
| No | Parking Policy Pricing | Limit Parking Supply | 0.00 | | |
| No | Parking Policy Pricing | Unbundle Parking Costs | 0.00 | | |
| No | Parking Policy Pricing | On-street Market Pricing | 0.00 | | |
| | Parking Policy Pricing | Parking Policy Pricing Subtotal | 0.00 | | |
| No | Transit Improvements | Provide BRT System | 0.00 | | |
| No | Transit Improvements | Expand Transit Network | 0.00 | | |
| No | Transit Improvements | Increase Transit Frequency | 0.00 | | |
| | Transit Improvements | Transit Improvements Subtotal | 0.00 | | |
| | · · · / · · · · · · · · · · · · · · · · · · · | Land Use and Site Enhancement Subtotal | 0.00 | | |
| No | Commute | Implement Trip Reduction Program | ++ | | |
| No | Commute | Transit Subsidy | ++ | | |
| No | Commute | Implement Employee Parking "Cash Out" | | | |
| No | Commute | Workplace Parking Charge | | | |
| No | Commute | Encourage Telecommuting and Alternative Work Schedules | 0.00 | | |
| No | Commute | Market Commute Trip Reduction Option | 0.00 | | |
| No | Commute | Employee Vanpool/Shuttle | 0.00 | 2.00 | |
| No | Commute | Provide Ride Sharing Program | | | |
| 1 | Commute | Commute Subtotal | 0.00 | | |

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|---|-------------------------------------|-------------|------------------------------|------|-------------------------|--|--|
| ſ | No | School Trip | Implement School Bus Program | 0.00 | | | |
| | | | Total VMT Reduction | 0.00 | | | |

Area Mitigation

| Measure Implemented | Mitigation Measure | Input Value |
|---------------------|--|-------------|
| Yes | Only Natural Gas Hearth | |
| No | No Hearth | |
| Yes | Use Low VOC Cleaning Supplies | |
| No | Use Low VOC Paint (Residential Interior) | 100.00 |
| No | Use Low VOC Paint (Residential Exterior) | 100.00 |
| No | Use Low VOC Paint (Non-residential Interior) | 150.00 |
| No | Use Low VOC Paint (Non-residential Exterior) | 150.00 |
| No | % Electric Lawnmower | 0.00 |
| No | % Electric Leafblower | 0.00 |
| No | % Electric Chainsaw | 0.00 |

Energy Mitigation Measures

| Measure Implemented | Mitigation Measure | Input Value 1 | Input Value 2 |
|---------------------|----------------------------------|---------------|---------------|
| Yes | Exceed Title 24 | 25.00 | |
| No | Install High Efficiency Lighting | | |
| No | On-site Renewable | | |

| Appliance Type | Land Use Subtype | % Improvement | |
|----------------|------------------|---------------|-------|
| ClothWasher | | | 30.00 |

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| DishWasher | | 15.00 |
|--------------|---|-------|
| Fan | | 50.00 |
| Refrigerator | r | 15.00 |

Water Mitigation Measures

| Measure Implemented | Mitigation Measure | Input Value 1 | Input Value 2 |
|---------------------|--|----------------|---------------|
| No | Apply Water Conservation on Strategy | | |
| No | Use Reclaimed Water | | |
| No | Use Grey Water | | |
| No | Install low-flow bathroom faucet | 32.00 | |
| No | Install low-flow Kitchen faucet | 18.00 | |
| No | Install low-flow Toilet | 20.00 | |
| No | Install low-flow Shower | 20.00 | |
| No | Turf Reduction | | |
| No | Use Water Efficient Irrigation Systems | 6.10 | |
| No | Water Efficient Landscape | # | |

Solid Waste Mitigation

| Mitigation Measures | Input Value |
|--|-------------|
| Institute Recycling and Composting Services Percent Reduction in Waste Disposed | |

APPENDIX B

DIESEL PARTICULATE MATTER RISK EVALUATION

SCS ENGINEERS

October 27, 2014 File No: 01214018.00

Mr. Rod Stinson Raney Planning and Management 1501 Sports Drive Sacramento, CA 95834

Subject: Diesel Particulate Matter Risk Evaluation for Proposed Stockton and T Residential Development, California

Dear Mr. Stinson:

SCS Engineers (SCS) hereby transmits this focused health risk screening conducted to evaluate health risks associated with planned development of residential property in Sacramento (Stockton and T Project or Project), bounded by Stockton Boulevard, 37th Street, S Street, 39th Street, and United States Highway 50 (US-50) (Site). This analysis evaluated the potential air quality impacts at the Site from vehicles on US-50.

To evaluate the potential health risks from traffic on US-50, SCS used the *Recommended Protocol for Evaluating the Location of Sensitive Land Uses Adjacent to Major Roadways* protocol (Roadway Protocol) developed by the Sacramento Metropolitan Air Quality Management District (SMAQMD).

BACKGROUND

Evergreen Management Company (Evergreen) has proposed the construction of a mixed use development at the Site. The Site is approximately two acres. Proposed use includes retail space, apartments, and single family homes. Due to the proximity of US-50, there is potential for excessive health risk impacts to residents at the Site resulting from exposure to vehicle exhaust from US-50. To evaluate the magnitude of the risk, SCS followed the Roadway Protocol. The purpose of the Roadway protocol is to allow developers, reviewers, and interested parties to evaluate health risk at a proposed development without requiring the use of complex air dispersion modeling. The Roadway Protocol is a stepwise process that indicates when dispersion modeling is required.

The Roadway Protocol establishes the cancer risk evaluation criterion of individual risk corresponding to a 70 percent reduction from the highest roadway risk in Sacramento County, as calculated on a hypothetical receptor located 50 feet from the nearest travel lane for the highest peak traffic volume in Sacramento County. This risk evaluation criterion is 276 in a million and was be used in this assessment.

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STEP 1 - TRAFFIC VOLUME

The first evaluation criterion in the Roadway Protocol is to determine the traffic count of major roadways near the Site. Project locations without a high traffic volume roadway within 500 feet require no further analysis. For the purposes of the Project, a high traffic volume roadway is a freeway with a traffic volume greater than 100,000 annual average daily trip count (AADT). US-50 is located near the Site and had an AADT of 205,000 in 2013 per Caltrans data, so the analysis must proceed to the next step.

STEP 2 - SCREENING TABLES

The second step of the Roadway Protocol screening uses more site specific characteristics to estimate the cancer risk. In the second step, the direction of the freeway, the trip count, and distance to the Site are considered. This information is used to look up the cancer risk from tables in the Roadway Protocol.

US-50 runs east-west near the Site, and the Site is located to the south of the freeway. Therefore, the bottom half of Table 1 from the Roadway Protocol should be consulted to evaluate cancer risk. The relevant section of *Table 1* is reproduced below.

| Table 1: 2011 Diesel PM Cancer Risk (Potential Incremental Cancer Chances per Million People) | | | | | | | | |
|--|----------|---|-----------|----------|--------|--------|---------|-----|
| N | orth and | d South | of an Ea | ast-Wes | t Road | way | | |
| PROJECTS NORT | H AND S | SOUTH (| OF AN E | AST-WE | ST ROA | DWAY \ | /ersion | 2.4 |
| | EMF | AC2007 | ' (Analy: | sis Year | 2011) | | | |
| Peak Hour Traffic | Recep | Receptor Distance from Edge of Nearest Travel Lane (feet) | | | | | | |
| (vehicle/hr) | 10 | 25 | 50 | 100 | 200 | 300 | 400 | 500 |
| 4,000 | 102 | 86 | 67 | 48 | 32 | 22 | 19 | 16 |
| 8,000 | 207 | 172 | 137 | 99 | 64 | 48 | 38 | 32 |
| 12,000 | 305 | 254 | 200 | 143 | 92 | 70 | 54 | 48 |
| 16,000 | 423 | 353 | 277 | 200 | 127 | 95 | 76 | 64 |
| 20,000 | 531 | 442 | 347 | 248 | 159 | 121 | 95 | 80 |
| 24,000 | 636 | 531 | 417 | 299 | 191 | 143 | 114 | 95 |

The cancer risk is then determined by looking up the peak hour traffic and the distance from the roadway to the Project site. The Project includes the proposed building locations, so it is appropriate and consistent with the Roadway Protocol to use the location of the nearest building rather than the property line to determine the distance. The distance between the roadway and the building nearest the roadway is 75 feet, and the peak hourly traffic on US-50 adjacent to the roadway is 18,000 vehicles per Caltrans data.

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The parameters of 18,000 AADT and 75 feet from the roadway are not shown in *Table 1*; however, the values can be interpolated from the risk values shown in *Table 1*. *Table 2* shows the values from Table 1 but with a column added for a site 75 feet from the roadway and a row added for 18,000 AADT.

| Table 2: 2011 Diesel PM Cancer Risk (Potential Incremental Cancer Chances per Million People) North and South of an East-West Roadway – With Interpolated Site Values | | | | | | | | | |
|---|--|----------|--------|--------|--------|--------|---------|---------|--------|
| | PROJECTS NORTH AND SOUTH OF AN EAST-WEST ROADWAY Version 2.4 EMFAC2007 (Analysis Year 2011) | | | | | | | | |
| Peak Hour Traffic | Recep | otor Dis | stance | from E | dge of | Neares | t Trave | el Lane | (feet) |
| (vehicle/hr) | 10 | 25 | 50 | 75 | 100 | 200 | 300 | 400 | 500 |
| 4,000 | 102 | 86 | 67 | 58 | 48 | 32 | 22 | 19 | 16 |
| 8,000 | 207 | 172 | 137 | 118 | 99 | 64 | 48 | 38 | 32 |
| 12,000 | 305 | 254 | 200 | 172 | 143 | 92 | 70 | 54 | 48 |
| 16,000 | 423 | 353 | 277 | 239 | 200 | 127 | 95 | 76 | 64 |
| 18,000 | 477 | 398 | 312 | 268 | 224 | 143 | 108 | 86 | 72 |
| 20,000 | 531 | 442 | 347 | 298 | 248 | 159 | 121 | 95 | 80 |
| 24,000 | 636 | 531 | 417 | 358 | 299 | 191 | 143 | 114 | 95 |

This linear interpolation yields a cancer risk of 268 in a million, which is less than the SMAQMD risk threshold of 276 in a million.

RISK SCREENING RESULTS

The cancer risk at the Site from US-50 is less than the SMAQMD Roadway Protocol threshold of 276; therefore, a site specific health risk assessment (HRA), including dispersion modeling, is not required. SCS notes the screening procedure in the Roadway Protocol is a conservative process and that dispersion modeling with updated emission factors is likely to produce a lower cancer risk for the Project than that the 268 in a million calculated in this evaluation.

SMAQMD notes in the Roadway Protocol that the threshold of 276 in a million is not characterized as an "acceptable" level of risk and that the Roadway Protocol does not establish which land use projects are acceptable or not. Rather, the Roadway Protocol is a stepwise process that indicates when dispersion modeling and a HRA is required.

Rod Stinson October 27, 2014 Page 4

CLOSING

Thank you for the opportunity to assist you with this evaluation. Please don't hesitate to call John Henkelman or Patrick Sullivan at 916-361-1297 if you have any questions or need any additional information.

Sincerely,

Supplie

Pater & Sullen

John Henkelman Senior Project Professional SCS ENGINEERS

Patrick S. Sullivan Senior Vice President SCS ENGINEERS

APPENDIX C

CAP CONSISTENCY REVIEW CHECKLIST

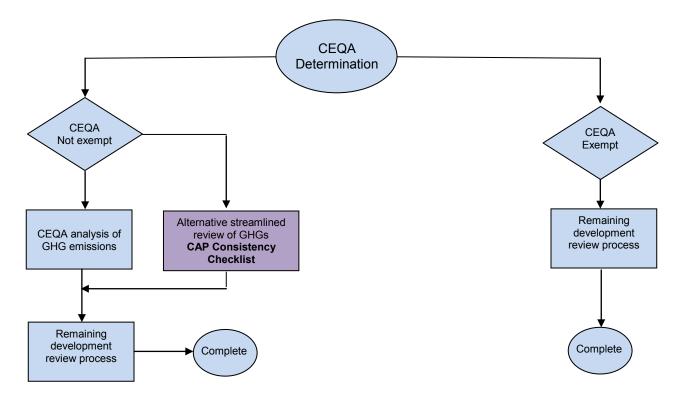


CLIMATE ACTION PLAN – CONSISTENCY REVIEW CHECKLIST

The purpose of the Climate Action Plan Consistency Review Checklist (CAP Consistency Review Checklist) is to provide a streamlined review process for proposed new development projects which are subject to discretionary review and trigger environmental review pursuant to the California Environmental Quality Act (CEQA)..

CEQA Guidelines require the analysis of greenhouse gas (GHG) emissions and potential climate change impacts from new development. The Sacramento Climate Action Plan qualifies under section 15183.5 of the CEQA Guidelines as a plan for the reduction of GHG emissions for use in cumulative impact analysis pertaining to development projects. This allows projects that demonstrate consistency with the CAP to be eligible for this streamlining procedure. Projects that demonstrate consistency with the CAP and the Sacramento 2030 General Plan may be able to answer "No additional significant environmental effect" in the City's initial study checklist. Projects that do not demonstrate consistency may, at the City's discretion, prepare a more comprehensive project-specific analysis of GHG emissions consistent with CEQA requirements. (See FAQ about the CAP Consistency Review Checklist for more details.)

The diagram below shows the context for the CAP Consistency Review Checklist within the planning review process framework.



Streamlined Review of GHG Emissions in Development Projects



CLIMATE ACTION PLAN – CONSISTENCY REVIEW CHECKLIST

Application Submittal Requirements

- 1. The CAP Consistency Review Checklist is required only for proposed new development projects which are subject to CEQA review (non-exempt projects)
- 2. If required, the CAP Consistency Review Checklist must be submitted in addition to the basic set of requirements set forth in the Universal Application and the Planning Application Submittal Matrix.
- 3. The applicant shall work with staff to meet the requirements of this checklist. These requirements will be reflected in the conditions of approval and/or mitigation measures.
- 4. All conditions of approval and mitigation measures from this checklist shall be shown on full-size sheets for building plan check submittals.

Application Information

| Project Number | |
|------------------|--|
| Address of Prop | erty: |
| Was a special of | nsultant retained to complete this checklist? \Box Yes \Box No. If yes, complete following |
| Consultant Nam | *: |
| Company: | |
| Phone: | E-Mail: |



CAP Consistency Checklist Form for Projects that are Not Exempt from CEQA

| | Checklist Item (Check the appropriate box, and provide explanation for your answer). | Yes | No* |
|----|--|-----------|--------|
| 1. | Is the proposed project substantially consistent with the City's over-all goals for land use and urban form, allowable floor area ratio (FAR) and/or density standards in the City's 2030 General Plan, as it currently exists? | | |
| | Please explain how proposed project compares to 2030 General Plan with respect to density standards and urban form. (See directions for filling out CAP Checklist) | , FAR, Ia | nd use |
| 2. | Would the project reduce average vehicle miles traveled (VMT) per capita of the proposed residents, employees, and/or visitors to the project by a minimum of 35% compared to the statewide average? | No* | NA |
| | Please explain how proposed project meets this requirement. If "not applicable", explain why this was project does not meet this requirement, see Directions for filling out CAP Consistency Review Checklist to meeting checklist requirements. | | |
| | (Attach a copy of the VMT model input and output. Record the model and version here | | _) |

*If "No", equivalent or better GHG reduction must be demonstrated as part of the project, and incorporated into conditions of approval.

Note: Requirements from this checklist should be incorporated into the conditions of approval, and shown on the full-size plans submitted for building plan check.

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| Ch | ecklist Item (Check the appropriate box, and provide explanation for your answer). | Yes | NA |
|----|---|-----------|-----|
| 3. | Would the project incorporate traffic calming measures? (Examples of traffic calming measures include, but are not limited to: curb extensions, speed tables, raised crosswalks, raised intersections, median islands, tight corner radii, roundabouts or mini-circles, on-street parking, planter strips with street trees, chicanes/chokers.) | | |
| | Please explain how the proposed project meets this requirement (list traffic calming measures). If "not an explain why traffic calming measures were not required. | pplicable | 3", |
| 4. | Would the project incorporate pedestrian facilities and connections to public transportation consistent with the City's Pedestrian Master Plan? | Yes | NA |
| | Please explain how the proposed project meets this requirement. If "not applicable", explain why this was required. | s not | |

*If "No", equivalent or better GHG reduction must be demonstrated as part of the project and incorporated into the conditions of approval.

Note: Requirements from this checklist should be incorporated into the conditions of approval, and shown on the full-size plans submitted for building plan check.



| s not | |
|--------------|-------|
| | |
| No* | |
| NO | NA |
| | |
| s not NCY | |
| ent. | · |
| 'es | NA |
| | |
| | rent. |

[°]If "No", equivalent or better GHG reduction must be demonstrated as part and incorporated into the conditions of approval. Note: Requirements from this checklist should be incorporated into the conditions of approval, and shown on the full-size plans submitted for building plan check.



Certification

I hereby certify that the statements furnished above and in the attached exhibits present the data and information required for this initial evaluation to the best of my ability and that the facts, statements and information presented are true and correct to the best of my knowledge and belief.

Signature: _____ Date:



DIRECTIONS FOR FILLING OUT CAP CONSISTENCY REVIEW CHECKLIST

General Plan Consistency

1. Is the proposed project substantially consistent with the land use and urban form designation, allowable floor area ratio (FAR) and/or density standards in the City's <u>2030 General Plan</u>?

Consistency with the General Plan land use and urban form designation, FAR and/or density standards is a key determining factor in whether or not the CAP Consistency Review procedure can be used. This is because future growth and development consistent with the General Plan was used to estimate business as usual emission forecasts, as well as emission reductions from actions that would be applicable to new development.

Refer to the 2030 General Plan, Land Use and Urban Form Designations and Development Standards starting on page 2-29. If a project is not fully consistent with the General Plan, the project still may qualify for consistency with the CAP, but this determination will need to be closely coordinated with the City. The City will determine whether the proposed land uses under consideration could be found consistent with the growth projections and assumptions used to develop the GHG emissions inventory and projections in the CAP.

Sustainable Land Use

2. Would the project reduce average vehicle miles traveled (VMT) per capita of the proposed residents, employees, and/or visitors to the project by a minimum of 35% compared to the statewide average? (Applicable CAP Action: 1.1.1)

The statewide VMT/capita in 2009 was 8,937 VMT/capita/year, which is approximately 24.5 VMT/capita/day^{1,2}. A 35% reduction below the 2009 statewide average would be 5,809 VMT/capita/year, or about 15.9 VMT/capita/day.

Steps to Determine if Proposed Project is Consistent with CAP Action 1.1.1:

Step 1: Consult VMT/Capita Screening Map:

The map below can be used as a quick screening tool to determine whether or not a proposed project is likely to meet the 35% reduction standard based on its geographic location.

If the proposed project is located in the green area of the map, it can be assumed to have a VMT/capita/day below 16, and no further action related to VMT is necessary. If the proposed project is located within one of the red areas, or in a white area adjacent to any red parcel, it cannot be assumed to achieve the standard, and further analysis is required to show that the project is below 16 VMT/capita/day. Proceed to Step 2, and estimate the project VMT using one of the computer modeling tools below.

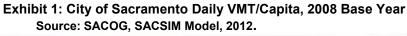
¹ Federal Highway Administration. 2009. Table VM-2 - Highway Statistics 2009. <u>http://www.fhwa.dot.gov/policyinformation/statistics/2009/vm2.cfm</u>. ² U.S. Census Bureau, 2005-2009 American Community Survey.

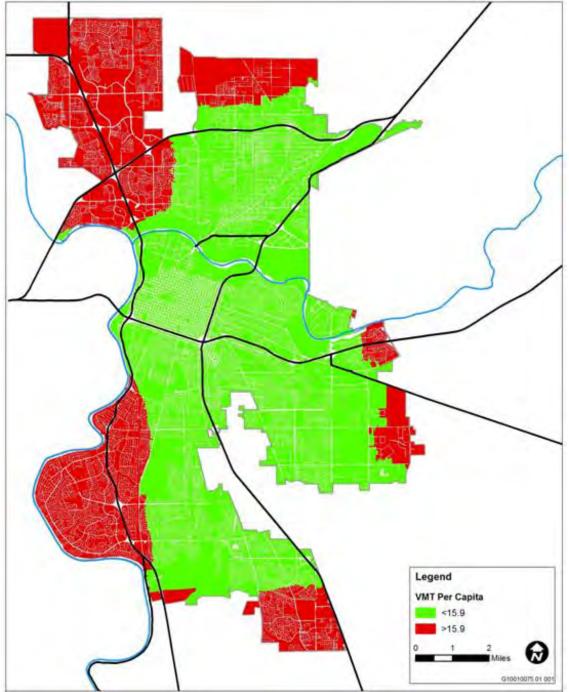
http://factfinder.census.gov/servlet/ACSSAFFFacts?_event=Search&_lang=en&_sse=on&geo_id=04000US06&_state=04000US06 CDD-0176 06-27-2013



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Step 2: VMT Modeling

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Download one of computer modeling tools from the following links and follow the user guide for the tool that you have selected. Select the year 2020 as the year of project operation and compare the modeled VMT/capita/day with the City's standard of 15.9 VMT/capita/day. If the result of the computer modeling supports the project's consistency with the City's VMT/capita standard, then the project is considered to comply with CAP Action 1.1.1. If the project's estimated VMT/capita exceeds the City's standard of 15.9, proceed to Step 3.

California Emission Estimator Model (CalEEMod 2013.2 or most recent version)

CalEEMod is a statewide land use emissions computer model that provides a comprehensive estimate of development project criteria pollutants and GHG emissions associated with both construction and operations from a variety of land use project types.

Sketch 7 VMT Estimation Tool (Contact SACOG for most recent version)

The Sketch 7 model is a web-based, parcel-level, scenario planning tool that allows users to input land uses and project attributes such as demographic data, design, density, quality of public transit, mix of land uses, and other planning-related features. Sketch 7 estimates VMT/capita and other environmental indicators based on region-specific parameters, local land use plans and the SACSIM model. Sketch 7 also accounts for the interaction of the project's proposed land uses with the surrounding land uses.

Step 3: Additional Mitigation and Further Analysis

If the proposed project does not pass Steps 1 and 2, additional mitigation from another category (such as building energy efficiency) can be substituted as long as this GHG reduction does not "double count" GHG reductions already taken by the CAP. In other words, mitigation will be necessary to reduce GHG emissions from the project beyond what is already accounted for in the CAP (to avoid double-counting).

<u>Step 3(a)</u> - Determine the increment of total VMT by which the project exceeds the City's 15.9 VMT/capita/day standard. For example, if the project would result in 18 VMT/capita/day and proposes to accommodate 400 new residents, the increment that the project would exceed the City's standard would be 306,600 VMT, which equals: (18 – 15.9 VMT/capita/day) * 400 residents *365 days/year.

<u>Step 3(b)</u> - Convert VMT into metric tons carbon dioxide equivalent per year (MT CO_2e /year) by use of a vehicle emission factor. The City recommends using an emission factor of 0.000452 MT CO_2e /VMT, which was obtained from the California Air Resources Board's (ARB's) Mobile-Source Emission Factor Model (EMFAC) and was used to develop the City's GHG inventory in its CAP. In the above example, the project would be required to mitigate approximately 139 MT CO_2e /year through additional mitigation.

Additional mitigation may include equivalent or better GHG reduction from individual measures or a combination of:

- Exceeding energy efficiency standards of Title 24, part 6 of the California Building Code (using 2008 T24 standards as a baseline)
- Generation of greater than 15% of the project's energy on-site through installation of solar panels or other onsite renewable energy technology
- Other land use (e.g., additional amenities), transportation, bicycle, or pedestrian improvements that would reduce VMT not already accounted for in Sketch 7 modeling under Step 2.

The applicant should provide documentation (e.g., <u>California Emissions Estimator Model [CalEEMod]</u>) that the combination of mitigation selected would achieve the equivalent GHG emission reduction necessary to close the gap between the proposed project's VMT/capita/day and the City's standard of 15.9 VMT/capita/day. If the project applicant can present equivalent mitigation as defined by this section, the City would consider the project consistent with CAP Action 1.1.1. If the project applicant could not identify sufficient surplus mitigation to reduce equivalent project-generated GHG emissions, the project would not be consistent with CAP Action 1.1.1.

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Mobility

3. Would the project incorporate traffic calming measures? (Applicable CAP Action: 2.1.1)

List the traffic calming measures that have been incorporated into the project. These may include, but are not limited to: curb extensions, speed tables, raised crosswalks, raised intersections, median islands, tight corner radii, roundabouts or mini-circles, on-street parking, planter strips with street trees, chicanes/chokers.

The project proponent and City staff should consult with staff in the Department of Public Works-Transportation Division to verify that traffic calming measures are adequate and in compliance with the City's Street Design Standards.

If the proposed project does not include any roadway or facility improvements, traffic calming measures may not apply. For example, certain infill projects may not result in on-street or transportation facility improvements because sufficient infrastructure already exists

4. Would the project incorporate pedestrian facilities and connections to public transportation consistent with the City's Pedestrian Master Plan? (Applicable CAP Action: 2.2.1)

List the pedestrian facilities and connections to public transportation that have been included in the proposed project on the Checklist. These may include, but are not limited to: sidewalks on both sides of streets, marked crosswalks, count-down signal timers, curb extensions, median islands, transit shelters, street lighting.

The project proponent and City staff should consult with Department of Public Works-Transportation Division staff to verify that pedestrian facilities are consistent with the <u>Pedestrian Master Plan</u>. As in the previous example, if "not applicable", an explanation shall be documented in the Checklist. The "Pedestrian Review Process Guide" (<u>Appendix A to the Master Plan</u>) will be used to determine consistency, as follows:

- For typical infill development projects where existing streets will serve the site (no new streets are proposed): the level of pedestrian improvements necessary to determine Pedestrian Master Plan consistency will be measured according to the "Basic, Upgrade or Premium" categories defined in Appendix A to the Pedestrian Master Plan, which are based on project location, surrounding land uses, proximity to transit, etc. If the proposed project does not include the minimum level of improvements per the assigned category for the project's location, the project will be required as a condition of approval to include appropriate features, per the approval of the Department of Public Works-Transportation Division.
- For new "greenfield" projects and/or larger infill development projects where new streets are proposed as part of the project, the following will apply:
 - "Basic, Upgrade or Premium" levels of improvement will be required based on the proposed project's location and context, where applicable, consistent with the criteria defined in the Master Plan. If the proposed project does not include the minimum level of improvements per the assigned category, the

project will be required as a condition of approval to include appropriate features, per the approval of the Department of Public Works-Transportation Division.

• The "Pedestrian Smart Growth Scorecard" (Appendix A to the Master Plan) will be required to be completed for the project, and a minimum score of 3 or better will need to be achieved. If the proposed



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project cannot achieve the minimum score, changes to the proposed project may be required, and/or the project may be required as a condition of approval to include certain improvements such that the average score will meet 3 or better. (Note: an Excel version of the Pedestrian Smart Growth Scorecard is available, to assist in automating the rating & scoring process)

 Would the project incorporate bicycle facilities consistent with the City's Bikeway Master Plan, and meet or exceed minimum standards for bicycle facilities in the Zoning Code and CALGreen? (Applicable CAP Action: 2.3.1)

List the bicycle facilities that are incorporated into the proposed project on the Checklist. In addition, list bicycle facilities. These include, but are not limited to: Class I bike trails and Class II bike lanes connecting the project site to an existing bike network and transit stations, bike parking [bike racks, indoor secure bike parking, bike lockers], end-of-trip facilities at non-residential land uses [showers, lockers]).

The project proponent and City staff should consult with staff in the Transportation Division of the Department of Public Works to verify that such facilities are consistent with the <u>Bikeway Master Plan</u> and meet or exceed Zoning Code and CALGreen standards. Generally, the following guidelines will be used:

- If existing on-street and off-street bikeways are already present and determined to be consistent with the Bikeway Master Plan, no additional on-street bikeways will be required. Check the "not applicable" box if appropriate. However, on-site facilities shall still be required to meet or exceed minimum Zoning and CALGreen requirements.
- If not applicable, fully document the reasons why using the Checklist.
- If on-street bicycle facilities are not present or are only partially consistent with the Master Plan, the project will be required as a condition of approval to construct or pay for its fair-share of on-street and/or off-street bikeways described in the Master Plan, in addition to meeting or exceeding minimum on-site facilities.
- In some cases, a combination of new or upgraded on-street and off-street bikeways may be used to determine consistency with the Master Plan, at the discretion of the Department of Public Works-Transportation Division staff.

Energy Efficiency and Renewable Energy

6. For residential projects of 10 or more units, commercial projects greater than 25,000 square feet, or industrial projects greater than 100,000 square feet, would the project include on-site renewable energy systems (e.g., solar photovoltaic, solar water heating etc.) that would generate at least 15% of the project's total energy demand? (CAP Actions: 3.4.1 and 3.4.2)

For projects of the minimum size specified in this measure, a commitment in the project description or in a mitigation measure that the project shall generate a minimum of 15% of the project's energy demand on-site is sufficient to demonstrate consistency with this measure. However, the project conditions of approval or mitigation measures should specify the intended renewable energy technology to be used (e.g. solar photovoltaic, solar water heating, wind, etc.) and estimated size of the systems to meet project demand based on the project description.

"Total energy demand" refers to the energy (electricity and natural gas) consumed by the built environment (including HVAC systems, water heating systems, and lighting systems) as well as uses that are independent of the construction of buildings, such as office equipment and other plug-ins.

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Applicants may estimate the total energy demand of their projects using California Emissions Estimator Model (CalEEMod 2013.2), the same software used to estimate greenhouse gas emissions. For CalEEMod estimates of energy demand to meet this specific requirement, the user should NOT select the "use historical" box, otherwise they will be "double-counting" emissions reductions that have already been counted. CalEEMod outputs for electricity demand are provided in annual kWh, and natural gas demand is provided in annual kBTU.

The energy demand estimate by CalEEMod is based on two datasets:

- The California Commercial End Use Survey (CEUS);
- The Residential Appliance Saturation Survey (RASS

CalEEMod takes energy use intensity data (above) and forecasts energy demand based on climate zone, land use subtype (such as "hospital", "arena", or "apartments, mid rise"), building area, and the number of buildings or units. This is an appropriate level of analysis for use at the planning submittal stage, but it may not provide an accurate picture of actual project energy demand because it does not factor project specifics such as building design.

Therefore, the applicant is advised (but not required) to run a more comprehensive energy simulation once projectspecific details are known: basic building design, square-footage, building envelope, lighting design (at least rudimentary), and the mechanical system (at least minimally zoned). Some of the energy simulation programs that are appropriate for this level of analysis include: DOE 2.2, Trace 700, and Energy Pro.

The U.S. DOE maintains a list of energy simulation programs that are available. <u>http://apps1.eere.energy.gov/buildings/tools_directory/subjects.cfm/pagename=subjects/pagename_menu=whole_buil</u> <u>ding_analysis/pagename_submenu=energy_simulation</u>

The applicant may then work with City staff to revise the estimate and make a final determination regarding the size of the PV system that is required.

<u>Substitutions</u>: Projects may substitute a quantity of energy efficiency for renewable energy, as long as the substituted GHG reduction does not "double count" GHG reductions already taken by the CAP. In other words, substitutions must reduce GHG emissions from the project beyond what is already accounted for in the CAP (to avoid double-counting).

- Additional mitigation may include equivalent or better GHG reduction from individual measures or a combination of:
- Exceeding energy efficiency standards of Title 24, part 6 of the California Building Code by 15% or better using 2008 T24 standards as a baseline. (Please note that due to more rigorous minimum energy efficiency standards, after January 1, 2014, residential projects will need to exceed the new minimum building code standards by 10% and commercial projects will need to exceed the new minimum building code by 5%).
- Other land use (e.g., additional amenities), transportation, bicycle, or pedestrian improvements that would reduce VMT not already accounted for in VMT models under Step 2.

7. Would the project comply with minimum CALGreen Tier I water efficiency standards? (CAP Action: 5.1.1)

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The <u>California Green Building Standards Code (CALGreen)</u> includes mandatory green building measures, as well as voluntary measures that local jurisdictions may choose to adopt to achieve higher performance tiers, at either Tier 1 or Tier 2 compliance levels. Sacramento has adopted Tier 1 Water Efficiency Standards to be required on or after January 1, 2014 Currently, in order to meet the Tier 1 Water Efficiency Standards, buildings are required to implement all mandatory water efficiency and conservation measures as well as certain Tier 1 specific measures that exceed minimum mandatory measures (e.g. 30% increase in indoor water efficiency). Specific Tier 1 provisions can be found in the CALGreen Code at http://www.bsc.ca.gov/Home/CALGreen.aspx.

The City recognizes that project construction details are often not known at the environmental review stage, and it may be premature for a project proponent to identify compliance with precise requirements of CALGreen. A condition of approval requiring the project to comply with minimum CALGreen Tier 1 water efficiency and conservation standards is sufficient to demonstrate consistency with this criterion.

Planning approval of your project will include the following condition:

Project must meet CALGreen Tier 1 water efficiency and conservation standards. Copies of the appropriate CalGreen checklist (see FAQ) shall be included on the full-size sheets for building plan check submittals.

Note: Requirements from this checklist should be incorporated into the conditions of approval, and shown on the full-size plans submitted for building plan check.

APPENDIX D

ENVIRONMENTAL NOISE ASSESSMENT



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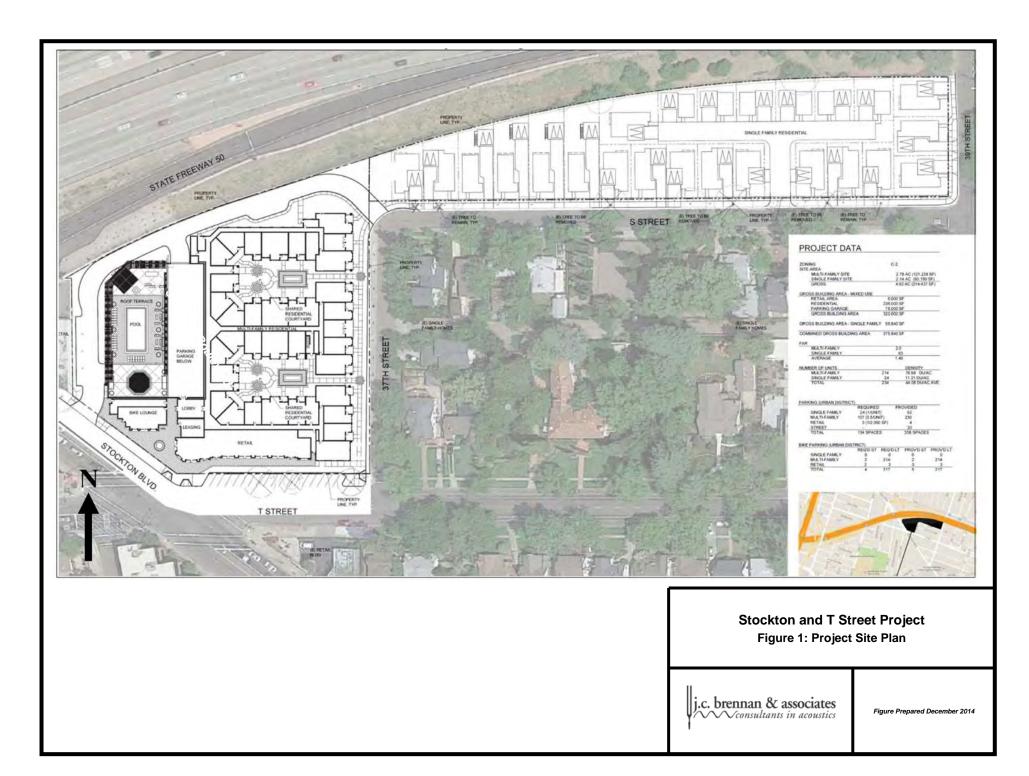
INTRODUCTION

This report has been prepared to address the noise impacts due to and upon the proposed Stockton and T Street project. The proposed project site is located within the City of Sacramento, California.

Figure 1 shows the project site plan and location.

PROJECT DESCRIPTION

The proposed project would remove the existing 120,000-square foot (sf) vacant office building (formerly AT&T) and associated parking lot and subdivide the property for construction of a mixed-use residential and commercial development. The proposed project includes a 214-unit, four-story, multi-family housing complex with ground floor commercial and parking garage, on the corner of Stockton Boulevard and T Street. In addition, the proposed project includes construction of approximately 24 single-family homes between S Street and U.S. Highway 50 (US 50).



ENVIRONMENTAL SETTING

Background Information on Noise and Vibration

Fundamentals of Acoustics

Acoustics is the science of sound. Sound may be thought of as mechanical energy of a vibrating object transmitted by pressure waves through a medium to human (or animal) ears. If the pressure variations occur frequently enough (at least 20 times per second), then they can be heard and are called sound. The number of pressure variations per second is called the frequency of sound, and is expressed as cycles per second or Hertz (Hz).

Noise is a subjective reaction to different types of sounds. Noise is typically defined as (airborne) sound that is loud, unpleasant, unexpected or undesired, and may therefore be classified as a more specific group of sounds. Perceptions of sound and noise are highly subjective from person to person.

Measuring sound directly in terms of pressure would require a very large and awkward range of numbers. To avoid this, the decibel scale was devised. The decibel scale uses the hearing threshold (20 micropascals), as a point of reference, defined as 0 dB. Other sound pressures are then compared to this reference pressure, and the logarithm is taken to keep the numbers in a practical range. The decibel scale allows a million-fold increase in pressure to be expressed as 120 dB, and changes in levels (dB) correspond closely to human perception of relative loudness.

The perceived loudness of sounds is dependent upon many factors, including sound pressure level and frequency content. However, within the usual range of environmental noise levels, perception of loudness is relatively predictable, and can be approximated by A-weighted sound levels. There is a strong correlation between A-weighted sound levels (expressed as dBA) and the way the human ear perceives sound. For this reason, the A-weighted sound level has become the standard tool of environmental noise assessment. All noise levels reported in this section are in terms of A-weighted levels, but are expressed as dB, unless otherwise noted.

The decibel scale is logarithmic, not linear. In other words, two sound levels 10 dB apart differ in acoustic energy by a factor of 10. When the standard logarithmic decibel is A-weighted, an increase of 10 dBA is generally perceived as a doubling in loudness. For example, a 70 dBA sound is half as loud as an 80 dBA sound, and twice as loud as a 60 dBA sound.

Community noise is commonly described in terms of the ambient noise level, which is defined as the all-encompassing noise level associated with a given environment. A common statistical tool to measure the ambient noise level is the average, or equivalent, sound level (L_{eq}), which corresponds to a steady-state A weighted sound level containing the same total energy as a time varying signal over a given time period (usually one hour). The L_{eq} is the foundation of the composite noise descriptor, L_{dn} , and shows very good correlation with community response to noise.

The day/night average level (L_{dn}) is based upon the average noise level over a 24-hour day, with a +10 decibel weighing applied to noise occurring during nighttime (10:00 p.m. to 7:00 a.m.) hours. The nighttime penalty is based upon the assumption that people react to nighttime noise exposures as though they were twice as loud as daytime exposures. Because L_{dn}

represents a 24-hour average, it tends to disguise short-term variations in the noise environment.

Table 1lists several examples of the noise levels associated with common situations.Appendix Aprovides a summary of acoustical terms used in this report.

| Common Outdoor Activities | Noise Level (dBA) | Common Indoor Activities |
|--|------------------------|--|
| | 110 | Rock Band |
| Jet Fly-over at 300 m (1,000 ft) | 100 | |
| Gas Lawn Mower at 1 m (3 ft) | 90 | |
| Diesel Truck at 15 m (50 ft), at 80 km/hr (50 mph) | 80 | Food Blender at 1 m (3 ft) Garbage Disposal at 1 m (3 ft) |
| Noisy Urban Area, Daytime Gas Lawn Mower, 30 m (100 ft) | 70 | Vacuum Cleaner at 3 m (10 ft) |
| Commercial Area Heavy Traffic at 90 m (300 ft) | 60 | Normal Speech at 1 m (3 ft) |
| Quiet Urban Daytime | 50 | Large Business Office Dishwasher in Next Room |
| Quiet Urban Nighttime | 40 | Theater, Large Conference Room (Background) |
| Quiet Suburban Nighttime | 30 | Library |
| Quiet Rural Nighttime | 20 | Bedroom at Night, Concert Hall (Background) |
| | 10 | Broadcast/Recording Studio |
| Lowest Threshold of Human Hearing | 0 | Lowest Threshold of Human Hearing |
| Source: Caltrans, Technical Noise Supplement | nt, Traffic Noise Anal | ysis Protocol. November, 2009. |

TABLE 1: TYPICAL NOISE LEVELS

Effects of Noise on People

The effects of noise on people can be placed in three categories:

- Subjective effects of annoyance, nuisance, and dissatisfaction
- Interference with activities such as speech, sleep, and learning
- Physiological effects such as hearing loss or sudden startling

Environmental noise typically produces effects in the first two categories. Workers in industrial plants can experience noise in the last category. There is no completely satisfactory way to measure the subjective effects of noise or the corresponding reactions of annoyance and dissatisfaction. A wide variation in individual thresholds of annoyance exists and different tolerances to noise tend to develop based on an individual's past experiences with noise.

Thus, an important way of predicting a human reaction to a new noise environment is the way it compares to the existing environment to which one has adapted: the so-called ambient noise level. In general, the more a new noise exceeds the previously existing ambient noise level, the less acceptable the new noise will be judged by those hearing it.

With regard to increases in A-weighted noise level, the following relationships occur:

- Except in carefully controlled laboratory experiments, a change of 1 dBA cannot be perceived;
- Outside of the laboratory, a 3 dBA change is considered a just-perceivable difference;
- A change in level of at least 5 dBA is required before any noticeable change in human response would be expected; and
- A 10 dBA change is subjectively heard as approximately a doubling in loudness, and can cause an adverse response.

Stationary point sources of noise – including stationary mobile sources such as idling vehicles – attenuate (lessen) at a rate of approximately 6 dB per doubling of distance from the source, depending on environmental conditions (i.e. atmospheric conditions and either vegetative or manufactured noise barriers, etc.). Widely distributed noises, such as a large industrial facility spread over many acres, or a street with moving vehicles, would typically attenuate at a lower rate.

EXISTING CONDITIONS

Existing Land Uses

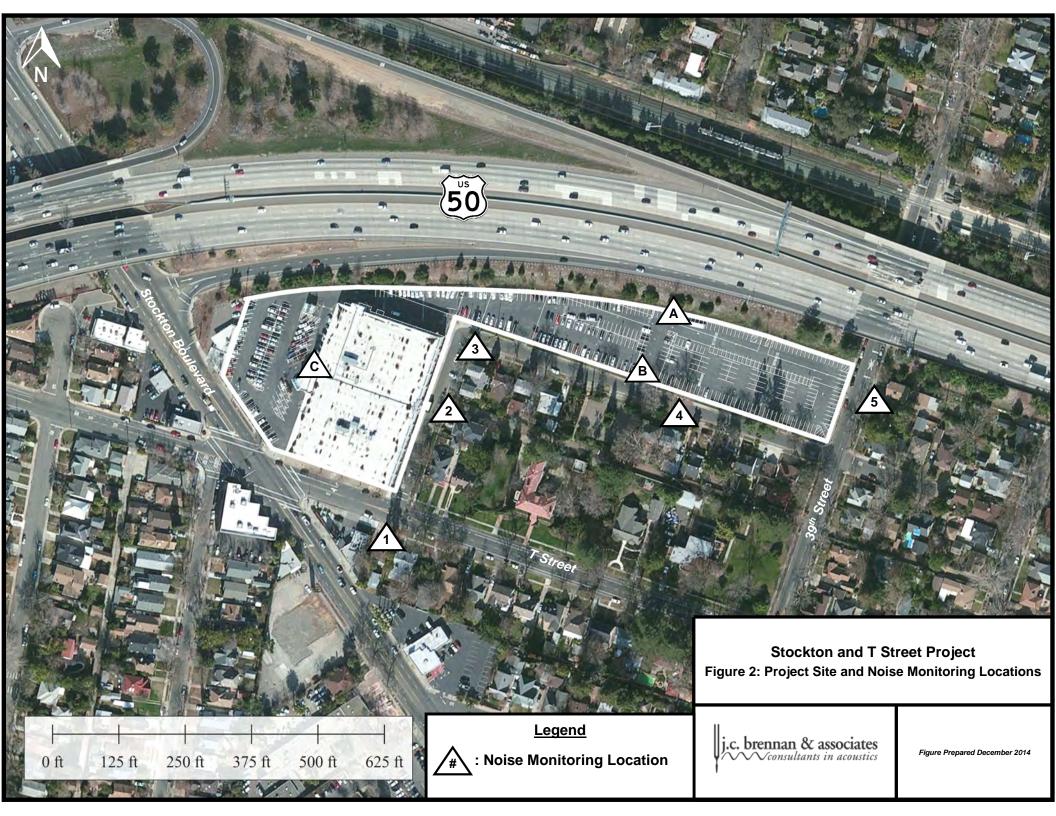
The project is in the City of Sacramento, Center and Corridor Community, the Folsom-line light rail group, and specifically within the half mile buffer around the existing 39th Street stop. The project is close to the central city area and bounded by US 50 to the north, Stockton Boulevard to the west, T Street to the south, and an existing single-family residential neighborhood to the west.

Existing Ambient Noise Levels

To quantify the existing ambient noise environment in the project vicinity, continuous 24 hour noise level measurements were conducted on the project site on Thursday September 18th - Friday September 19th, 2014. The noise measurement locations are shown on **Figure 2**. The continuous noise level measurement survey results are provided in **Table 2**. **Table 3** provides a summary of the short-term ambient noise level survey. **Appendix B** provides the complete results of the continuous noise level measurement survey.

The sound level meters were programmed to collect hourly noise level intervals at each site during the survey. The maximum value (L_{max}) represents the highest noise level measured during an interval. The average value (L_{eq}) represents the energy average of all of the noise measured during an interval. The median value (L_{50}) represents the sound level exceeded 50 percent of the time during an interval.

Larson Davis Laboratories (LDL) Model 820 precision integrating sound level meters were used for the ambient noise level measurement survey. The meters were calibrated before and after use with an LDL Model CAL200 acoustical calibrator to ensure the accuracy of the measurements. The equipment used meets all pertinent specifications of the American National Standards Institute for Type 1 sound level meters (ANSI S1.4).



| | | | | Average Measured Hourly Noise Levels, dB | | | | dB | |
|---|--|-------------------|-----------------|--|-----------------|------------------|-----------------|-----------------|------------------|
| | | | | Dayt | ime (7am- | 10pm) | Night | time (10p | m-7am) |
| Site | Location | Date | L _{dn} | L_{eq} | L ₅₀ | L _{max} | L _{eq} | L ₅₀ | L _{max} |
| Continuous (24-hour) Noise Level Measurements | | | | | | | | | |
| А | On Project Site – At Caltrans R.OW. | 9/18-9/19 2014 | 72 | 68 | 66 | 77 | 65 | 63 | 75 |
| В | On Project Site – At south boundary of project site | 9/18-9/19 2014 | 73 | 69 | 67 | 72 | 66 | 64 | 76 |
| С | On Project Site – Roof of existing two-story building. 315 feet to US-50 centerline | 9/18-9/19 2014 | 77 | 73 | 72 | 84 | 70 | 68 | 81 |
| Source | : j.c. brennan & associa | tes, Inc., 201 | 4. | | • | | • | • | • |

TABLE 2: SUMMARY OF CONTINUOUS AMBIENT NOISE MEASUREMENTS

TABLE 3: SUMMARY OF SHORT-TERM AMBIENT NOISE MONITORING

| | | Date - | Measured | Sound L | evel, dB | Estimated Day/Night Level | Notes |
|-------|---|-------------------------|----------|-----------------|------------------|---|--|
| Site | Location | Time ¹ | L_{eq} | L ₅₀ | L _{max} | (Ldn)* | Notes |
| ST-1 | T Street & 37 th South Side | 9/19/14 - 11:31 a.m. | 63 | 61 | 74 | 67 dB | US 50 & T Street Traffic is the Primary Noise Source, Background Noise is Stockton Blvd Traffic |
| ST-2 | S Street / T Street Alley @ 37th | 9/19/14 - 11:46 a.m. | 62 | 62 | 67 | 66 dB | US 50 Traffic is Primary Noise Source |
| ST-3 | SE Corner of 37 th & S Street | 9/19/14 - 11:58 a.m. | 68 | 68 | 74 | 72 dB | US 50 Traffic is Primary Noise Source |
| ST-4 | 3870 S Street, South Side | 9/19/14 - 12:20 p.m. | 68 | 68 | 71 | 72 dB | US 50 Traffic is Primary Noise Source |
| ST-5 | ST-5 1841 39 th Street 9/19/14 - 12:33 p.m. 68 68 66 72 dB is the Primary No source, Light Ra | | | | | US 50 & 39 th Street Traffic is the Primary Noise source, Light Rail is Audible but not Significant | |
| 12:00 | * L_{dn} is estimated based upon the difference between L_{eq} and L_{dn} as measured at continuous Site B for the 11:00 and 12:00 hours. The L_{dn} offset was measured to be equal to L_{eq} + 4 dB at 11:00 and 12:00. Source: j.c. brennan & associates, Inc., 2014. | | | | | | |

Existing Roadway Noise Levels

To predict existing noise levels due to traffic, the Federal Highway Administration Highway Traffic Noise Prediction Model (FHWA RD-77-108) was used. The model is based upon the Calveno reference noise emission factors for automobiles, medium trucks, and heavy trucks, with consideration given to vehicle volume, speed, roadway configuration, distance to the receiver, and the acoustical characteristics of the site. The FHWA model was developed to predict hourly L_{eq} values for free-flowing traffic conditions.

Traffic volumes for existing conditions were obtained from the traffic study prepared for the project (Fehr & Peers). Truck percentages and vehicle speeds on the local area roadways were estimated from field observations.

Traffic noise levels are predicted at the sensitive receptors located at the closest typical setback distance along each project-area roadway segment. In some locations sensitive receptors may be located at distances which vary from the assumed calculation distance and may experience shielding from intervening barriers or sound walls. However, the traffic noise analysis is believed to be representative of the majority of sensitive receptors located closest to the project-area roadway segments analyzed in this report.

Table 4 shows the existing traffic noise levels in terms of L_{dn} at closest sensitive receptors along each roadway segment. This table also shows the distances to existing traffic noise contours. A complete listing of the FHWA Model input data is contained in **Appendix C.**

| Roadway | Segment | Exterior Traffic Noise Level, dB L _{dn} |
|---|---|--|
| 35th Street | West of Stockton Blvd. | 70.2 |
| Stockton Blvd. | US 50 EB Ramp to T Street | 70.2 |
| Stockton Blvd. | South of T Street | 63.2 |
| T Street | West of Stockton Blvd. | 67.5 |
| T Street | Stockton Blvd to 37th St. | 67.5 |
| T Street | 37th St. to 39th St. | 59.7 |
| T Street | East of 39th St. | 59.8 |
| 39th St. | North of S Street | 70.3 |
| 39th St. | S Street to T Street | 61.5 |
| 39th St. | South of T Street | 60.3 |
| S Street | East of 39th St. | 37.2 |
| S Street | 39th St. to 37 St. | 72.0 |
| 37th St. | T Street to S Street. | 66.1 |
| Gerber Ave. | South of T Street | 48.0 |
| Notes: Traffic noise levels be a primary contributor to o | include estimated contribution from US-50 v | where traffic noise from US-50 was observed t |

TABLE 4: EXISTING TRAFFIC NOISE LEVELS

REGULATORY CONTEXT

Federal

There are no federal regulations related to noise that apply to the Proposed Project.

State

California Environmental Quality Act

The California Environmental Quality Act (CEQA) Guidelines, Appendix G, indicate that a significant noise impact may occur if a project exposes persons to noise or vibration levels in excess of local general plans or noise ordinance standards, or cause a substantial permanent or temporary increase in ambient noise levels. CEQA standards are discussed more below under the Thresholds of Significance criteria section.

California State Building Codes

The State Building Code, Title 24, Part 2 of the State of California Code of Regulations establishes uniform minimum noise insulation performance standards to protect persons within new buildings which house people, including hotels, motels, dormitories, apartment houses and dwellings other than single-family dwellings. Title 24 mandates that interior noise levels attributable to exterior sources shall not exceed 45 dB L_{dn} or CNEL in any habitable room.

Title 24 also mandates that for structures containing noise-sensitive uses to be located where the L_{dn} or CNEL exceeds 60 dB, an acoustical analysis must be prepared to identify mechanisms for limiting exterior noise to the prescribed allowable interior levels. If the interior allowable noise levels are met by requiring that windows be kept closed, the design for the structure must also specify a ventilation or air conditioning system to provide a habitable interior environment.

City of Sacramento General Plan

The City of Sacramento General Plan Noise Element provides the following goals and policies relative to noise.

Goal EC 3.1

Noise Reduction. Minimize noise impacts on human activity to ensure the health and safety of the community.

Policies

EC 3.1.1 Exterior Noise Standards. The City shall require noise mitigation for all development where the projected exterior noise levels exceed those shown in Table EC 1 [Table 5], to the extent feasible. (RDR)

| Table EC 1 Exterior Noise Compatibility Standards for various Land Uses | | | | |
|---|---|--|--|--|
| Land Use Type | Highest Level of Noise Exposure That Is Regarded as "Normally Acceptable" ^a (Ldn ^b or CNEL ^c) | | | |
| Residential – Low Density Single Family, Duplex, Mobile Homes | 60 dBA ^{d,c} | | | |
| Residential – Multi-family | 65 dBA | | | |
| Urban Residential Infill and Mixed-Use Projects | 70 dBA | | | |
| Transient Lodging – Motels, Hotels | 65 dBA | | | |
| Schools, Libraries, Churches, Hospitals, Nursing Homes | 70 dBA | | | |
| Auditoriums, Concert Halls, Amphitheaters | Mitigation based on site-specific study | | | |
| Sports Arena, Outdoor Spectator Sports | Mitigation based on site-specific study | | | |
| Playgrounds, Neighborhood Parks | 70 dBA | | | |
| Golf Courses, Riding Stables, Water Recreation, Cemeteries | 75 dBA | | | |
| Office buildings – business, Commercial and Professional | 70 dBA | | | |
| Industrial, Manufacturing, Utilities, Agriculture | 75 dBA | | | |
| Source: governor's Office of Planning and Research, State of California (| General Plan Guidelines 2003, October 2003. | | | |
| a. As defied in the <i>Guidelines</i>, "Normally Acceptable" means that the "specified land use is satisfactory, based upon the assumption that any building involved is of normal conventional construction, without any special noise insulation requirements." b. Ldn or Day Night Average Level is an average 24-hour noise measurement that factors in day and night noise levels. c. CNEL or Community Noise Equivalent Level measurements are a weighted average of sound levels gathered throughout a 24-hour period. d. dBA or A-weighted decibel scale is a measurement of noise levels. | | | | |
| d. dBA or A-weighted decibel scale is a measurement of noise levels. e. The exterior noise standard for the residential area west of McClellan Airport known as McClellan Heights/Parker Homes is 65 dBA. f. With land use designations of Central Business District, Urban Neighborhood (Low, Medium, or High) Urban Center (Low or High). g. All mixed-use projects located anywhere in the City of Sacramento. | | | | |

TABLE 5: CITY OF SACRAMENTO GENERAL PLAN NOISE COMPATIBILITY STANDARDS

g. All mixed-use projects located anywhere in the City of Sacramento.

EC 3.1.2 Exterior Incremental Noise Standards. The City shall require mitigation for all development that increases existing noise levels by more than the allowable increment as shown in Table EC 2 [Table 6], to the extent feasible. (RDR)

| | and Buildings where people hormally sleep ^a | Institutional land uses with p | primarily daytime and evening uses |
|--------------|---|--------------------------------|------------------------------------|
| Existing Ldn | Allowable Noise Increment | Existing Peak Hour Leq | Allowable Noise Increment |
| 45 | 8 | 45 | 12 |
| 50 | 5 | 50 | 9 |
| 55 | 3 | 55 | 6 |
| 60 | 2 | 60 | 5 |
| 65 | 1 | 65 | 3 |
| 70 | 1 | 70 | 3 |
| 75 | 0 | 75 | 1 |
| 80 | 0 | 80 | 0 |

 TABLE 6: CITY OF SACRAMENTO GENERAL PLAN INCREMENTAL NOISE STANDARDS

Source: Federal Transit Administration, *Transit Noise Impact and Vibration Assessment*, Mat 2006.

This category includes homes, hospitals, and hotels where a nighttime sensitivity to noise is assumed to be of utmost importance.

This category includes schools, libraries, theaters, and churches where it is important to avoid interference with such activities as speech, mediation, and concentration on reading material.

- **EC 3.1.3** Interior noise Standards. The City shall require new development to include noise mitigation to assure acceptable interior noise levels appropriate to the land use type: 45 dBA Ldn for residential, transient lodgings, hospitals, nursing homes and other uses where people normally sleep; and 45 dBA Leq (peak hour) for office buildings and similar uses. (RDR)
- **EC 3.1.4** Interior Noise Standards for Single Events. The City may require new development in areas subject to frequent, high-noise events (such as aircraft over-flights and trains) to meet the following interior noise standards during single noise events: 50 dBA SEL in bedrooms and 55 dBA SEL in other habitable rooms. In areas where high-noise events are especially frequent (e.g., near major truck routes), the City can require a more stringent standard of 45 dBA SEL in bedrooms unless it is demonstrated that sleep disturbance can be kept within acceptable limits at 50 dBA SEL. (RDR)
- **EC 3.1.5** Interior Vibration Standards. The City shall require construction projects anticipated to generate a significant amount of vibration to ensure acceptable interior vibration levels at nearby residential and commercial uses based on the current City or Federal Transit Administration (FTA) criteria. (RDR)

- **EC 3.1.6** Vibration Screening Distances. The City shall require new residential and commercial projects located adjacent to major freeways, hard rail lines, or light rail lines to follow the FTA screening distance criteria. (RDR)
- **EC 3.1.7 Vibration.** The City shall require an assessment of the damage potential of vibration-induced construction activities, highways, and rail lines in close proximity to historic buildings and archaeological sites and require all feasible mitigation measures be implemented to ensure no damage would occur. (RDR)
- **EC 3.1.8 Operational Noise.** The City shall require mixed-use, commercial, and industrial projects to mitigate operational noise impacts to adjoining sensitive uses when operational noise thresholds are exceeded. (RDR)
- **EC 3.1.9 Compatibility with Park and Recreation Uses.** The City shall limit the hours of operation for parks and active recreation areas in residential areas to minimize disturbance to residences. (RDR/SO)
- **EC 3.1.10 Construction Noise.** The City shall require development projects subject to discretionary approval to assess potential construction noise impacts on nearby sensitive uses and to minimize impacts on these uses, to the extent feasible. (RDR)
- **EC 3.1.11** Alternatives to Sound Walls. The City shall encourage the use of design strategies and other noise reduction methods along transportation corridors in lieu of sound walls to mitigate noise impacts and enhance aesthetics. (RDR)
- **EC 3.1.12 Residential Streets.** The City shall discourage widening streets or converting streets to one-way in residential areas where the resulting increased traffic volumes would raise ambient noise levels. (MPSP/SO)
- **EC 3.1.13** Vehicle Purchase. The City shall purchase vehicles and equipment with low noise generation and maintain them to minimize noise. (SO)

Sacramento City Municipal Code

Article II. Noise Standards

8.68.060 Exterior noise standards.

- A. The following noise standards unless otherwise specifically indicated in this article shall apply to all agricultural and residential properties.
 - 1. From seven a.m. to ten p.m. the exterior noise standard shall be fifty-five (55) dBA.
 - 2. From ten p.m. to seven a.m. the exterior noise standard shall be fifty (50) dBA.
- B. It is unlawful for any person at any location to create any noise which causes the noise levels when measured on agricultural or residential property to exceed for the duration of time set forth following, the specified exterior noise standards in any one hour by:

Cumulative Duration of the Intrusive Sound

Allowance Decibels

- 1. Cumulative period of 30 minutes per hour.....0 dB
- 2. Cumulative period of 15 minutes per hour.....+5 dB
- 3. Cumulative period of 5 minutes per hour.....+10 dB
- 4. Cumulative period of 1 minute per hour.....+15 dB
- 5. Level not to be exceeded for any time per hour.....+20 dB
- C. Each of the noise limits specified in subsection B of this section shall be reduced by five dBA for impulsive or simple tone noises, or for noises consisting of speech or music.
- D. If the ambient noise level exceeds that permitted by any of the first four noise limit categories specified in subsection B of this section, the allowable noise limit shall be increased in five dBA increments in each category to encompass the ambient noise level. If the ambient noise level exceeds the fifth noise level category, the maximum ambient noise level shall be the noise limit for that category. (Prior code § 66.02.201)

8.68.070 Interior noise standards.

- A. In any apartment, condominium, townhouse, duplex or multiple dwelling unit it is unlawful for any person to create any noise from inside his or her unit that causes the noise level when measured in a neighboring unit during the periods ten p.m. to seven a.m. to exceed:
 - 1. Forty-five (45) dBA for a cumulative period of more than five minutes in any hour;
 - 2. Fifty (50) dBA for a cumulative period of more than one minute in any hour;
 - 3. Fifty-five (55) dBA for any period of time.
- B. If the ambient noise level exceeds that permitted by any of the noise level categories specified in subsection A of this section, the allowable noise limit shall be increased in five dBA increments in each category to encompass the ambient noise level. (Prior code § 66.02.202)

8.68.080 Exemptions.

The following activities shall be exempted from the provisions of this chapter:

- A. School bands, school athletic and school entertainment events. School entertainment events shall not include events sponsored by student organizations;
- B. Activities conducted on parks and public playgrounds, provided such parks and public playgrounds are owned and operated by a public entity;
- C. Any mechanical device, apparatus or equipment related to or connected with emergency activities or emergency work;
- D. Noise sources due to the erection (including excavation), demolition, alteration or repair of any building or structure between the hours of seven a.m. and six p.m., on Monday, Tuesday, Wednesday, Thursday, Friday and Saturday, and between nine a.m. and six p.m. on Sunday; provided, however, that the operation of an internal combustion engine shall not be exempt pursuant to this subsection if such engine is not equipped with suitable exhaust and intake silencers which are in good working order. The director of building inspections, may permit work to be done during the hours not exempt by this subsection in the case of urgent necessity and in the interest of public health and welfare for a period not to exceed three days. Application for this exemption may be made in conjunction with the application for the work permit or during progress of the work;
- E. Noise sources associated with agricultural operations provided such operations take place between the hours of six a.m. and eight p.m.; provided, however, that the operation of an internal combustion engine shall not be exempt pursuant to this subsection if such engine is not equipped with suitable exhaust and intake silencers which are in good working order;

- F. Any mechanical device, apparatus or equipment which are utilized for the protection or salvage of agricultural crops during period of adverse weather conditions or when the use of mobile noise sources is necessary for pest control; provided, however, that the operation of an internal combustion engine shall not be exempt pursuant to this subsection if such engine is not equipped with suitable exhaust and intake silencers which are in good working order;
- G. Noise sources associated with maintenance of street trees and residential area property provided said activities take place between the hours of seven a.m. and six p.m.;
- H. Tree and park maintenance activities conducted by the city department of parks and community services; provided, however, that use of portable gasoline-powered blowers within two hundred (200) feet of residential property shall comply with the requirements of Section 8.68.150 of this chapter;
- I. Any activity to the extent provisions of Chapter 65 of Title 42 of the United States Code, and Articles 3 and 3.5 of Chapter 4 of Division 9 of the Public Utilities Code of the state of California preempt local control of noise regulations and land use regulations related to noise control of airports and their surrounding geographical areas, any noise source associated with the construction, development, manufacture, maintenance, testing or operation of any aircraft engine, or of any weapons system or subsystems which are owned, operated or under the jurisdiction of the United States, any other activity to the extent regulation thereof has been preempted by state or federal law or regulation;
- J. Any noise sources associated with the maintenance and operation of aircraft or airports which are owned or operated by the United States. (Ord. 2010-021 § 10; prior code § 66.02.203)

Vibration Standards

Vibration is like noise in that it involves a source, a transmission path, and a receiver. While vibration is related to noise, it differs in that in that noise is generally considered to be pressure waves transmitted through air, whereas vibration usually consists of the excitation of a structure or surface. As with noise, vibration consists of an amplitude and frequency. A person's perception to the vibration will depend on their individual sensitivity to vibration, as well as the amplitude and frequency of the source and the response of the system which is vibrating.

Vibration can be measured in terms of acceleration, velocity, or displacement. A common practice is to monitor vibration measures in terms of peak particle velocities in inches per second. Standards pertaining to perception as well as damage to structures have been developed for vibration levels defined in terms of peak particle velocities.

The City of Sacramento does not have specific policies pertaining to vibration levels. However, vibration levels associated with construction activities and project operations are addressed as potential noise impacts associated with project implementation.

Human and structural response to different vibration levels is influenced by a number of factors, including ground type, distance between source and receptor, duration, and the number of perceived vibration events. **Table 7** indicates that the threshold for damage to structures ranges

from 0.2 to 0.6 peak particle velocity in inches per second (in/sec p.p.v). The general threshold at which human annoyance could occur is noted as 0.1 in/sec p.p.v.

| Peak Part | icle Velocity | Human Reaction | Effect on Buildings |
|------------|-----------------|---|--|
| mm/sec. | in./sec. | numan Reaction | Effect on Buildings |
| 0.15-0.30 | 0.006-0.019 | Threshold of perception; possibility of intrusion | Vibrations unlikely to cause damage of any type |
| 2.0 | 0.08 | Vibrations readily perceptible | Recommended upper level of the vibration to which ruins and ancient monuments should be subjected |
| 2.5 | 0.10 | Level at which continuous vibrations begin to annoy people | Virtually no risk of "architectural" damage to normal buildings |
| 5.0 | 0.20 | Vibrations annoying to people in buildings (this agrees with the levels established for people standing on bridges and subjected to relative short periods of vibrations) | Threshold at which there is a risk of "architectural" damage to normal dwelling - houses with plastered walls and ceilings. Special types of finish such as lining of walls, flexible ceiling treatment, etc., would minimize "architectural" damage |
| 10-15 | 0.4-0.6 | Vibrations considered unpleasant by people subjected to continuous vibrations and unacceptable to some people walking on bridges | Vibrations at a greater level than normally expected from traffic, but would cause "architectural" damage and possibly minor structural damage. |
| Source: Ca | ltrans. Transpo | ortation Related Earthborne Vibrations | s. TAV-02-01-R9601 February 20, 2002. |

 TABLE 7: EFFECTS OF VIBRATION ON PEOPLE AND BUILDINGS

IMPACTS AND MITIGATION MEASURES

Method of Analysis

Traffic Noise Impact Assessment Methodology

To describe future noise levels due to traffic, the Federal Highway Administration Highway Traffic Noise Prediction Model (FHWA RD-77-108) was used. Direct inputs to the model included ADT traffic volumes provided by Fehr & Peers. The FHWA model is based upon the Calveno reference noise factors for automobiles, medium trucks and heavy trucks, with consideration given to vehicle volume, speed, roadway configuration, distance to the receiver, and the acoustical characteristics of the site. The FHWA model was developed to predict hourly L_{eq} values for free-flowing traffic conditions. To predict $L_{dn}/CNEL$ values, it is necessary to determine the day/night distribution of traffic and adjust the traffic volume input data to yield an equivalent hourly traffic volume.

Construction Noise and Vibration Impact Methodology

Construction noise and vibration was analyzed using data compiled for various pieces of construction equipment at a representative distance of 50 feet. Construction activities are discussed relative to the applicable City of Sacramento noise policies. Potential impacts and mitigation measures are discussed.

Thresholds of Significance

Consistent with Appendix G of the CEQA Guideline, and the City's General Plan and Noise Ordinance, the project will have a significant impact related to noise if it will result in:

- A. Exposure of persons to, or generation of noise levels in excess of standards established in the local general plan or noise ordinance, or applicable standards of other agencies. Specifically, 70 dB L_{dn} for urban infill residential at exterior outdoor use areas and 45 dB L_{dn} at interior residential areas.
- Exposure of persons to or generation of excessive groundborne vibration or groundborne noise levels. Specifically, a limit of 0.1 in/sec p.p.v., as discussed above;
- C. A substantial permanent increase in ambient noise levels in the project vicinity above levels existing without the project, as defined by **Table 6** above;
- A substantial temporary or periodic increase in ambient noise levels in the project vicinity, as defined by **Table 6** above, beyond levels permissible under the City's General Plan and Noise Ordinance;
- E. For a project located within an airport land use plan or, where such a plan has not been adopted, within two miles of a public airport or public use airport, expose people residing or working in the project area to excessive noise levels within two miles of a public airport or public use airport; or
- F. For a project within the vicinity of a private airstrip, expose people residing or working in the project area to excessive noise levels.

The proposed project is not located within two miles of a public or private airport or airstrip. Therefore, aircraft noise is not discussed further in this analysis.

PROJECT-SPECIFIC IMPACTS AND MITIGATION MEASURES

Impact 1 Construction Noise at Sensitive Receptors

Construction of the Proposed Project would temporarily increase noise levels during construction. This would be a *less than significant* impact.

During the construction of the project including water and sewer lines and related infrastructure, noise from construction activities would add to the noise environment in the project vicinity. Activities involved in construction would generate maximum noise levels, as indicated in **Table 8**, ranging from 76 to 90 dB at a distance of 50 feet. Construction activities would be temporary in nature and are anticipated to occur during normal daytime working hours.

Noise would also be generated during the construction phase by increased truck traffic on area roadways. A substantial project-generated noise source would be truck traffic associated with transport of heavy materials and equipment to and from construction sites. This noise increase would be of short duration, and would likely occur primarily during daytime hours. It should also be noted that existing ambient noise levels in the project vicinity are influenced substantially by traffic on US-50 during daytime and nighttime hours. Existing ambient noise levels due to traffic on US-50 were found to be approximately 66-72 dB L_{dn} around the project site, as shown in **Table 3**.

| Type of Equipment | Maximum Level, dB at 50 feet |
|-------------------|------------------------------|
| Backhoe | 78 |
| Compactor | 83 |
| Compressor (air) | 78 |
| Concrete Saw | 90 |
| Dozer | 82 |
| Dump Truck | 76 |
| Excavator | 81 |
| Generator | 81 |
| Jackhammer | 89 |
| Pneumatic Tools | 85 |

TABLE 8 : CONSTRUCTION EQUIPMENT NOISE

Source: *Roadway Construction Noise Model User's Guide*. Federal Highway Administration. FHWA-HEP-05-054. January 2006.

The City of Sacramento Municipal Code Section 8.68.080 exempts constructiongenerated noise as outlined below:

Noise sources due to the erection (including excavation), demolition, alteration or repair of any building or structure between the hours of seven a.m. and six p.m., on Monday, Tuesday, Wednesday, Thursday, Friday and Saturday, and between nine a.m. and six p.m. on Sunday; provided, however, that the operation of an internal combustion engine shall not be exempt pursuant to this subsection if such engine is not equipped with suitable exhaust and intake silencers which are in good working order. The director of building inspections, may permit work to be done during the hours not exempt by this subsection in the case of urgent necessity and in the interest of public health and welfare for a period not to exceed three days. Application for this exemption may be made in conjunction with the application for the work permit or during progress of the work;

These exemptions are typical of City and County Noise Ordinances and reflect the recognition that construction-related noise is temporary in character, is generally acceptable when limited to daylight hours, and is part of what residents of urban areas expect as part of a typical urban noise environment (along with sirens, etc.).

Construction activities would be temporary in nature, will occur during normal daytime working hours listed above, and will comply with the requirements of the City of Sacramento Noise Ordinance. Therefore, construction noise will be a **less than significant** impact.

Impact 2 Transportation Noise at Existing Sensitive Receptors

Traffic generated by the Proposed Project could generate traffic noise increases exceeding the substantial increase criteria as outlined in the Thresholds of Significance criteria above. This would be a *less than significant* impact.

To predict existing plus project noise levels due to traffic, the Federal Highway Administration Highway Traffic Noise Prediction Model (FHWA RD-77-108) was used. The model is based upon the Calveno reference noise emission factors for automobiles, medium trucks, and heavy trucks, with consideration given to vehicle volume, speed, roadway configuration, distance to the receiver, and the acoustical characteristics of the site. The FHWA model was developed to predict hourly L_{eq} values for free-flowing traffic conditions.

Traffic volumes for existing conditions were obtained from the traffic study prepared for the project (Fehr & Peers). Truck percentages and vehicle speeds on the local area roadways were estimated from field observations.

Traffic noise levels are predicted at the sensitive receptors located at the closest typical setback distance along each project-area roadway segment. In some locations sensitive receptors may be located at distances which vary from the assumed calculation distance and may experience shielding from intervening barriers or sound walls. However, the traffic noise analysis is believed to be representative of the majority of sensitive receptors located closest to the project-area roadway segments analyzed in this report.

Table 9 shows the predicted traffic noise level increases on the local roadway network for existing and existing plus project conditions.

Appendix C provides the complete inputs and results of the FHWA traffic noise modeling.

| | | Noise Levels (L _{dn} , dB) at Nearest Sensitive Receptors | | | | |
|----------------|---------------------------|--|--------------------|--------|--|--|
| Roadway | Segment | Existing | Existing + Project | Change | | |
| 35th Street | West of Stockton Blvd. | 70.2 | 70.2 | 0.0 | | |
| Stockton Blvd. | US 50 EB Ramp to T St. | 70.2 | 70.2 | 0.0 | | |
| Stockton Blvd. | South of T Street | 63.2 | 63.4 | 0.2 | | |
| T Street | West of Stockton Blvd. | 67.5 | 67.5 | 0.0 | | |
| T Street | Stockton Blvd to 37th St. | 67.5 | 67.8 | 0.3 | | |
| T Street | 37th St. to 39th St. | 59.7 | 59.8 | 0.1 | | |
| T Street | East of 39th St. | 59.8 | 59.8 | 0.0 | | |
| 39th St. | North of S Street | 70.3 | 70.3 | 0.0 | | |
| 39th St. | S Street to T Street | 61.5 | 61.6 | 0.1 | | |
| 39th St. | South of T Street | 60.3 | 60.3 | 0.0 | | |
| S Street | East of 39th St. | 37.2 | 37.2 | 0.0 | | |
| S Street | 39th St. to 37 St. | 72.0 | 72.0 | 0.0 | | |
| 37th St. | T Street to S Street. | 66.1 | 66.2 | 0.1 | | |
| Gerber Ave. | South of T Street | 48.0 | 49.0 | 1.0 | | |

TABLE 9: EXISTING AND EXISTING + PROJECT TRAFFIC NOISE LEVELS

Some noise sensitive receptors located along the project-area roadways are currently exposed to exterior traffic noise levels exceeding the City of Sacramento 60 dB L_{dn} exterior noise level standard for residential uses, as shown in **Table 9**. These receptors will continue to experience elevated exterior noise levels with implementation of the proposed project. The proposed project's contribution to traffic noise increases is predicted to be 1.0 dBA L_{dn} , or less. This is less than the City's allowable increase threshold of 5 dB where existing noise levels are 50 dB L_{dn} or less, as outlined in **Table 6**. Therefore, the increase of 1.0 dB L_{dn} is considered less than significant relative to the substantial increase threshold.

The proposed project would not cause increased noise levels exceeding the City of Sacramento 60 dB L_{dn} exterior noise level standard at existing noise-sensitive residential receptors. Therefore, this would be a less-than-significant impact relative to the CEQA checklist threshold (a). Additionally, the noise level increases associated with the proposed project do not exceed the City's substantial increase criteria outlined above. Therefore, this would be a less-than-significant impact relative to the CEQA checklist threshold (b).

This impact is considered **less than significant** relative to the project's significance criteria.

Mitigation for Impact 2: None required

Impact 3: Transportation Noise at New Sensitive Receptors

The proposed project could expose new noise-sensitive uses to transportation noise levels that exceed the City of Sacramento exterior and interior noise level standards. This is considered to be a **potentially significant** impact.

Exterior Traffic Noise Level Impacts:

The FHWA traffic noise prediction model was used to predict Cumulative + Project traffic noise levels at the proposed residential land uses associated with the project. Future traffic projections for US-50 were obtained from the Sacramento County General Plan Update EIR Appendix E. Truck percentages were obtained from Caltrans vehicle counts.

Table 10 shows the predicted traffic noise levels at the proposed residential uses adjacent to US-50. **Table 10** also indicates the property line noise barrier heights required to achieve compliance with an exterior noise level standard of 60 dB L_{dn} .

Appendix D provides the complete inputs and results to the FHWA traffic noise prediction model and barrier calculations. The modeled noise barriers are relative to building pad elevations.

| Noise Source | Receptor Description | Approximate Residential Setback, feet ¹ | ADT | Prec | licted Noise | Levels, dBA | L _{dn} ² |
|---|----------------------|--|---------|---------|--------------|-------------|------------------------------|
| | Traffic Noise | | | No Wall | 8' Wall | 10' Wall | 12' Wall |
| Highway 50 | SF Backyards | 170 | 275,700 | 72 dB | 66 dB | 65 dB | 65 dB |
| Highway 50 | MF Roof Pool Deck | 285 | 275,700 | 78 dB | 67 dB | 66 dB | 65 dB |
| Setback distances are measured in feet from the centerlines of the roadways to the center of residential backyards. - Meets the City of Sacramento exterior noise standard without mitigation. Standard does not apply to second floor acades. Source: FHWA-RD-77-108 with inputs from Fehr & Peers, and j.c. brennan & associates, Inc. 2014. | | | | | | | |

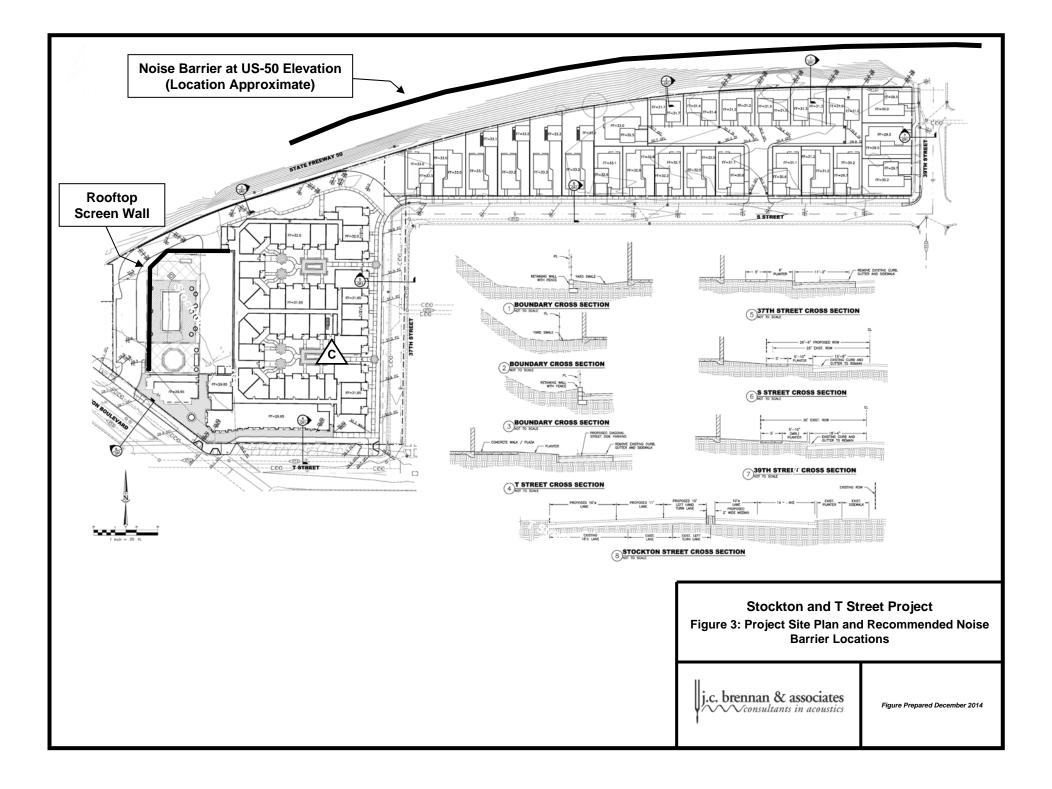
TABLE 10: TRANSPORTATION NOISE LEVELS AT PROPOSED RESIDENTIAL USES

The **Table 10** data indicate that noise barriers 8-feet in height would be sufficient to reduce exterior noise levels to less than 70 dB L_{dn} at sensitive receptors located adjacent to US-50.

It should be noted that this analysis assumes that a noise barrier for the single-family residential portion of the project would be constructed on the US-50 berm at the roadway edge, within the Caltrans right-of-way. It is our understanding that Caltrans is currently reviewing plans to install a 10-foot tall barrier at this location, associated with a high-occupancy vehicle lane project.

For the multi-family residential project, this analysis assumes that a rooftop screen wall would be constructed to a minimum height of 8-feet relative to the pool deck. This wall may consist of glass, metal or wood-framed stucco construction, or any combination of these materials. It is our understanding that the project currently includes this wall as a design feature of the project.

Figure 3 shows the noise barrier locations reviewed in this analysis.



Interior Noise Impacts:

Modern construction typically provides a 25 dB exterior-to-interior noise level reduction with windows closed. Therefore, sensitive receptors exposed to exterior noise of 70 dB L_{dn} , or less, will typically comply with the City of Sacramento 45 dB L_{dn} interior noise level standard. Additional noise reduction measures, such as acoustically rated windows are generally required for exterior noise levels exceeding 70 dB L_{dn} .

The proposed single-family residential uses are predicted to be exposed to exterior noise levels of 79 dB L_{dn} or 80 dB L_{dn} for the multi-family uses, as shown in **Appendix D**. It should be noted that this assessment is conservative as no shielding is assumed for second or third floor facades. Depending on the final barrier design along US-50, some second or third floor shielding could occur which would result in lower exterior and interior noise levels.

Based upon a 25 dB exterior-to-interior noise level reduction interior traffic noise levels are predicted to range between 54-55 dB L_{dn} at these uses, without special construction techniques. Therefore, interior noise control measures would be required for the residential uses adjacent to US-50.

At this time no building plans are available for the proposed project. Therefore, specific interior noise control measures cannot be recommended at this time. However, it is likely that windows having a sound transmission class (STC) rating of 40-45 would be required for any facades with direct exposure to US-50 traffic noise. These facades may also require the use of resilient channels (RC) for exterior walls, or similar wall type construction. Additional acoustic treatments to ventilation openings and HVAC mechanical penetrations may also be required. Such measures should be reviewed when building plans are available.

Facades which are separated by an exterior corridor wall, such as is currently proposed for the multi-family site would not require extensive acoustical upgrades.

Mitigation for Impact 3:

- *MM 3a:* A sound wall 8-feet in height (minimum) shall be constructed along US-50, at the location shown on **Figure 3**. Noise barrier walls shall be constructed of concrete panels, concrete masonry units, earthen berms, or any combination of these materials.
- *MM3b:* The multifamily pool deck screen wall shall be constructed to a minimum height of 8-feet.
- **MM 3c:** A detailed analysis of interior noise levels shall be conducted when building plans are available for the residential uses with direct exposure to US-50 traffic noise. The analysis shall detail noise control measures that are required to achieve compliance with the City of Sacramento 45 dB L_{dn} interior noise level standard. Such analysis shall be conducted by a qualified acoustical consultant recognized by the City of Sacramento.
- *MM 3d:* Mechanical ventilation shall be installed in all residential uses to allow residents to keep doors and windows closed, as desired for acoustical isolation.

Significance after Mitigation: Less than significant.

Impact 4: Construction Vibration at Sensitive Receptors

The proposed project has the potential to expose sensitive receptors to substantial vibration associated with construction activities. This would be a **less than significant** impact.

The primary vibration-generating activities associated with the proposed project would occur during construction when activities such as grading and utility placement.

Construction vibration impacts include human annoyance and building structural damage. Human annoyance occurs when construction vibration rises significantly above the threshold of perception. Building damage can take the form of cosmetic or structural. **Table 11** shows the typical vibration levels produced by construction equipment.

Sensitive receptors could be impacted by construction related vibrations, especially vibratory compactors/rollers. The nearest receptors are located approximately 50 feet or further from any areas of the project site that might require grading or paving. At this distance construction vibrations are not predicted to exceed acceptable levels. Additionally, construction activities would be temporary in nature and would likely occur during normal daytime working hours.

| | Peak Particle Velocity @ 25 feet | Peak Particle Velocity @ 50 feet | Peak Particle Velocity @ 100 feet |
|-------------------------------|-------------------------------------|-------------------------------------|--------------------------------------|
| Type of Equipment | (inches/second) | (inches/second) | (inches/second) |
| Large Bulldozer | 0.089 | 0.031 | 0.011 |
| Loaded Trucks | 0.076 | 0.027 | 0.010 |
| Small Bulldozer | 0.003 | 0.001 | 0.000 |
| Auger/drill Rigs | 0.089 | 0.031 | 0.011 |
| Jackhammer | 0.035 | 0.012 | 0.004 |
| Vibratory Hammer | 0.070 | 0.025 | 0.009 |
| Vibratory Compactor/roller | 0.210 | 0.074 | 0.026 |
| Source: Federal Transit Admin | istration, Transit Noise and | Vibration Impact Assessm | nent Guidelines, May 2006 |

TABLE 11: VIBRATION LEVELS FOR VARYING CONSTRUCTION EQUIPMENT

The **Table 11** data indicate that construction vibration levels anticipated for the project are less than the 0.1 in/sec criteria at distances of 50 feet. Therefore, construction vibrations are not predicted to cause damage to existing buildings or cause annoyance to sensitive receptors which are located 500 feet from the project site. Implementation of the proposed project would have a **less than significant** impact.

Mitigation for Impact 4: None required

Appendix A Acoustical Terminology

Acoustics The science of sound. **Ambient Noise** The distinctive acoustical characteristics of a given space consisting of all noise sources audible at that location. In many cases, the term ambient is used to describe an existing or pre-project condition such as the setting in an environmental noise study. Attenuation The reduction of an acoustic signal. A-Weighting A frequency-response adjustment of a sound level meter that conditions the output signal to approximate human response. Decibel or dB Fundamental unit of sound, A Bell is defined as the logarithm of the ratio of the sound pressure squared over the reference pressure squared. A Decibel is one-tenth of a Bell. CNEL Community Noise Equivalent Level. Defined as the 24-hour average noise level with noise occurring during evening hours (7 - 10 p.m.) weighted by a factor of three and nighttime hours weighted by a factor of 10 prior to averaging. Frequency The measure of the rapidity of alterations of a periodic signal, expressed in cycles per second or hertz (Hz). Day/Night Average Sound Level. Similar to CNEL but with no evening weighting. Ldn Lea Equivalent or energy-averaged sound level. The highest root-mean-square (RMS) sound level measured over a given period of time. Lmax The sound level exceeded a described percentile over a measurement period. For instance, an hourly L_{50} is L_(n) the sound level exceeded 50% of the time during the one hour period. Loudness A subjective term for the sensation of the magnitude of sound. Unwanted sound. Noise NRC Noise Reduction Coefficient. NRC is a single-number rating of the sound-absorption of a material equal to the arithmetic mean of the sound-absorption coefficients in the 250, 500, 1000, and 2,000 Hz octave frequency bands rounded to the nearest multiple of 0.05. It is a representation of the amount of sound energy absorbed upon striking a particular surface. An NRC of 0 indicates perfect reflection; an NRC of 1 indicates perfect absorption. **Peak Noise** The level corresponding to the highest (not RMS) sound pressure measured over a given period of time. This term is often confused with the "Maximum" level, which is the highest RMS level. **RT**₆₀ The time it takes reverberant sound to decay by 60 dB once the source has been removed. Sabin The unit of sound absorption. One square foot of material absorbing 100% of incident sound has an absorption of 1 Sabin. SEL Sound Exposure Level. SEL is s rating, in decibels, of a discrete event, such as an aircraft flyover or train passby, that compresses the total sound energy into a one-second event. STC Sound Transmission Class. STC is an integer rating of how well a building partition attenuates airborne sound. It is widely used to rate interior partitions, ceilings/floors, doors, windows and exterior wall configurations. Threshold The lowest sound that can be perceived by the human auditory system, generally considered to be 0 dB for of Hearing persons with perfect hearing. Approximately 120 dB above the threshold of hearing. Threshold of Pain Impulsive Sound of short duration, usually less than one second, with an abrupt onset and rapid decay. Simple Tone Any sound which can be judged as audible as a single pitch or set of single pitches.



Appendix B

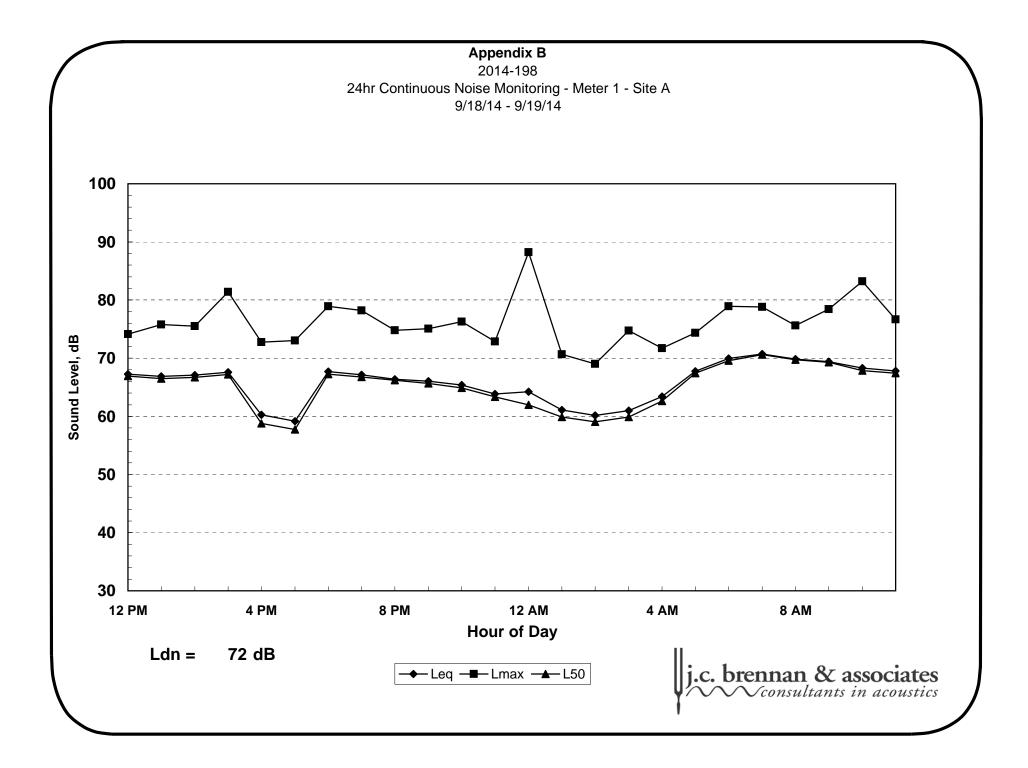
2014-198 24hr Continuous Noise Monitoring - Meter 1 - Site A 9/18/14 - 9/19/14

| Hour | Leq | Lmax | L50 | L90 |
|-------|-----|------|-----|-----|
| 12:00 | 67 | 74 | 67 | 65 |
| 13:00 | 67 | 76 | 67 | 65 |
| 14:00 | 67 | 76 | 67 | 65 |
| 15:00 | 68 | 81 | 67 | 65 |
| 16:00 | 60 | 73 | 59 | 56 |
| 17:00 | 59 | 73 | 58 | 55 |
| 18:00 | 68 | 79 | 67 | 66 |
| 19:00 | 67 | 78 | 67 | 65 |
| 20:00 | 66 | 75 | 66 | 64 |
| 21:00 | 66 | 75 | 66 | 64 |
| 22:00 | 65 | 76 | 65 | 62 |
| 23:00 | 64 | 73 | 63 | 60 |
| 0:00 | 64 | 88 | 62 | 58 |
| 1:00 | 61 | 71 | 60 | 56 |
| 2:00 | 60 | 69 | 59 | 53 |
| 3:00 | 61 | 75 | 60 | 55 |
| 4:00 | 63 | 72 | 63 | 57 |
| 5:00 | 68 | 74 | 67 | 64 |
| 6:00 | 70 | 79 | 70 | 68 |
| 7:00 | 71 | 79 | 71 | 69 |
| 8:00 | 70 | 76 | 70 | 68 |
| 9:00 | 69 | 78 | 69 | 68 |
| 10:00 | 68 | 83 | 68 | 66 |
| 11:00 | 68 | 77 | 67 | 65 |

| | Statistical Summary | | | | | | | |
|------------------|---------------------|---|---------|------|-----|---------|--|--|
| | Daytim | Daytime (7 a.m 10 p.m.) Nighttime (10 p.m 7 a | | | | | | |
| | High | Low | Average | High | Low | Average | | |
| Leq (Average) | 71 | 59 | 68 | 70 | 60 | 65 | | |
| Lmax (Maximum) | 83 | 73 | 77 | 88 | 69 | 75 | | |
| L50 (Median) | 71 | 58 | 66 | 70 | 59 | 63 | | |
| L90 (Background) | 69 | 55 | 64 | 68 | 53 | 59 | | |

| Computed Ldn, dB | 72 |
|--------------------|-----|
| % Daytime Energy | 74% |
| % Nighttime Energy | 26% |

j.c. brennan & associates *Consultants in acoustics*



Appendix B

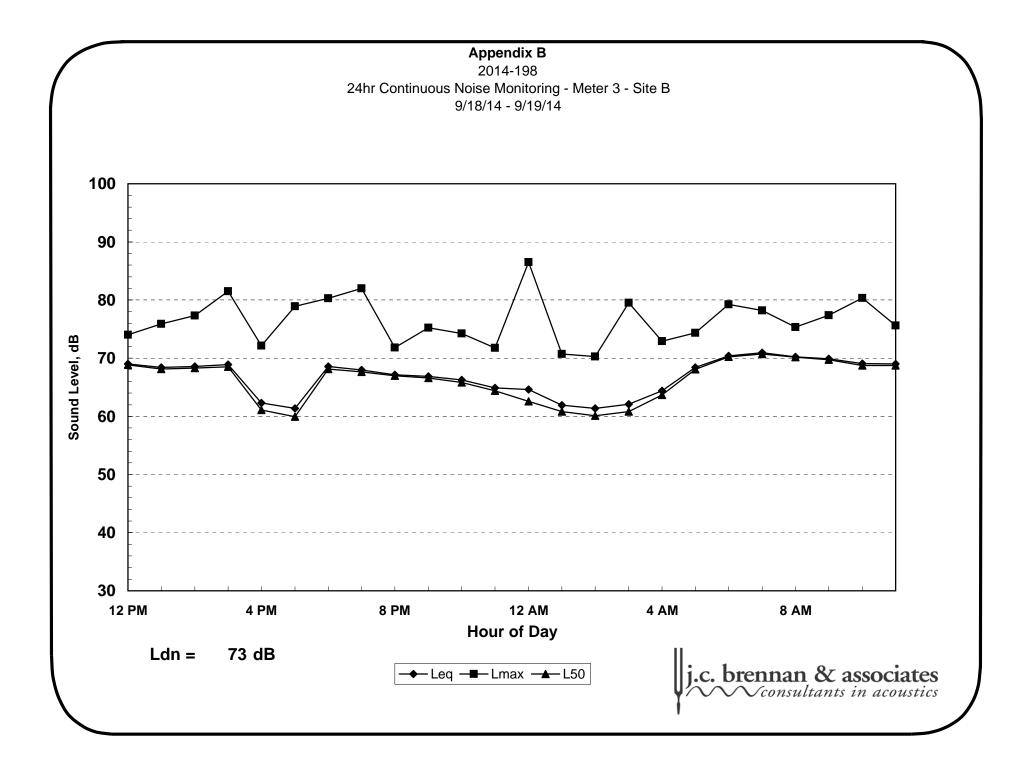
2014-198 24hr Continuous Noise Monitoring - Meter 3 - Site B 9/18/14 - 9/19/14

| Hour | Leq | Lmax | L50 | L90 |
|-------|-----|------|-----|-----|
| 12:00 | 69 | 74 | 69 | 67 |
| 13:00 | 68 | 76 | 68 | 66 |
| 14:00 | 69 | 77 | 68 | 67 |
| 15:00 | 69 | 82 | 69 | 67 |
| 16:00 | 62 | 72 | 61 | 58 |
| 17:00 | 61 | 79 | 60 | 57 |
| 18:00 | 69 | 80 | 68 | 67 |
| 19:00 | 68 | 82 | 68 | 66 |
| 20:00 | 67 | 72 | 67 | 65 |
| 21:00 | 67 | 75 | 67 | 64 |
| 22:00 | 66 | 74 | 66 | 63 |
| 23:00 | 65 | 72 | 64 | 61 |
| 0:00 | 65 | 87 | 63 | 58 |
| 1:00 | 62 | 71 | 61 | 56 |
| 2:00 | 61 | 70 | 60 | 54 |
| 3:00 | 62 | 80 | 61 | 56 |
| 4:00 | 64 | 73 | 64 | 59 |
| 5:00 | 68 | 74 | 68 | 65 |
| 6:00 | 70 | 79 | 70 | 68 |
| 7:00 | 71 | 78 | 71 | 69 |
| 8:00 | 70 | 75 | 70 | 69 |
| 9:00 | 70 | 77 | 70 | 68 |
| 10:00 | 69 | 80 | 69 | 67 |
| 11:00 | 69 | 76 | 69 | 67 |

| | Statistical Summary | | | | | | | |
|------------------|---------------------|------------|------------|-------------------|-----|---------|--|--|
| | Daytime | e (7 a.m ' | e (10 p.m. | e (10 p.m 7 a.m.) | | | | |
| | High | Low | Average | High | Low | Average | | |
| Leq (Average) | 71 | 61 | 68 | 70 | 61 | 66 | | |
| Lmax (Maximum) | 82 | 72 | 77 | 87 | 70 | 76 | | |
| L50 (Median) | 71 | 60 | 67 | 70 | 60 | 64 | | |
| L90 (Background) | 69 | 57 | 66 | 68 | 54 | 60 | | |

| Computed Ldn, dB | 73 |
|--------------------|-----|
| % Daytime Energy | 75% |
| % Nighttime Energy | 25% |

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Appendix B

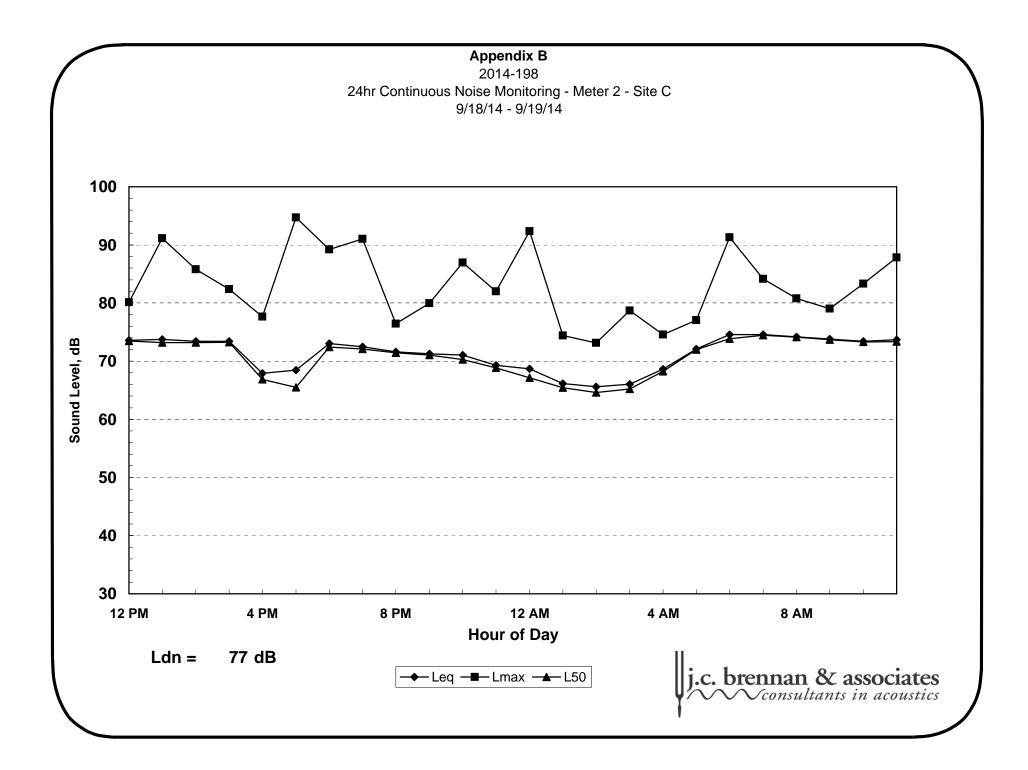
2014-198 24hr Continuous Noise Monitoring - Meter 2 - Site C 9/18/14 - 9/19/14

| Hour | Leq | Lmax | L50 | L90 |
|-------|-----|------|-----|-----|
| 12:00 | 74 | 80 | 73 | 72 |
| 13:00 | 74 | 91 | 73 | 72 |
| 14:00 | 73 | 86 | 73 | 72 |
| 15:00 | 73 | 82 | 73 | 72 |
| 16:00 | 68 | 78 | 67 | 64 |
| 17:00 | 68 | 95 | 65 | 63 |
| 18:00 | 73 | 89 | 72 | 71 |
| 19:00 | 72 | 91 | 72 | 71 |
| 20:00 | 72 | 76 | 71 | 70 |
| 21:00 | 71 | 80 | 71 | 69 |
| 22:00 | 71 | 87 | 70 | 68 |
| 23:00 | 69 | 82 | 69 | 66 |
| 0:00 | 69 | 92 | 67 | 63 |
| 1:00 | 66 | 74 | 65 | 61 |
| 2:00 | 66 | 73 | 65 | 59 |
| 3:00 | 66 | 79 | 65 | 60 |
| 4:00 | 69 | 75 | 68 | 63 |
| 5:00 | 72 | 77 | 72 | 69 |
| 6:00 | 75 | 91 | 74 | 72 |
| 7:00 | 75 | 84 | 74 | 73 |
| 8:00 | 74 | 81 | 74 | 73 |
| 9:00 | 74 | 79 | 74 | 72 |
| 10:00 | 73 | 83 | 73 | 72 |
| 11:00 | 74 | 88 | 73 | 72 |

| | Statistical Summary | | | | | | | |
|------------------|---------------------|---|---------|------|-----|---------|--|--|
| | Daytime | Daytime (7 a.m 10 p.m.) Nighttime (10 p | | | | | | |
| | High | Low | Average | High | Low | Average | | |
| Leq (Average) | 75 | 68 | 73 | 75 | 66 | 70 | | |
| Lmax (Maximum) | 95 | 76 | 84 | 92 | 73 | 81 | | |
| L50 (Median) | 74 | 65 | 72 | 74 | 65 | 68 | | |
| L90 (Background) | 73 | 63 | 70 | 72 | 59 | 65 | | |

| Computed Ldn, dB | 77 |
|--------------------|-----|
| % Daytime Energy | 76% |
| % Nighttime Energy | 24% |

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Appendix C FHWA-RD-77-108 Highway Traffic Noise Prediction Model Data Input Sheet

Project #:2014-197 T Street ResidentialDescription:ExistingLdn/CNEL:LdnHard/Soft:Soft

| Segment | Roadway Name | Segment | ADT | Day % | Eve % | Night % | % Med. Trucks | , | Speed | Distance | Offset (dB) |
|---------|----------------|---------------------------|----------------|-------|-------|---------|------------------|-----|-------|----------|----------------|
| 1 | 35th Street | West of Stockton Blvd. | 2,420 | 83 | | 17 | 1 | 0.5 | 30 | 50 | |
| 2 | Stockton Blvd. | US 50 EB Ramp to T Street | 2,420 | 83 | | 17 | 2 | 0.5 | 30 | 100 | -5 |
| 2 | Stockton Blvd. | South of T Street | 18,770 | 83 | | 17 | 2 | 0.5 | 30 | 75 | -5 |
| 4 | T Street | West of Stockton Blvd. | 9,130 | 83 | | 17 | 2 1 | 0.5 | 30 | 40 | |
| 4 5 | T Street | Stockton Blvd to 37th St. | 9,130 4,640 | 83 | | 17 | 1 | 0.5 | 30 | 40 60 | |
| 6 | T Street | 37th St. to 39th St. | 4,040 6,410 | 83 | | 17 | 1 | 0.5 | 30 | 60 60 | |
| 7 | T Street | East of 39th St. | 6,520 | 83 | | 17 | 1 | 0.5 | 30 | 60 60 | |
| 8 | 39th St. | North of S Street | 0,320 5,350 | 83 | | 17 | 1 | 0.5 | 30 | 60 60 | |
| 9 | 39th St. | S Street to T Street | 5,270 | 83 | | 17 | 1 | 0.5 | 30 | 40 | |
| 10 | 39th St. | South of T Street | 4,010 | 83 | | 17 | 1 | 0.5 | 30 | 40 | |
| 10 | S Street | East of 39th St. | 30 | 83 | | 17 | 1 | 0.5 | 25 | 40 | |
| 12 | S Street | 39th St. to 37 St. | 210 | 83 | | 17 | 1 | 0.5 | 25 | 40 | |
| 13 | 37th St. | T Street to S Street | 300 | 83 | | 17 | 1 | 0.5 | 25 | 40 | |
| 14 | Gerber Ave. | South of T Street | 360 | 83 | | 17 | 1 | 0.5 | 25 | 40 | |

Appendix C FHWA-RD-77-108 Highway Traffic Noise Prediction Model Predicted Levels

Project #: 2014-197 T Street Residential Description: Existing

Ldn/CNEL: Ldn

Hard/Soft: Soft

| | | | | Medium | Heavy | | | |
|---------|----------------|---------------------------|-------|--------|--------|-------|--------|-------|
| Segment | Roadway Name | Segment | Autos | Trucks | Trucks | Local | Hwy 50 | Total |
| | | | | | | | | |
| 1 | 35th Street | West of Stockton Blvd. | 55 | 46 | 50 | 56.7 | 70.0 | 70.2 |
| 2 | Stockton Blvd. | US 50 EB Ramp to T Street | 54 | 47 | 49 | 55.6 | 70.0 | 70.2 |
| 3 | Stockton Blvd. | South of T Street | 61 | 55 | 56 | 63.2 | | 63.2 |
| 4 | T Street | West of Stockton Blvd. | 62 | 53 | 57 | 63.9 | 65.0 | 67.5 |
| 5 | T Street | Stockton Blvd to 37th St. | 57 | 47 | 52 | 58.3 | 67.0 | 67.5 |
| 6 | T Street | 37th St. to 39th St. | 58 | 49 | 53 | 59.7 | | 59.7 |
| 7 | T Street | East of 39th St. | 58 | 49 | 53 | 59.8 | | 59.8 |
| 8 | 39th St. | North of S Street | 57 | 48 | 52 | 58.9 | 70.0 | 70.3 |
| 9 | 39th St. | S Street to T Street | 60 | 51 | 55 | 61.5 | | 61.5 |
| 10 | 39th St. | South of T Street | 59 | 49 | 54 | 60.3 | | 60.3 |
| 11 | S Street | East of 39th St. | 35 | 27 | 32 | 37.2 | | 37.2 |
| 12 | S Street | 39th St. to 37 St. | 44 | 35 | 40 | 45.7 | 72.0 | 72.0 |
| 13 | 37th St. | T Street to S Street | 45 | 37 | 42 | 47.2 | 66.0 | 66.1 |
| 14 | Gerber Ave. | South of T Street | 46 | 38 | 42 | 48.0 | | 48.0 |

Appendix C FHWA-RD-77-108 Highway Traffic Noise Prediction Model Data Input Sheet

Project #:2014-197 T Street ResidentialDescription:Existing + ProjectLdn/CNEL:LdnHard/Soft:Soft

| Segment | Roadway Name | Segment | ADT | Day % | Eve % | Night % | % Med. Trucks | , | Speed | Distance | Offset (dB) |
|---------|-----------------|---------------------------|--------|-------|-------|---------|------------------|-----|-------|----------|----------------|
| | OF the Other at | West of Oteslaters Divid | 0.400 | 00 | | 47 | A | 0.5 | 20 | 50 | |
| 1 | 35th Street | West of Stockton Blvd. | 2,420 | 83 | | 17 | 1 | 0.5 | 30 | 50 | _ |
| 2 | Stockton Blvd. | US 50 EB Ramp to T Street | 20,510 | 83 | | 17 | 2 | 0.5 | 30 | 100 | -5 |
| 3 | Stockton Blvd. | South of T Street | 19,520 | 83 | | 17 | 2 | 0.5 | 30 | 75 | |
| 4 | T Street | West of Stockton Blvd. | 9,360 | 83 | | 17 | 1 | 0.5 | 30 | 40 | |
| 5 | T Street | Stockton Blvd to 37th St. | 7,320 | 83 | | 17 | 1 | 0.5 | 30 | 60 | |
| 6 | T Street | 37th St. to 39th St. | 6,510 | 83 | | 17 | 1 | 0.5 | 30 | 60 | |
| 7 | T Street | East of 39th St. | 6,590 | 83 | | 17 | 1 | 0.5 | 30 | 60 | |
| 8 | 39th St. | North of S Street | 5,500 | 83 | | 17 | 1 | 0.5 | 30 | 60 | |
| 9 | 39th St. | S Street to T Street | 5,360 | 83 | | 17 | 1 | 0.5 | 30 | 40 | |
| 10 | 39th St. | South of T Street | 4,050 | 83 | | 17 | 1 | 0.5 | 30 | 40 | |
| 11 | S Street | East of 39th St. | 30 | 83 | | 17 | 1 | 0.5 | 25 | 40 | |
| 12 | S Street | 39th St. to 37 St. | 370 | 83 | | 17 | 1 | 0.5 | 25 | 40 | |
| 13 | 37th St. | T Street to S Street | 920 | 83 | | 17 | 1 | 0.5 | 25 | 40 | |
| 14 | Gerber Ave. | South of T Street | 450 | 83 | | 17 | 1 | 0.5 | 25 | 40 | |

Appendix C FHWA-RD-77-108 Highway Traffic Noise Prediction Model Predicted Levels

Project #:2014-197 T Street ResidentialDescription:Existing + ProjectLdn/CNEL:LdnHard/Soft:Soft

| Segment | Roadway Name | Segment | Autos | Medium Trucks | Heavy Trucks | Local | Hwy 50 | Total |
|---------|----------------|---------------------------|-------|------------------|-----------------|-------|--------|-------|
| | • | | | | | | | |
| 1 | 35th Street | West of Stockton Blvd. | 55 | 46 | 50 | 56.7 | 70.0 | 70.2 |
| 2 | Stockton Blvd. | US 50 EB Ramp to T Street | 55 | 49 | 50 | 56.7 | 70.0 | 70.2 |
| 3 | Stockton Blvd. | South of T Street | 62 | 55 | 56 | 63.4 | | 63.4 |
| 4 | T Street | West of Stockton Blvd. | 62 | 53 | 57 | 64.0 | 65.0 | 67.5 |
| 5 | T Street | Stockton Blvd to 37th St. | 59 | 49 | 54 | 60.3 | 67.0 | 67.8 |
| 6 | T Street | 37th St. to 39th St. | 58 | 49 | 53 | 59.8 | | 59.8 |
| 7 | T Street | East of 39th St. | 58 | 49 | 53 | 59.8 | | 59.8 |
| 8 | 39th St. | North of S Street | 58 | 48 | 52 | 59.0 | 70.0 | 70.3 |
| 9 | 39th St. | S Street to T Street | 60 | 51 | 55 | 61.6 | | 61.6 |
| 10 | 39th St. | South of T Street | 59 | 49 | 54 | 60.3 | | 60.3 |
| 11 | S Street | East of 39th St. | 35 | 27 | 32 | 37.2 | | 37.2 |
| 12 | S Street | 39th St. to 37 St. | 46 | 38 | 42 | 48.1 | 72.0 | 72.0 |
| 13 | 37th St. | T Street to S Street | 50 | 42 | 46 | 52.1 | 66.0 | 66.2 |
| 14 | Gerber Ave. | South of T Street | 47 | 39 | 43 | 49.0 | | 49.0 |

Appendix D FHWA Traffic Noise Prediction Model (FHWA-RD-77-108) Noise Prediction Worksheet

Project Information:

| Job Number: | 2014-198 |
|---------------|----------------------|
| Project Name: | T Street Residential |
| Roadway Name: | US 50 |

Traffic Data:

| Existing |
|----------|
| 230,000 |
| 75 |
| 25 |
| 2 |
| 2 |
| 65 |
| Soft |
| |

Traffic Noise Levels:

| | | | | | L _{dn} , d | ;в | |
|-----------|------------------------------------|----------|-------------|-------|---------------------|--------|-------|
| | | | | | Medium | Heavy | |
| Location: | Description | Distance | Offset (dB) | Autos | Trucks | Trucks | Total |
| A | 24-hr Site A - Measured 72 dBA Ldn | 160 | -7.0 | 71 | 60 | 64 | 72 |
| В | 24-hr Site B - Measured 73 dBA Ldn | 285 | -2.5 | 72 | 61 | 65 | 73 |
| С | 24-hr Site C - Measured 77 dBA Ldn | 320 | 2.6 | 76 | 65 | 69 | 77 |

Traffic Noise Contours (No Calibration Offset):

| L _{dn} Contour, dB | Distance from Centerline, (ft) |
|-----------------------------|--------------------------------|
| 75 | 298 |
| 70 | 643 |
| 65 | 1385 |
| 60 | 2983 |

Notes:

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Appendix D FHWA Traffic Noise Prediction Model (FHWA-RD-77-108) Noise Prediction Worksheet

Project Information:

| Job Number: 2 | 2014-198 |
|-----------------|--------------------|
| Project Name: 1 | Street Residential |
| Roadway Name: l | JS 50 |

Traffic Data:

| Year: | Cumulative - Sac County GP |
|---------------------------------|----------------------------|
| Average Daily Traffic Volume: | 275,700 |
| Percent Daytime Traffic: | 75 |
| Percent Nighttime Traffic: | 25 |
| Percent Medium Trucks (2 axle): | 2 |
| Percent Heavy Trucks (3+ axle): | 2 |

Assumed Vehicle Speed (mph): 65 Intervening Ground Type (hard/soft): **Soft**

Traffic Noise Levels:

| | | | | L _{dn} , dB | | | |
|-----------|--------------|----------|-------------|----------------------|--------|--------|-------|
| | | | | | Medium | Heavy | |
| Location: | Description | Distance | Offset (dB) | Autos | Trucks | Trucks | Total |
| 1 | SF Backyards | 170 | -7 | 71 | 61 | 64 | 72 |
| 2 | MF Roof Pool | 285 | 2 | 77 | 66 | 70 | 78 |
| 3 | SF Facades | 170 | 0 | 78 | 68 | 71 | 79 |
| 4 | MF Facades | 200 | 2 | 79 | 69 | 72 | 80 |

Traffic Noise Contours (No Calibration Offset):

| L _{dn} Contour, dB | Distance from Centerline, (ft) |
|-----------------------------|--------------------------------|
| 75 | 337 |
| 70 | 725 |
| 65 | 1562 |
| 60 | 3366 |

Notes:



| / | | e Prediction Model (FHWA-RD-77-108) tiveness Prediction Worksheet | |
|---|----------------------|--|--|
| | Project Information: | Job Number: 2014-198 Project Name: T Street Residential Roadway Name: US 50 Location(s): SF Backyards | |
| | Noise Level Data: | Year: Cumulative - Sac County GP | |
| | | Auto L _{dn} , dB: 78 | |
| | | Medium Truck L _{dn} , dB: 68 | |
| | | Heavy Truck L _{dn} , dB: 71 | |
| | Site Geometry: | Receiver Description: SF Backyards Centerline to Barrier Distance (C_1) : 120 Barrier to Receiver Distance (C_2) : 50 Automobile Elevation: 15 Medium Truck Elevation: 17 Heavy Truck Elevation: 23 Pad/Ground Elevation at Receiver: 0 Receiver Elevation ¹ : 5 Base of Barrier Elevation: 15 Starting Barrier Height 8 | |
| | | | |

Barrier Effectiveness:

| Top of Barrier | Barrier | | L _{dn} Medium | , dB Heavy | | Barrier B | reaks Line of Medium | Sight to Heavy |
|-------------------|--------------------------|-------|---------------------------|---------------|-------|-----------|-------------------------|-------------------|
| Elevation (ft) | Height ² (ft) | Autos | Trucks | Trucks | Total | Autos? | Trucks? | Trucks? |
| 23 | 8 | 65 | 54 | 59 | 66 | Yes | Yes | Yes |
| 24 | 9 | 64 | 54 | 58 | 66 | Yes | Yes | Yes |
| 25 | 10 | 64 | 54 | 58 | 65 | Yes | Yes | Yes |
| 26 | 11 | 64 | 53 | 57 | 65 | Yes | Yes | Yes |
| 27 | 12 | 64 | 53 | 57 | 65 | Yes | Yes | Yes |
| 28 | 13 | 63 | 52 | 57 | 64 | Yes | Yes | Yes |
| 29 | 14 | 63 | 52 | 57 | 64 | Yes | Yes | Yes |
| 30 | 15 | 62 | 52 | 56 | 64 | Yes | Yes | Yes |
| 31 | 16 | 62 | 52 | 56 | 64 | Yes | Yes | Yes |

Notes: 1.S

1.Standard receiver elevation is five feet above grade/pad elevations at the receiver location(s)

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| | se Prediction Model (FHWA-RD-77-108) activeness Prediction Worksheet | |
|----------------------|--|--|
| Project Information: | Job Number: 2014-198 Project Name: T Street Residential Roadway Name: US 50 Location(s): MF Roof Pool | |
| Noise Level Data: | Year: Cumulative - Sac County GP | |
| | Auto L _{dn} , dB: 77 | |
| | Medium Truck L _{dn} , dB: 66 | |
| | Heavy Truck L _{dn} , dB: 70 | |
| Site Geometry: | Receiver Description: MF Roof Pool Centerline to Barrier Distance (C_1): 200 Barrier to Receiver Distance (C_2): 50 Automobile Elevation: 15 Medium Truck Elevation: 17 Heavy Truck Elevation: 23 Pad/Ground Elevation at Receiver: 50 Receiver Elevation ¹ : 55 Base of Barrier Elevation: 50 Starting Barrier Height 8 | |
| | Starting Barrier Height 8 | |

Barrier Effectiveness:

| Top of Barrier | Barrier | | L _{dn} Medium | , dB Heavy | | Barrier B | reaks Line of Medium | Sight to Heavy |
|-------------------|--------------------------|-------|---------------------------|---------------|-------|-----------|-------------------------|-------------------|
| Elevation (ft) | Height ² (ft) | Autos | Trucks | Trucks | Total | Autos? | Trucks? | Trucks? |
| 58 | 8 | 66 | 55 | 60 | 67 | Yes | Yes | Yes |
| 59 | 9 | 65 | 55 | 59 | 67 | Yes | Yes | Yes |
| 60 | 10 | 65 | 54 | 59 | 66 | Yes | Yes | Yes |
| 61 | 11 | 64 | 54 | 58 | 65 | Yes | Yes | Yes |
| 62 | 12 | 64 | 53 | 57 | 65 | Yes | Yes | Yes |
| 63 | 13 | 63 | 53 | 57 | 65 | Yes | Yes | Yes |
| 64 | 14 | 63 | 52 | 56 | 64 | Yes | Yes | Yes |
| 65 | 15 | 63 | 52 | 56 | 64 | Yes | Yes | Yes |
| 66 | 16 | 62 | 52 | 56 | 64 | Yes | Yes | Yes |

Notes: 1.Standard receiver elevation is five feet above grade/pad elevations at the receiver location(s)

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APPENDIX E

TRANSPORTATION IMPACT STUDY

Prepared for City of Sacramento





Fehr / Peers

February 25, 2015

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EXECUTIVE SUMMARY

This study analyzes the transportation impacts associated with the proposed Stockton Boulevard/T Street Mixed-Use project, which would consist of the following:

- Demolition of a 120,000 square-foot vacant office building (and associated surface parking areas) located in the northeast quadrant of the Stockton Boulevard/T Street intersection.
- Construction of a mixed-use project consisting of the following land uses:
 - o 214 apartment units
 - 24 single-family dwelling units
 - o 6,000 square feet of retail

The potential off-site traffic impacts of the project are analyzed under existing and cumulative conditions. Impacts to transit, bicycle, parking, and pedestrian circulation are also evaluated. Access to the project site is analyzed for all modes of travel. Temporary impacts during project construction are also evaluated.

Since this project is consistent with the City's 2030 General Plan, the cumulative impacts on roadway segments, freeway segments, transit, bicycle facilities, pedestrian circulation, and parking from development associated with the General Plan were identified and analyzed in the Master EIR, and this study reviews such issues on a project-specific basis only. The proposed project qualifies as a Transit Priority Project (TPP) under Senate Bill (SB) 375. TPPs may be reviewed through a Sustainable Communities Environmental Assessment (SCEA), which eliminates the need for certain environmental reviews including analysis of the regional transportation network (i.e., US 50).

EXISTING CONDITIONS

Roadway System

Six intersections along the Stockton Boulevard, T Street, and 39th Street corridors were selected for analysis for weekday AM and PM peak hours. All intersections were analyzed using a state-of-the-practice SimTraffic micro-simulation model. Each intersection operates at an acceptable level of service (LOS) E or better during both peak hours. The northbound direction of Stockton Boulevard is congested during the PM peak period due, in part, to ramp metering of the US 50/Stockton Boulevard westbound loop on-ramp.

The Stockton Boulevard/T Street/Gerber Avenue intersection is complex based on its lane configurations, traffic signal timings, turn movement prohibitions, and volume of vehicles, bicyclists, and pedestrians. Refer to Figure 5 for an illustration of existing conditions at this intersection, which operates at Level of Service (LOS) C during the AM peak hour and LOS E during the PM peak hour.

Transit System

Public transit service within the study area is provided by light rail and bus. The 39th Street Light Rail Station, which is a stop along the Gold line, is less than ½-mile from the project site. Regional Transit (RT) bus routes 38, 212, 213, and 214 include stops within a ½-mile walk of the project site. The Capital City Hospital Shuttle service stops at the 39th Street Light Rail station. This free shuttle transports employees, patients, and visitors to the Mercy, Sutter, UC Davis Medical Centers located in Midtown and East Sacramento.

Bicycle/Pedestrian System

The study area includes a variety of bicycle and pedestrian facilities including Class II bike lanes on portions of T Street, sidewalks along most public streets, and crosswalks at the signalized Stockton Boulevard/T Street intersection.

EXISTING PLUS PROJECT CONDITIONS

The proposed project would generate 83 new AM peak hour vehicle trips, 109 new PM peak hour vehicle trips, and 1,180 new average daily vehicle trips. These are new trips that are not currently on the roadway network. These estimates account for internal trips between the residential and retail uses and external trips made by walking, bicycling, and transit.

The project would cause the average delay at the Stockton Boulevard/T Street intersection to increase from 56 to 71 seconds per vehicle during the PM peak hour. Since LOS E operations would be maintained and are considered acceptable at this location, the added delay, in and of itself, is not considered a significant impact. However, the effects of the project on increased vehicle queuing and the ability to safely pass through the Stockton Boulevard/T Street intersection are considered significant.

CUMULATIVE CONDITIONS

The Stockton Boulevard/T Street intersection would operate at LOS F during the PM peak hour under Cumulative Plus Project Conditions. This occurs as a result of background traffic growth. Project impacts at this intersection under cumulative conditions are considered less than significant because the No Project condition (i.e., office building remains and is occupied by tenants) would experience more delays due to its greater trip generation when compared to the proposed project.

PROJECT ACCESS AND ON-SITE CIRCULATION

A comprehensive review of project access was performed including driveways, proposed on-street parking, internal circulation, and other considerations. Several recommendations were offered to improve access to the project site for all users, conform with City design standards, and better accommodate circulation within the project site. These recommendations are illustrated on **Figure ES-1**.

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Figure ES-1

Recommendations



Project Site

IMPACTS AND MITIGATION MEASURES

The project would cause two project-specific and cumulatively considerable significant impacts on the transportation system. Each impact is described below followed by a recommended mitigation measure, which would reduce each impact to less than significant.

<u>Impact TR-1</u>: The addition of project traffic would cause adverse queuing effects and safety concerns in the southbound left-turn lane at the Stockton Boulevard/T Street intersection.

Mitigation Measure TR-1

The project applicant shall work with the City of Sacramento to modify the traffic signal at the Stockton Boulevard/T Street intersection to operate the northbound and southbound left-turns with protected phasing.

Refer to Table 11 for a detailed discussion of Mitigation Measure TR-1 including timing, responsibility, and operational benefits. The project would not cause any adverse effects at other study intersections.

<u>Impact TR-2</u>: Construction of the proposed project could potentially cause a temporary but prolonged impact due to construction-related travel activities.

Mitigation TR-2

The project applicant shall develop a Construction Traffic Management Plan to the satisfaction of the City's Transportation Department. The plan would include items such as: the number and size of trucks per day, expected arrival/departure times, truck circulation patterns, location of truck staging areas, location/amount of employee parking, and the proposed use of traffic control/partial street closures on public streets. The overall goal of the Construction Traffic Management Plan would be to minimize traffic impacts to public streets and maintain a high level of safety for all roadway users. The Construction TMP shall adhere to the following performance standards throughout project construction:

- 1) Delivery trucks do not idle/stage on Stockton Boulevard and T Street.
- *2)* With the exception of trucks coming from local destinations via 39th Street, all delivery trucks shall use Stockton Boulevard to access the site.
- 3) Any lane closures on northbound Stockton Boulevard during the demolition of the existing office building or proposed project construction are limited to a single lane during off-peak hours (9:00 AM to 2:30 PM).
- 4) Roadways, sidewalks, crosswalks, and bicycle facilities shall be maintained clear of debris (e.g., rocks) that could otherwise impede travel and impact public safety.

Table ES-1 summarizes the evaluation of project impacts on all travel modes, emergency access, and construction-related activities. With implementation of Mitigation Measures TR-1 and TR-2, all impacts are considered less than significant.

| TABLE ES-1: SUMMARY OF IMPACTS AND MITIGATION MEASURES | | | | | | |
|---|---|------------|----------------------|--------------------------|--|--|
| Impact Type | Discussion | Mitigation | | Residual Significance | | |
| Roadway System | Adverse queuing effects and safety concerns in the southbound left-turn lane at the Stockton Boulevard/T Street intersection. | Yes | TR-1 LTS None LTS | | | |
| Bicycle Network | Continuous Class II bike lanes present on portions of T Street. On-site bicycle parking provided. | No | None | LTS | | |
| Pedestrian Facilities | Continuous sidewalks and crosswalks are present (including to bus/light rail stops). | No | None | LTS | | |
| Transit System and Facilities | 39 th Street light rail (Gold Line) station, and multiple bus stops less than ½-mile walk from project site. | No | None | LTS | | |
| Emergency Vehicle Access | Emergency vehicle pre-emption provided at Stockton Boulevard/T Street intersection. | No | None | LTS | | |
| Construction-Related | Temporary, but prolonged traffic impacts could occur due to construction-related activities. | Yes | TR-2 | LTS | | |
| LTS = Less Than Significant. Source: Fehr & Peers, 2015. | | | | | | |

1. INTRODUCTION

PURPOSE

This study analyzes the transportation impacts associated with the proposed Stockton Boulevard/T Street Mixed-Use project, which would consist of the following:

- Demolition of a 120,000 square-foot vacant office building (and associated surface parking areas) located in the northeast quadrant of the Stockton Boulevard/T Street intersection.
- Construction of a mixed-use project consisting of the following land uses:
 - o 214 apartment units
 - 24 single-family dwelling units
 - 6,000 square feet of retail

The potential off-site traffic impacts of the project are analyzed under existing and cumulative conditions. Impacts to transit, bicycle, parking, and pedestrian circulation are also evaluated. Access to the project site is analyzed for all modes of travel. Temporary impacts during project construction are also evaluated.

The cumulative impacts on roadway segments, freeway segments, transit, bicycle facilities, pedestrian circulation, and parking from development associated with the general plan were identified and analyzed in the Master EIR, and this study reviews such issues on a project-specific basis only. Project impacts on intersections were included in the traffic study to determine the project's conformity with the Mobility Element of the 2030 General Plan and to confirm that no substantial new or additional information shows that the impacts on the roadway system are more significant than as described in the Master EIR.

The proposed project qualifies as a Transit Priority Project (TPP) under Senate Bill (SB) 375. Environmental documents for TPPs are not required to reference, describe or discuss: 1) growth inducing impacts, 2) impacts from car and light-duty truck trips on climate change or regional transportation network, or a 3) reduced density alternative to the project. TPPs may be reviewed through a Sustainable Communities Environmental Assessment (SCEA). Accordingly, it was not necessary to analyze project effects on US 50 within the study area because this freeway is part of the regional transportation network. Refer to Page 5 for further details.

The project is situated within the green area of Exhibit 1 of the City's Climate Action Plan (CAP). Projects located within the green area are known to generate 35 percent less Vehicle Miles of Travel (VMT) per capita when compared to the statewide average, which is one of the conditions that must be met to conclude that the project is consistent with the City's CAP. Since the project is located within the green area, no further of VMT is presented in report. City's website analysis this Refer to the (at http://portal.cityofsacramento.org/Community-Development/Resources/Online-Library/Sustainability) for additional information on this topic. The project is also being evaluated for its consistency with SACOG's Sustainable Communities Strategy (SCS). Projects that achieve this distinction are granted certain CEQA streamlining benefits under Senate Bill 375.

STUDY AREA

In urban environments such as the study area, roadway capacity is governed by the operations of intersections. For this reason and because roadway segments were included in the traffic analysis for the 2030 General Plan, the City of Sacramento determines impacts on the roadway system based upon the operations of intersections.

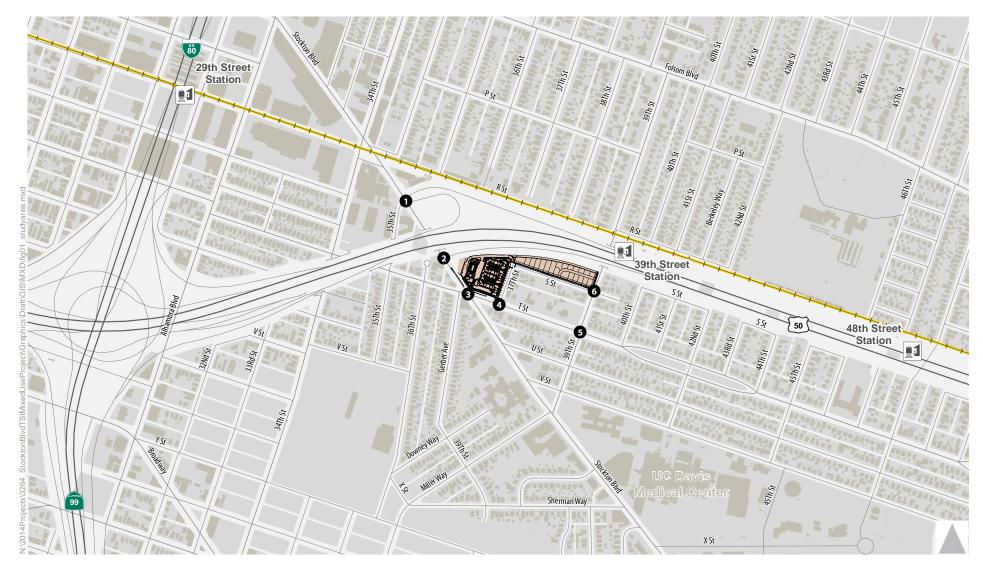
The study area includes the following six intersections along the Stockton Boulevard, T Street, and 39th Street corridors. These intersections were selected based on their proximity to the project site, expected usage by project traffic, and susceptibility for being impacted. The list was reviewed and approved by the City's Public Works Department. Refer to **Figure 1** for a map showing the study intersections. The study area also includes bicycle, pedestrian, and transit facilities within the project vicinity.

- 1. Stockton Boulevard/35th Street/US 50 WB Ramps
- 2. Stockton Boulevard/US 50 EB On-ramp
- 3. Stockton Boulevard/T Street/Gerber Avenue
- 4. T Street/37th Street
- 5. T Street/39th Street
- 6. S Street/39th Street

PROJECT DESCRIPTION

Figure 2 shows the project site plan (*Stockton Boulevard and T Street Mixed-Use Project*, RSC Engineering 1/22/2015). The project land uses are described below.

- The apartment building would be situated nearest the Stockton Boulevard/T Street intersection in a mid-rise (five-floor) configuration. Below ground parking consisting of 230 spaces would be provided. Vehicular access to the apartments would be provided as follows:
 - Right-turn only driveway located on Stockton Boulevard approximately 100 feet north of the Stockton Boulevard/T Street intersection. In conjunction, a narrow raised median would be constructed on Stockton Boulevard to prohibit left-turns at this driveway.
 - \circ $\;$ Full-access driveway located at the intersection of S Street and 37 th Street.
- The 24 single-family dwelling units would be situated along S Street between 37th and 39th Streets. These units would feature vehicular driveways on S Street and also along a new internal street that extends from S Street to 39th Street.
- Ground floor retail (6,000 square feet) would be situated along T Street directly east of Stockton Boulevard. Parking for this use is proposed via eight (8) traditional angled parking spaces, which would require removal and reconstruction of existing curb, gutter, and sidewalk along the project frontage. In addition, a narrow raised median would be constructed on T Street to physically prohibit wrong-way vehicle entry into these spaces.



Study Intersection
 Project Site
 LRT Gold Line Tracks

Figure 1

Study Area



39th St. LRT Station

Station Project Site

Þ

Figure 2

Project Site Plan

The project would not alter the lane configurations at the Stockton Boulevard/T Street intersection. However, by virtue of constructing narrow raised medians as described above, movements to/from adjacent businesses on Stockton Boulevard and T Street would also be restricted to right-turns. Although signage is not present to prohibit u-turns at the Stockton Boulevard/T Street intersection, field observations indicate that such movements are difficult to accomplish given the configuration of the intersection.

ANALYSIS SCENARIOS

The following scenarios are analyzed in this study:

- Existing Conditions represents the baseline condition, upon which project impacts are measured. The baseline condition represents conditions in Fall 2014 (i.e., traffic counts were collected in October 2014).
- Existing Plus Project Conditions reflects changes in travel conditions associated with implementation of the proposed project.
- Cumulative Plus Project Conditions Analyzes conditions for a cumulative scenario, which includes reasonably foreseeable land uses and proposed project implementation. Refer to Chapter 4 for a discussion of specific assumptions for this scenario.

The proposed project qualifies as a Transit Priority Project (TPP) under Senate Bill (SB) 375. Public Resources Code section 21155 sets forth the requirements for a project to qualify as a TPP. The following qualifications must be met to be considered a TPP:

- 1. At least 50 percent of total building square footage for residential use OR if 26-50% of total building square footage is nonresidential, a minimum FAR of 0.75;
- 2. Minimum net density of 20 du/acre;
- 3. Within 0.5 miles of major transit stop or high-quality transit corridor included in the regional transportation plan (No parcel more than 25% further, and less than 10% of units or no more than 100 units further than 0.5 miles); and
- 4. Consistent with the use designation, density, building intensity, and applicable policies of an SCS or APS.

Criterion 1 is met since all but 6,000 square feet of the 240,000 square foot apartment building will be dedicated to residential. Criterion 2 is met since 238 dwelling units are proposed on the 4.92-acre site (48 units per gross acre implies the net density will exceed 20 units per acre). Criterion 3 is met since the 39th Street light rail station is situated within ½-mile of the project site. Criterion 4 is met since the project is consistent with the existing General Plan designation of "Urban Corridor Low" and located within a Transit Priority Area in the SACOG 2035 MTP/SCS.

Guidance for environmental reviews of TPPs is provided at: <u>http://sacog.org/mtpscs/implementation/</u>. Environmental documents for TPPs are not required to reference, describe or discuss: 1) growth inducing

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impacts, 2) impacts from car and light-duty truck trips on climate change or regional transportation network, or a 3) reduced density alternative to the project. TPPs may be reviewed through a Sustainable Communities Environmental Assessment (SCEA). (Pub. Res. Code, § 21155.2, subd. (b)). The standard of review for the SCEA is the "substantial evidence" standard, which is deferential to the agency. Thus, once an SCEA is deemed appropriate, the burden of proof for a legal challenge to the agency's analysis is presumed to be adequate and the burden of proof is on a petitioner/plaintiff to demonstrate otherwise.

According to the above, it was not necessary to analyze project effects on the US 50 freeway within the study area because this freeway is part of the regional transportation network.

ANALYSIS METHODOLOGY

Traffic operations at all study intersections were analyzed for weekday AM and PM peak hour conditions using procedures and methodologies contained in the *Highway Capacity Manual* (Transportation Research Board, 2010) for calculating delay at intersections. These methodologies were applied using the SimTraffic software program, which considers the effects of lane utilization, turn pocket storage lengths, upstream/downstream queue spillbacks, and coordinated signal timings on intersection queuing and delays. The SimTraffic model was validated against observed queues. Reported results are based on an average of 10 runs. The following procedures and assumptions were applied in the development of the SimTraffic model:

- Roadway geometric data were gathered using aerial photographs and field observations.
- Peak hour traffic volumes were entered into the model according to the peak hour of the study area.
- The peak hour factor (PHF) was set at 1.0 in accordance with City of Sacramento Traffic Impact Study Guidelines.
- The counted pedestrian and bicycle volumes were entered into the model according to the peak hour measurements.
- Signal phasing and timings were based on existing signal timing plans provided by the City of Sacramento and field observations.
- Speeds for the model network were based on the posted speed limits.

Level of service is a qualitative measure of traffic operating conditions whereby a letter grade, from A (the best) to F (the worst), is assigned. These grades represent the perspective of drivers and are an indication of the comfort and convenience associated with driving. In general, LOS A represents free-flow conditions with no congestion, and LOS F represents severe congestion and delay under stop-and-go conditions. **Table 1** displays the average delay ranges associated with each LOS category.

| Level of Service | Average Control Delay (seconds/vehicle) ¹ | | |
|------------------|--|--------------|--|
| | Signalized | Unsignalized | |
| А | 0 - 10.0 | 0 - 10.0 | |
| В | 10.1 - 20.0 | 10.1 – 15.0 | |
| С | 20.1 - 35.0 | 15.1 – 25.0 | |
| D | 35.1 – 55.0 | 25.1 – 35.0 | |
| E | 55.1 - 80.0 | 35.1 – 50.0 | |
| F | > 80.0 | > 50.0 | |

Source: Fehr & Peers, 2015

For signalized intersections, the LOS is based on the average delay experienced by all vehicles passing through the intersection. For side-street stop controlled intersections, the delay and LOS for the worst case movement is reported along with the average delay for the entire intersection.

LEVEL OF SERVICE STANDARDS

The Mobility Element of the City of Sacramento's 2030 General Plan outlines goals and policies that coordinate the transportation and circulation system with planned land uses. The following LOS policy is relevant to this study:

Policies:

- **M 1.2.2** The City shall allow for flexible Level of Service (LOS) standards, which will permit increased densities and mix of uses to increase transit ridership, biking, and walking, which decreases auto travel, thereby reducing air pollution, energy consumption, and greenhouse gas emissions.
 - a. Core Area Level of Service Exemption—LOS F conditions are acceptable during peak hours in the Core Area bounded by C Street, the Sacramento River, 30th Street, and X Street. If a Traffic Study is prepared and identifies a LOS impact that would otherwise be considered significant to a roadway or intersection that is in the Core Area as described above, the project would not be required in that particular instance to widen roadways in order for the City to find project conformance with the General Plan. Instead, General Plan conformance could still be found if the project provides improvements to other parts of the citywide transportation system in order to improve transportation-system-wide roadway capacity, to make intersection improvements, or

to enhance non-auto travel modes in furtherance of the General Plan goals. The improvements would be required within the project site vicinity or within the area affected by the project's vehicular traffic impacts. With the provision of such other transportation infrastructure improvements, the project would not be required to provide any mitigation for vehicular traffic impacts to road segments in order to conform to the General Plan. This exemption does not affect the implementation of previously approved roadway and intersection improvements identified for the Railyards or River District planning areas.

- b. Level of Service Standards for Multi-Modal Districts The City shall seek to maintain the following standards in multi-modal districts including the Central Business District, areas within ¹/₂ mile walking distance of light rail stations, and in areas designated for urban scale development (Urban Centers, Urban Corridors, and Urban Neighborhoods as designated in the Land Use and Urban Form Diagram). These areas are characterized by frequent transit service, enhanced pedestrian and bicycle systems, a mix of uses, and higher-density development.
 - Maintain operations on all roadways and intersections at LOS A-E at all times, including peak travel times, unless maintaining this LOS would, in the City's judgment, be infeasible and/or conflict with the achievement of other goals. LOS F conditions may be acceptable, provided that provisions are made to improve the overall system and/or promote non-vehicular transportation and transit as part of a development project or a City-initiated project.
- c. Base Level of Service Standard The City shall seek to maintain the following standards for all areas outside of multi-modal districts:
 - Maintain operations on all roadways and intersections at LOS A-D at all times, including peak travel times, unless maintaining this LOS would, in the City's judgment, be infeasible and/or conflict with the achievement of other goals. LOS E or F conditions may be accepted, provided that provisions are made to improve the overall system and/or promote non-vehicular transportation as part of a development project or Cityinitiated project.
- M 1.2.2 applies to the study area intersections as follows:
 - Since the project site and all six study intersections are located within a ¹/₂-mile walk of the 29th Street or 39th Street light rail stations, LOS E is considered an acceptable LOS for this study. As noted above, the City may conclude that maintaining LOS E conditions may be infeasible and/or conflict with the achievement of other goals. In such instances, LOS F conditions may be acceptable, provided that provisions are made to improve the overall system and/or promote non-vehicular transportation and transit as part of a development project or a City-initiated project.

SIGNIFICANCE CRITERIA

The following describes the significance criteria used to identify project-specific and cumulatively considerable impacts to the transportation system.

Intersections

Impacts to the roadway system are considered significant if:

- The traffic generated by the project degrades LOS from acceptable (without the project) to unacceptable (with the project);
- The LOS (without project) is already (or projected to be) unacceptable and project generated traffic increases the average vehicle delay by 5 seconds or more.

The project site and all six study intersections are located within a ¹/₂-mile walk of the 29th Street or 39th Street light rail stations. Accordingly, the study area is situated within a Multi-Modal District. According to Policy M 1.2.2(b), these intersections should:

Maintain operations LOS A-E at all times, including peak travel times, unless maintaining this LOS would, in the City's judgment, be infeasible and/or conflict with the achievement of other goals. LOS F conditions may be acceptable, provided that provisions are made to improve the overall system and/or promote non-vehicular transportation and transit as part of a development project or a City-initiated project.

Transit

Impacts to the transit system are considered significant if the Proposed Project would:

- Adversely affect public transit operations; or
- Fail to adequately provide access to transit.

Bicycle Facilities

Impacts to bicycle facilities are considered significant if the Proposed Project would:

- Adversely affect existing or planned bicycle facilities; or
- Fail to adequately provide for access by bicycle.

Pedestrian Circulation

Impacts to pedestrian circulation are considered significant if the Proposed Project would:

- Adversely affect existing or planned pedestrian facilities; or
- Fail to adequately provide for access by pedestrians.

Emergency Access

Impacts to emergency access are considered significant if the Proposed Project would:

• Result in inadequate emergency access.

Construction-Related Traffic Impacts

The project would have a temporarily significant impact during construction if it would:

- Degrade an intersection or roadway to an unacceptable level;
- Cause inconveniences to motorists due to prolonged road closures; or
- Result in increased frequency of potential conflicts between vehicles, pedestrians, and bicyclists.

2. EXISTING CONDITIONS

This chapter describes the existing physical and operational characteristics of the transportation system within the study area including the roadway, transit, bicycle, and pedestrian components of the system.

ROADWAY SYSTEM

Figure 3 shows the study area roadway network. Key roadways in the study area include:

- Stockton Boulevard is an arterial street that begins at Alhambra Boulevard and extends in a generally southern direction through the City of Sacramento. Within the study area, it consists of two lanes in each direction separated by either a left-turn pocket or a two-way left-turn lane. It has a posted speed limit of 30 mph. Stockton Boulevard has a partial interchange with US Highway 50 (US 50) including an eastbound diagonal on-ramp, westbound diagonal off-ramp, and westbound loop on-ramp. On-street parking is permitted on Stockton Boulevard under the US 50 overcrossing, but prohibited south of the interchange.
- T Street extends in an easterly direction from Midtown into East Sacramento, terminating near 65th Street. Within the study area, it is a two-lane undivided roadway with a posted speed limit of 30 mph. On-street parking is permitted on portions of T Street east of Stockton Boulevard. Speed lumps (undulations with advisory speeds of 15 mph) are situated on T Street between 37th and 39th Streets.

The residential area in the vicinity of T Street, 37th Street, S Street, and 39th Street has a residential permit parking program. This program prohibits on-street parking between the hours of 8 AM and 6 PM unless vehicles are equipped with a B Parking Permit.

Traffic counts were collected at all study intersections on Tuesday, October 21, 2014 during the AM (7 – 9 AM) and PM (4 – 6:30 PM) peak periods. Due to the importance of the Stockton Boulevard/T Street intersection to overall corridor operations, it was also counted during the PM peak period on October 22^{nd} . Traffic volumes varied by less than three percent between the two days. Schools were in session at the time of the counts, weather conditions were dry, and no unusual traffic conditions were observed.

Figure 4 displays the existing AM and PM peak hour traffic volumes, lane configurations, and traffic controls at each intersection. At the Stockton Boulevard/T Street intersection, the AM peak hour occurred from 7:15 to 8:15 AM and the PM peak hour occurred from 4:30 to 5:30 PM. Figure 4 shows that three of the six study intersections are controlled by traffic signals.



Number of Travel Lanes

(Both directions excluding turn lanes) 4

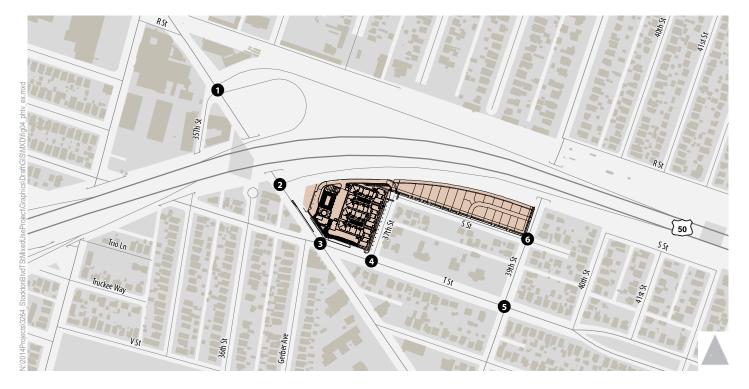
____ 1

2

5 Project Site

Figure 3

Existing Roadway Network



| 1. Stockton Blvd/35th St/US 50 WB Ramps | 2. Stockton Blvd/US 50 EB On-Ramp | 3. Stockton Blvd/T St/Gerber Ave | 4. 37th St/T St |
|---|--|---|---|
| (8) (1) (2) (3) <td>857 (1,120) → 321 (419) → 321 (419) → 500 BBDvd 321 (419) → 500 BBDvd 321 (419) → 510 (419)</td> <td>(10000000 + 10000000 + 10000000 + 100000000</td> <td>(0) (1) (2) (2) (3) (3) (3) (3) (3) (3) (3) (3</td> | 857 (1,120) → 321 (419) → 321 (419) → 500 BBDvd 321 (419) → 500 BBDvd 321 (419) → 510 (419) | (10000000 + 10000000 + 10000000 + 100000000 | (0) (1) (2) (2) (3) (3) (3) (3) (3) (3) (3) (3 |
| 5. 39th St/T St | 6. 39th St/S St | | |
| 19 (48) 181 (259) 181 (259) ↓ | (6) 0 (0) 0 (0) 1 (0) 1 (0) 1 (1) (235 (241) (1) (235 (241) (1) (241) (1) (241) (1) (241) | Study Intersection AM (F Project Site Turn Lane Note: Counts conducted on | Traffic SignalStop Sign |
| 181 (259) ▲ (₹) (£) (£) (59) ▲ (₹) (59) (7) (7) (7) (7) (7) (7) (7) (7) (7) (7 | 0 (0) 2 (1) 2 (1) 2 (2) 2 (2) 2 (2) 2 (2) 3 (2) 5 (2) 5 (2) 6 (0) 6 (0) 6 (0) 7 (0) 6 (0) 7 | Tuesday, October 21, 201 | 4. |

Figure 4 Peak Hour Traffic Volumes and Lane Configurations -Existing Conditions



The study area experiences considerable congestion during the PM peak period. This occurs, in part, due to the effects of ramp metering of the US 50/Stockton Boulevard westbound loop on-ramp. This on-ramp features a single, metered lane that accommodates two vehicles per green cycle, with successive green cycles being about 9 to 10 seconds apart. Assuming optimal usage, between 720 and 800 vehicles per hour are able to pass through this ramp meter. The traffic counts revealed 732 vehicles during the PM peak hour that entered the loop on-ramp. Field observations revealed lengthy vehicle queues and imbalanced lane utilization on northbound Stockton Boulevard resulting from the ramp meter. ¹ Below is a photo illustrating the extent of northbound vehicle queuing.



View of vehicle queues on northbound Stockton Boulevard (extending to T Street) due to ramp metering of the westbound US 50 loop on-ramp

A ramp meter also exists on the US 50 eastbound on-ramp from Stockton Boulevard. However, it was not operational at the time of the traffic counts.

¹ The loop on-ramp becomes a westbound US 50 auxiliary lane that terminates at the Capital City Freeway offramp. Although the general purpose lanes along this segment of US 50 were congested during recent field observations, the auxiliary lane was not. This implies that the source of the surface street queuing is due to the effects of the ramp meter and not freeway congestion.

Figure 5 shows the following at the Stockton Boulevard/T Street intersection:

- Lane Configurations
- Crosswalk lengths
- Traffic signal phasing
- Turn movement prohibitions
- AM and PM peak hour vehicle, bicycle, and pedestrian volumes

Field observations indicate that the intersection operates with a 90-second cycle length during peak hours. The pedestrian WALK / DON'T WALK indications are operational on all legs regardless of the presence of a pedestrian. As shown on Figure 5, the north-south movements operate with permitted phasing, as do the east-west movements. When a vehicle arrives at the Gerber Avenue approach, it has its own (actuated) phase. If vehicle(s) are not present on this approach, its phase is skipped.

Vehicles on westbound T Street are prohibited (by signage) from turning right on red. Eastbound T Street features left/through and through/right lanes approaching Stockton Boulevard (though the limit line is at Gerber Avenue). Directly beyond the intersection, T Street is approximately 24 feet wide but does not include striping for two receiving lanes. An advisory 'lanes merge' sign is posted.

Figure 5 shows that the crosswalk on the south leg of the intersection (i.e., across Stockton Boulevard) is the most heavily utilized among all the crosswalks. T Street east of Stockton Boulevard accommodates the greatest number of bicyclists passing through the intersection.

The following page contains charts that display the directional, peak hour traffic volumes on Stockton Boulevard north and south of T Street. These charts reveal the following travel characteristics in the corridor:

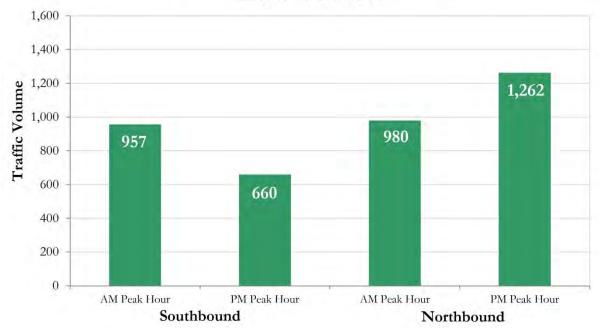
- During the AM Peak Hour, traffic volumes on Stockton Boulevard south of T Street are much heavier than volumes north of T Street. This is due to the heavy eastbound right-turn movement (430 vehicles) from T Street. Many of these trips likely originate from Midtown or the US 50 eastbound offramp and are destined for UC Davis Medical Center.
- 2. The segment of Stockton Boulevard north of T Street carries substantially more northbound traffic than southbound traffic. During the PM peak hour, 77 percent of all traffic on this segment is northbound. This occurs as a consequence of typical commute patterns in the area, and the presence of two on-ramps, but only one off-ramp (from WB direction) at the US 50/Stockton Boulevard interchange.

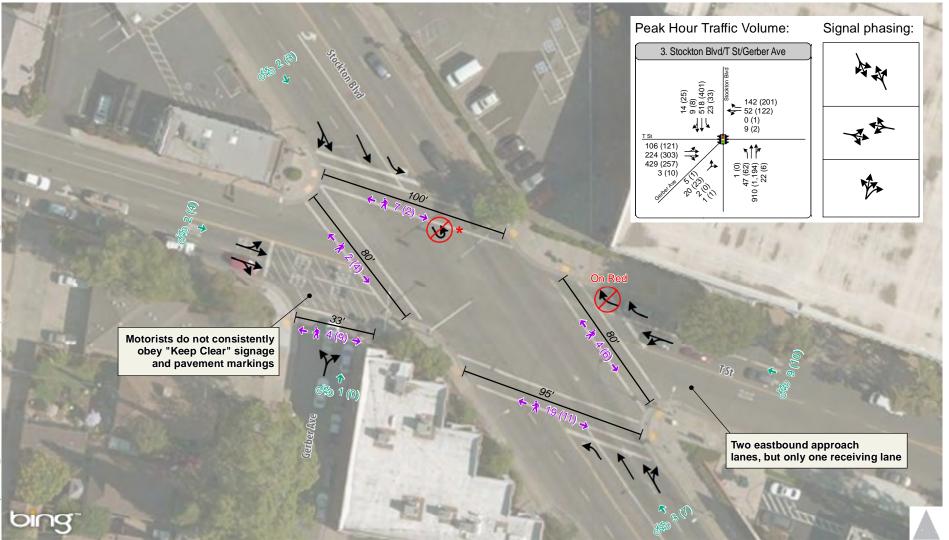
It is important that the SimTraffic model be adequately validated to existing conditions so that it can accurately predict "plus project" conditions. Model validation often consists of measures relating to volume served, queue lengths, and average travel time. Given the modest size of the study area but considerable levels of congestion, vehicle queuing is considered the most important validation parameter.

Existing Directional Traffic on Stockton Boulevard North of T Street 1,600 1,539 1,400 1,200 Traffic Volume 1,178 1,000 800 600 564 400 467 200 0 AM Peak Hour PM Peak Hour AM Peak Hour PM Peak Hour Southbound Northbound

Final Transportation Impact Study for the Stockton Boulevard/T Street Mixed-Use Project February 25, 2015

Existing Directional Traffic on Stockton Boulevard South of T Street





Turn Lane
AM (PM) Peak Hour Traffic Volume
 Traffic Signal

- AM (PM) Peak Hour Pedestrians
 MM (PM) Peak Hour Bicyclists
- ★ Signs do not prohibit u-turns. However, geometric configuration makes them difficult to make.

Figure 5 Stockton Boulevard/T Street Intersection -



Existing Conditions

As part of the traffic count data collection, maximum vehicle queues were recorded for several critical turning movements at the Stockton Boulevard/T Street intersection. **Table 2** displays the available storage, observed maximum vehicle queue, and modeled (via SimTraffic) maximum queue length at this intersection.²

| TABLE 2: PM PEAK HOUR QUEUING ANALYSIS – EXISTING CONDITIONS | | | | | | |
|---|-------------------------|----------|--|---|-----------------------------|--|
| Intersection | Available Storage | Movement | Maximum Observed Vehicle Queue ¹ | Maximum Modeled Vehicle Queue ² | Difference (in vehicles) | |
| 3. Stockton Boulevard / T St / Gerber Avenue | 1,100 ft. per lane 3 | NB TH/RT | 750 ft. | 900 ft. | +6 | |
| | 570 ft. ⁴ | EB LT/TH | 450 ft. | 375 ft. | -3 | |
| | 375 ft. | EB TH/RT | 350 ft. | 350 ft. | 0 | |
| | 800 ft. per lane | SB TH/RT | 200 ft. | 150 ft. | -2 | |
| | 175 ft. | SB LT | 25 ft. | 50 ft. | +1 | |
| | 200 ft. ⁵ | WB LT/TH | 100 ft. | 175 ft. | +3 | |
| | 130 ft. ⁶ | WB RT | 200 ft. | 200 ft. | 0 | |

Notes:

1. Observed queues during PM peak hour on Tuesday October 21, 2014. Values rounded to the nearest 25 ft.

2. Modeled results based on maximum predicted queue length reported from SimTraffic. Rounded to nearest 25 feet.

3. Distance to upstream signalized Stockton Boulevard/39th Street intersection. Maximum queue reported for outside northbound travel lane, which has more lengthy queues due to motorists' lane selection in advance of US 50/Stockton Boulevard interchange.

4. Distance to upstream T Street/35th Street intersection.

5. Distance to upstream T Street/37th Street intersection.

6. Distance to first upstream on-street parking space on T Street.

Source: Fehr & Peers, 2015

For most movements, the SimTraffic model validates well against the observed maximum vehicle queues at the Stockton Boulevard/T Street intersection. However, the model over-predicts queuing for the following two movements:

1. Northbound Outside Through/Right – The model over-predicts (by six vehicles) the maximum observed vehicle queue. This occurs as a result of the model's requirement that a minimum advance lane selection distance be selected for vehicles that desire to access the eastbound or westbound on-

² The PM peak hour experienced much greater levels of congestion and queuing (and was more directly affected by ramp metering) than the AM peak hour. For this reason, vehicle queue observations and model validation focused on PM peak hour conditions.

ramps. Field observations indicate that most motorists queue in the outside through lane in anticipation of accessing these ramps. However, some motorists remain in the inside through lane, and merge into the outside lane downstream of T Street. SimTraffic is not able to accurately model this aggressive and irregular driver behavior, which explains why the model over-predicts the maximum observed vehicle queue in the outside northbound through/right lane.

 Westbound Left/Through – The model overpredicts (by three vehicles) the maximum observed vehicle queue. Based on observations of the SimTraffic on-screen results, this occurs as a result of a simulated left-turning vehicle having difficulty turning onto southbound Gerber Avenue (i.e., waiting for a substantially long gap in eastbound T Street through traffic).

These over-predictions are caused by limitations in the software program. They do not appreciably affect the intersection's overall average delay or LOS. When queue lengths for these two movements are estimated under 'plus project' conditions, a modified difference method procedure (whereby the SimTraffic model's estimated increase in queuing resulting from the project is added to the existing observed maximum queue) is used to correct for these over-predictions.



Below is a screenshot of the SimTraffic model used to analyze the study intersections.

View of SimTraffic micro-simulation model used to analyze study intersections

Figure 6 illustrates the existing maximum observed vehicle queues in the study area during the PM peak hour. As shown, lengthy queues form at the ramp meter on the westbound US 50 loop on-ramp. This queuing spills back onto Stockton Boulevard, extending to T Street and beyond. The indirect effect of this queuing is frequent/continuous blockage of the southbound left-turn movement onto the eastbound US 50 on-ramp. The length of queues on the eastbound, westbound, and northbound approaches to the Stockton Boulevard/T Street intersection are also affected by queuing from the on-ramp.

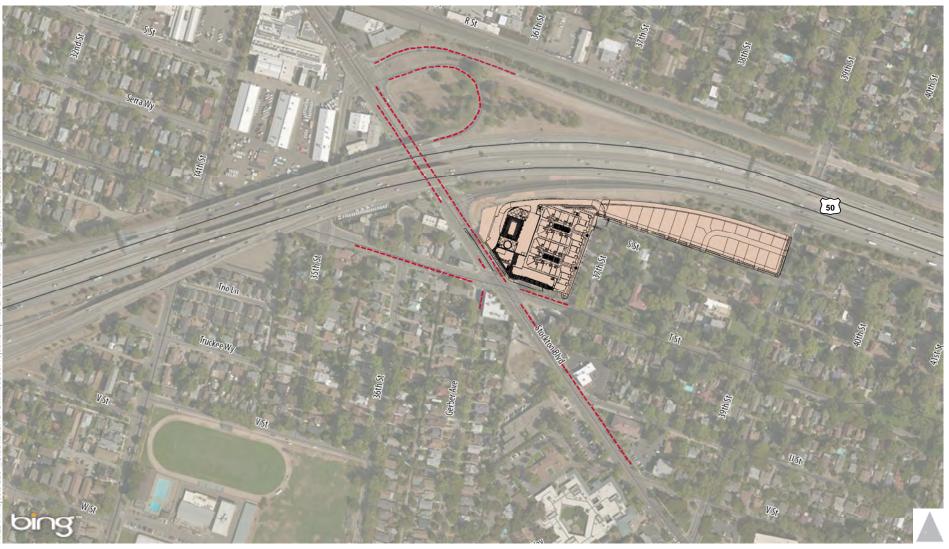
On December 17, 2014, additional PM peak hour field observations were conducted at the Stockton Boulevard/T Street intersection. The purpose of these observations was to determine the arrival and departure characteristics of southbound left-turning vehicles relative to their arrival during different phases of the traffic signal. The following shows the results:

| Number of Vehicles Arriving During Red Indication: | 10 |
|--|----|
| Number of Vehicles Turning Left During Successive Green Indication: | 1 |
| Number of Vehicles Turning Left During Successive Yellow/All-Red Indication: | 9 |
| Number of Vehicles Arriving During First Half of Green Indication: | 9 |
| Number of Vehicles Turning Left During Same Green Indication: | 2 |
| Number of Vehicles Turning Left During Successive Yellow/All-Red Indication: | 7 |
| Number of Vehicles Arriving During Second Half of Green Indication: | 5 |
| Number of Vehicles Turning Left During Same Green Indication: | 3 |
| Number of Vehicles Turning Left During Successive Yellow/All-Red Indication: | 2 |

This data indicates that 25 percent of all left-turning vehicles were able to turn during the green indication. Due to lack of available gaps, the remaining 75 percent of motorists turned left during the yellow or all-red signal indications when gaps in northbound traffic became available. This is important when considering how the left-turn would operate with the addition of project trips.

Table 3 summarizes the existing AM and PM peak hour operations at the study intersections (refer to separate Appendix A for detailed calculations). Key findings from this table include:

- During the AM peak hour, all study intersections operate at LOS C or better.
- During the PM peak hour, the Stockton Boulevard/T Street intersection operates at LOS E. As noted earlier, this result is due, in part, to ramp metering on the westbound US 50 loop on-ramp that spills back onto Stockton Boulevard into the intersection.



Vehicle Queue Project Site Note: Queue length observation on surface streets collected on Tuesday, October 21, 2014.

Figure 6

Maximum Observed Vehicle Queues – Existing PM Peak Hour Conditions



| TABLE 3: INTERSECTION OPERATIONS – EXISTING CONDITIONS | | | | | | |
|--|------------------|--------------------|--------|--------------------|-------|--|
| | | AM Pea | k Hour | PM Peak Hour | | |
| Intersection | Control | Delay (sec/veh) | LOS | Delay (sec/veh) | LOS | |
| 1. Stockton Boulevard/35 th Street/US 50 WB Ramps | Traffic Signal | 23.5 | С | 43.4 | D | |
| 2. Stockton Boulevard/US 50 EB Ramps | Uncontrolled | 1.9 (10.5) | A (B) | 14.8 (52.1) | B (F) | |
| 3. Stockton Boulevard/T Street/Gerber Avenue | Traffic Signal | 25.9 | С | 55.9 | E | |
| 4. T Street/37 th Street | Side-Street Stop | 2.1 (6.2) | A (A) | 12.9 (24.8) | B (C) | |
| 5. T Street/39 th Street | Traffic Signal | 14.1 | В | 14.8 | В | |
| 6. S Street/39 th Street | Side-Street Stop | 0.7 (3.5) | A (A) | 1.2 (7.4) | A (A) | |

Notes:

¹ For signalized intersections, the LOS is based on the average delay experienced by all vehicles passing through the intersection. For uncontrolled and side-street stop controlled intersections, the delay and LOS for the worst case movement (in parentheses) is reported along with the average delay for the entire intersection and for the overall movement not in parentheses.

Source: Fehr & Peers, 2015

An analysis was conducted to better understand the degree to which the ramp meter on the westbound loop on-ramp affects the Stockton Boulevard corridor. The existing PM peak hour SimTraffic model was reanalyzed with the ramp meter removed (with all other inputs remaining unchanged). The results indicated that the Stockton Boulevard/T Street intersection would improve to LOS C and vehicle queues would be reduced on all approaches. However, this analysis did not take into consideration the likelihood that additional motorists may use the Stockton Boulevard corridor in response to the reduced queuing and travel times. Thus, it is more realistic that operations at Stockton Boulevard/T Street intersection would be in the LOS D range if the ramp meter was removed.

Fehr & Peers obtained collision data for the Stockton Boulevard/T Street intersection from January 1, 2009 through November 6, 2014. Over this nearly six-year period, 12 total collisions were reported. Given the level of traffic that passes through this intersection, an average of two collisions per year is considered a relatively low collision frequency. Review of the collision data indicated that the vast majority involved two vehicles. Most collisions were either rear-end, sideswipe, or broadside. Only one collision involved a vehicle performing a southbound left-turn. This data suggests that motorists are using care when driving through the intersection based on the type and rate of collisions.

BICYCLE SYSTEM

Figure 7 displays the existing bicycle facilities located in the vicinity of the project site based on field observations and review of aerial imagery. As shown, Class II bike lanes (on-street with appropriate signing and striping) exist on both sides of T Street east of 37th Street, and portions of T Street west of Stockton Boulevard. According to the *Sacramento Existing and Proposed Bikeways Map* (Updated October 2011), a continuous Class II bike lane is shown to currently exist on T Street throughout the study area. However, bicycle lanes are not present on the T Street approach and departure legs at Stockton Boulevard. Furthermore, as shown in the image on the following page, the Class II bike lane on the south side of T Street currently terminates at 36th Street.

The *Sacramento Existing and Proposed Bikeways Map* shows a proposed Class II bike lane on Stockton Boulevard from T Street southerly to Broadway.

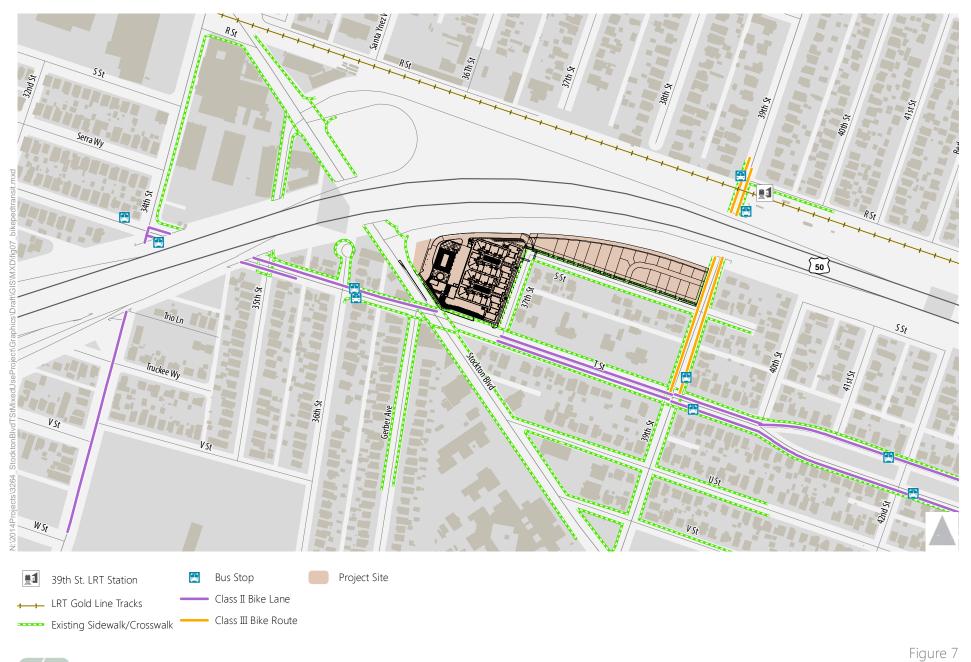
PEDESTRIAN SYSTEM

Figure 7 displays the pedestrian facilities located in the vicinity of the project site. As shown, sidewalks are present along the majority of Stockton Boulevard and T Street. Crosswalks exist on all approaches to the Stockton Boulevard/T Street intersection. Regardless of the presence of pedestrians, the WALK / DON'T WALK indication is operational for all crosswalks. As shown on Figure 7, sidewalks also exist on the majority of 37th Street, S Street, and 39th Street. Continuous pedestrian facilities connect the project site with the 39th Street light rail station.

TRANSIT SYSTEM

Public transit service within the study area is provided by light rail and bus, which is operated by the Sacramento Regional Transit (RT).

39th **Street Light Rail Station** – This station is a stop along the Gold Line, which operates between downtown Sacramento and the City of Folsom. Trains stop at this station from approximately 4 AM to 12 AM Monday through Friday. The Gold Line operates on 15-minute headways from approximately 5 AM to 7 PM Monday through Friday, and 30-minute headways beyond these hours. On Saturdays, Sundays, and Holidays, the Gold Line operates on 30-minute headways from about 5:30 AM to 11:00 PM. The light rail station is less than a ¹/₂-mile walk from any part of the project site.



Bicycle, Pedestrian, and Transit Facilities – Existing Conditions

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View of T Street at 36th Street – Eastbound Class II bike lane terminates just west of 36th Street

Route 38 provides service on T Street west of Stockton Boulevard and continues on Stockton Boulevard south of T Street. This route features a bus stop in each direction of T Street at 36th Street. This route begins in Land Park and terminates at 65th Street and Folsom Boulevard. Monday through Friday, Route 38 operates on 60-minute headways from about 6:30 AM to 8:30 PM. On Saturdays, Route 38 operates on 60-minute headways from about 8 AM to 8 PM. On Sundays and Holidays, Route 38 operates on 60-minute headways from about 8 AM to 6 PM.

Routes 212, 213, & 214 provide service to Kit Carson Middle School in East Sacramento. Each line features bus stops adjacent to the 39th Street/T Street intersection. Route 212 begins at 21st Avenue and 65th Street, Route 213 begins at West Campus High School in South Sacramento, and Route 214 begins at T Street and 34th Street. Monday through Friday, these routes operate one morning trip from about 7 AM to 8 AM and one afternoon trip from about 2 PM to 3 PM. Routes 212, 213, and 214 do not operate on Saturdays, Sundays, or Holidays.

Bus service does not currently exist along Stockton Boulevard north of T Street or T Street between Stockton Boulevard and 39th Street.

The Capital City Hospital Shuttle service stops at the 39th Street Light Rail station. This free shuttle transports employees, patients, and visitors to the Mercy, Sutter, UC Davis Medical Centers located in Midtown and East Sacramento.

3. EXISTING PLUS PROJECT CONDITIONS

This chapter analyzes the potential traffic impacts of the proposed project on the surrounding roadway system under existing conditions. Chapter 6 describes the specific impacts of the project on the roadway system, as well as impacts to bicycle, pedestrian, and transit modes.

PROJECT TRAVEL CHARACTERISTICS

This chapter begins by describing the project's expected travel characteristics including the anticipated number of vehicle trips, directionality of those trips, and their expected travel routes.

Trip Generation

The first step in analyzing the proposed project's travel characteristics was to estimate its AM and PM peak hour trip generation using data published in the *Trip Generation Manual*, 9th Edition (Institute of Transportation Engineers, 2012). The *Manual* is the most widely used industry resource for this type of data. The trip generation data are organized by land use types, with more than 170 different categories of land uses. For each category, the *Manual* provides a data set for use in estimating the number of vehicle and person trips generated by a site based on its characteristics such as physical size or intensity. Trips may be estimated by direction (entering or exiting the site), and for time periods typically pertaining to a full day (weekday or weekend), peak periods of the adjacent roadway, and peak hours of the particular land use. Used properly, the *Trip Generation Manual* provides an objective basis for estimating trips generated by a proposed development.

Most of the observation sites used to develop trip rates in the *Manual* were collected in suburban settings, which often feature limited transit service, and may not have nearby destinations within close walking/biking distance. Therefore, adjustments to ITE trip rates are warranted based on the proximity of transit service, and numerous nearby attractions within bicycling and walking distance.

The expected amount of internal trip-making between the residential and retail uses, and proportion of external trips made by walking, bicycling, and transit was estimated using the Mixed-Use Trip Generation Model (MXD). This model was developed for the US Environmental Protection Agency (EPA) by consultants and academic researchers to more accurately estimate the external vehicular trip generation of mixed-use land development projects than prior methods (e.g., ITE internalization spreadsheet). The model was developed based on empirical evidence at 240 mixed-use projects located across the U.S. The model considers various built environment variables such as land use density, regional location, proximity to transit, and various design variables when calculating the project's internal trips, and external trips made by auto, transit, and non-motorized modes. The MXD model has been used in dozens of EIRs and other environmental documents throughout California.

Table 4 displays the trip generation of the proposed project during the weekday AM and PM peakhours. Refer to Appendix B for the MXD model output.

| | | | | ABLE 4: | | | | | | | |
|--------------------------------|-------------------------------------|---|-----------|--|---------|--------------------|-----|-------|----------------------|-----|--|
| | | ND PM PEAK | | | N – PRO | POSED I | | | | | |
| Land Use | Quantity Use Code | | AM Peak | Trip Rate ¹ Peak PM Peak | | Tr AM Peak Hour | | | rips PM Peak Hour | | |
| | | | Hour Hour | Hour | Total | In | Out | Total | In | Out | |
| Single-Family Housing | 24 du's | 210 | 1.21 | 1.29 | 29 | 8 | 21 | 31 | 20 | 11 | |
| Mid-Rise Apartments | 214 du's | 223 | 0.39 | 0.48 | 84 | 18 | 66 | 102 | 63 | 39 | |
| Retail | 6 ksf | 820 | 0.96 | 3.71 | 6 | 4 | 2 | 22 | 11 | 11 | |
| Gross Trips | | | | | 119 | 30 | 89 | 155 | 94 | 61 | |
| | | Internal Trips ² | | | | -3 | -3 | -10 | -5 | -5 | |
| | | F | -2 | -1 | -1 | -4 | -2 | -2 | | | |
| | | Pass-by Trips (to Retail) ² External Walk & Bike Trips ² | | | | -4 | -13 | -19 | -11 | -8 | |
| | External Transit Trips ² | | | -11 | -3 | -8 | -13 | -8 | -5 | | |
| New Vehicle Trips ² | | | | 83 | 19 | 64 | 109 | 68 | 41 | | |

Notes:

¹ Trip rates from *Trip Generation* (ITE, 2012). Fitted curve equation used to estimate trips for residential uses. Average rate used to estimate trips for retail use (due to very small square footage). Use of equation would have substantially overestimated trip generation for the retail use.

² Refer to text below for process used to develop these estimates.

ksf = thousand square feet. du's = dwelling units.

The following describes the adjustments made in Table 4:

- <u>Internalization</u>: The MXD model predicts that about five percent of trips will remain internal to the project site. This is reasonable given the limited size of the retail (i.e., one end of the trip match with the residential).
- <u>Pass-by Trips</u>: Per *Trip Generation Handbook, 3rd Edition* (Institute of Transportation Engineers, 2014), 34 percent of non-internal p.m. peak hour retail trips are expected to be pass-by trips.
- <u>External Walk/Bike Trips</u>: The MXD model predicts that about 13 to 15 percent of non-internal trips (varies by analysis hour) will made by walking or bicycling. This is reasonable given the proximity of attractions in the area (e.g., UCD Medical Center, Sacramento Charter High School, and various retail/employment uses along Stockton Boulevard).
- <u>External Transit Trips</u>: The MXD model predicts that about 9 to 10 percent of non-internal trips (varies by analysis hour) will be made by transit. This is reasonable given that the 39th Street Gold

line light rail station is about a 0.2-mile walk from the 37th Street/S Street intersection. In addition, bus service is provided on segments of Stockton Boulevard, T Street, and 39th Street adjacent to the project site. Lastly, the Capital City Hospital Shuttle service stops at the 39th Street Light Rail station. This free shuttle transports employees, patients, and visitors to the Mercy, Sutter, UC Davis medical centers located in mid-town and East Sacramento.

After making these adjustments, the project would generate 83 new AM peak hour vehicle trips and 109 new PM peak hour vehicle trips. These totals represent a 30 percent reduction in trips when compared to the gross trip totals.

Table 5 displays the project's average weekday daily trip generation estimate. As shown, the project would generate 1,180 new average weekday daily trips.

| TABLE 5: DAILY TRIP GENERATION – PROPOSED PROJECT | | | | | | | |
|--|----------|-------------------|--|-------|--|--|--|
| Land Use | Quantity | ITE Land Use Code | Trip Rate ¹ | Trips | | | |
| Single-Family Housing | 24 du's | 210 | 11.77 | 283 | | | |
| Mid-Rise Apartments | 214 du's | 223 | 4.99 | 1,068 | | | |
| Retail | 6 ksf | 820 | 42.70 | 256 | | | |
| | | | Gross Trips | 1,607 | | | |
| | | | Internal Trips ² | -74 | | | |
| | | F | Pass-by Trips (to Retail) ² | -38 | | | |
| External Walk & Bike Trips ² -240 | | | | | | | |
| External Transit Trips ² -77 | | | | | | | |
| New Vehicle Trips ² 1,178 | | | | | | | |

Notes:

¹ Trip rates from *Trip Generation* (ITE, 2012). Fitted curve equation used to estimate trips for single-family residential uses. Since mid-rise apartments land use category does not contain a daily trip rate, the AM and PM peak hour trip rates were factored up to a daily rate based using the same ratio as exists for the Apartments (220) land use category. Average rate used to estimate trips for retail use (due to very small square footage). Use of equation would have substantially overestimated trip generation for the retail use.

² Refer to text above for process used to develop these estimates.

ksf = thousand square feet. du's = dwelling units.

Trip Distribution/Assignment

Figures 8a and 8b show the expected distribution of inbound and outbound vehicle trips, respectively, to the project. It was necessary to develop separate inbound and outbound percentages due to the effects of different freeway accesses. Specifically, inbound trips to the project traveling eastbound on US 50 would exit at 34th Street and access the site via T Street. In contrast, outbound trips from the project site traveling on westbound US 50 would use Stockton Boulevard to the US 50 loop on-ramp.

The distribution percentages are based on an assignment of project trips using the base year version of SACOG's travel demand model. Minor adjustments to the model's predicted assignment of trips were made in consideration of existing turning movements and travel patterns in the area, roadway segments featuring directional congestion, and project access provisions (i.e., right-turn only driveway on Stockton Boulevard).

TRAFFIC FORECASTS

AM and PM peak hour traffic forecasts were developed for the "existing plus project" condition by adding project trips to existing volumes using the project's trip generation from Table 4 and trip distribution percentages from Figures 8A and 8B.

The assignment of project trips considers that the project driveway on Stockton Boulevard would be restricted to right-turns only. The assignment also reflects the planned restriction of the new internal street on 39th Street to inbound travel only. All other project accesses would permit all turning movements.

Figure 9 displays the resulting existing plus project forecasts. This figure shows trips entering/exiting the new driveway on Stockton Boulevard. The project would cause the following increases in the southbound left-turn movement at the Stockton Boulevard/T Street intersection:

- o <u>AM Peak Hour</u>: Traffic volume would increase from 23 to 29 vehicles (26 percent increase)
- <u>PM Peak Hour</u>: Traffic volume would increase from 33 to 53 vehicles (61 percent increase)



Inbound Project Trip Distribution

Figure 8A



Inbound Project Trip Distribution



Outbound Project Trip Distribution
 Project Site

Figure 8B

Outbound Project Trip Distribution





| 1. Stockton Blvd/35th St/US 50 WB Ramps | 2. Stockton Blvd/US 50 EB On-Ramp | 3. Stockton Blvd/T St/Gerber Ave | 4. 37th St/T St | | |
|--|---|---|---|--|--|
| 10 (16) 58 (49) 72 (30) 72 (30) 572 (570) 35th Street 572 (570) 10 (16) 58 (49) 72 (30) 572 (570) | 886 (1,143) → 329 (421) → 6 00 00 00 00 00 00 00 00 00 00 00 00 00 | $(100) \begin{array}{c} 100 \\$ | (¹ C) (C) ¹ C (C) ¹ | | |
| 5. 39th St/T St | 6. 39th St/S St | 7. Stockton Blvd/New Driveway | | | |
| 38th Si |) 38th St | n Blvd | 1 Study Intersection | | |
| (60) (153) (40) | 6 (12) 236 (245) 0 (1) 0 (1) 0 (1) 0 (1) | 87) Stockton Biva | Project Site | | |
| 59 (64) 59 (64) ↓ 129 (251) 11 (11) | $\begin{array}{c c} & & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & & \\ & &$ | (287) 025 ► 17 (14) | - Turn Lane | | |
| T Street | <u>S St</u> | New Driveway | AM (PM) Peak Hour Traffic Volume | | |
| 10 (48) | 10 (14) | | Traffic Signal | | |
| 133 (260) ★ 183 (220) ↓ 63 (22) ↓ (1) ↓ | 50 (0) 0 50 (2) 5 50 (2) 8 50 (0) 0 50 (0 | 1,198 (1,550) 5 (8) | 💩 Stop Sign | | |

Figure 9

Peak Hour Traffic Volumes and Lane Configurations -Existing Plus Project Conditions



INTERSECTION OPERATIONS

Table 6 displays the results at the study intersections under "existing plus project" conditions. Refer to Appendix C for technical calculations. This table indicates the following:

- During the PM peak hour, the average delay at the Stockton Boulevard/T Street intersection would increase from 56 to 71 seconds per vehicle. Operations would remain at LOS E.
- The project would cause additional delays during the PM peak hour for the southbound left-turn (yield-controlled) movement at the US 50 EB ramps/Stockton Boulevard intersection. This occurs as a result of the project adding 25 additional northbound trips, which causes fewer gaps for this movement.

| TABLE 6: INTERSECTION OPERATIONS – EXISTING PLUS PROJECT CONDITIONS | | | | | | | | | |
|--|---------------------|--------------------|------------|--------------------|--------|--------------------|------------|--------------------|-------|
| | | | Existing (| Conditions | | Existin | g Plus Pro | oject Condi | tions |
| Intersection | Control | AM Pea | k Hour | PM Peal | (Hour | AM Pea | k Hour | PM Peak | Hour |
| intersection | Control | Delay (sec/veh) | LOS | Delay (sec/veh) | LOS | Delay (sec/veh) | LOS | Delay (sec/veh) | LOS |
| 1. Stockton Boulevard/35 th Street/US 50 WB Ramps | Traffic Signal | 23.5 | С | 43.4 | D | 22.5 | С | 42.2 | D |
| 2. Stockton Boulevard/US 50 EB Ramps | Uncontrolled | 1.9 (10.5) | A (B) | 14.8 (52.1) | B (F) | 2.1 (11.8) | A (B) | 17.0 (61.5) | C (F) |
| Stockton Boulevard/T Street/Gerber Avenue | Traffic Signal | 25.9 | С | 55.9 | E | 29.3 | С | 71.2 | E |
| 4. T Street/37 th Street | Side-Street Stop | 2.1 (6.2) | A (A) | 12.9 (24.8) | B (C) | 2.3 (5.5) | A (A) | 8.7 (21.6) | A (C) |
| 5. T Street/39 th Street | Traffic Signal | 14.1 | В | 14.8 | В | 14.4 | В | 14.8 | В |
| 6. S Street/39 th Street | Side-Street Stop | 0.7 (3.5) | A (A) | 1.2 (7.4) | A (A) | 0.9 (5.9) | A (A) | 1.0 (7.6) | A (A) |

Notes:

¹ For signalized intersections, the LOS is based on the average delay experienced by all vehicles passing through the intersection. For uncontrolled and side-street stop controlled intersections, the delay and LOS for the worst case movement (in parentheses) is reported along with the average delay for the entire intersection and for the overall movement not in parentheses.

Source: Fehr & Peers, 2015

Table 7 displays the maximum expected vehicle queues during the PM peak hour at the Stockton Boulevard/T Street intersection under "existing plus project" conditions. This table indicates the following:

- The project would cause the northbound outside through lane maximum queue to increase by 10 vehicles (250 feet at 25 feet per vehicle). This occurs as a result of the project adding northbound traffic to Stockton Boulevard.
- The project would cause the southbound left-turn lane maximum queue to increase from two to five vehicles (50 to 125 feet). The following page shows a SimTraffic screenshot of this queuing situation.
- The project would cause the westbound left/through and right-turn lane maximum queues to spill back into the 37th Street/T Street intersection. The following page also shows a SimTraffic screenshot of this queuing situation.

| TABLE 7: PM PEAK HOUR QUEUING ANALYSIS – EXISTING PLUS PROJECT CONDITIONS | | | | | | | |
|--|-------------------------|------------|---------------------|--|--|--|--|
| | | | Maximum Ve | ehicle Queue | | | |
| Intersection | Available Storage | Movement - | Existing Conditions | Existing Plus Project Conditions ² | | | |
| | 1,100 ft. per lane 3 | NB TH/RT | 750 ft. | 1,000 ft. | | | |
| | 570 ft. ⁴ | EB LT/TH | 375 ft. | 525 ft. | | | |
| | 375 ft. | EB TH/RT | 350 ft. | 400 ft. | | | |
| 3. Stockton Boulevard / T St / Gerber Avenue | 800 ft. per lane | SB TH/RT | 150 ft. | 150 ft. | | | |
| | 175 ft. | SB LT | 50 ft. | 125 ft. | | | |
| | 200 ft. ⁵ | WB LT/TH | 175 ft. | 200 (t) 75 (t) ⁷ | | | |
| | 130 ft. ⁶ | WB RT | 200 ft. | 200 ft. + 75 ft. ⁷ | | | |

Notes:

1. Observed queues during PM peak hour on Tuesday October 21, 2014. Values rounded to the nearest 25 ft.

2. Modeled results based on maximum predicted queue length reported from SimTraffic. Rounded to nearest 25 feet.

3. Distance to upstream signalized Stockton Boulevard/39th Street intersection. Maximum queue reported for outside northbound travel lane, which has more lengthy queues due to motorists' lane selection in advance of US 50/Stockton Boulevard interchange.

4. Distance to upstream T Street/35th Street intersection.

5. Distance to upstream T Street/37th Street intersection.

6. Distance to first upstream on-street parking space on T Street.

Maximum queue extends into the T Street/37th Street intersection, and includes an additional three vehicles queued on the WB through and SB approaches to the intersection.

Source: Fehr & Peers, 2015



SimTraffic screenshot showing a southbound left-turn queue of five vehicles



SimTraffic screenshot showing westbound queue extending into 37th Street/T Street intersection

NEIGHBORHOOD STREETS

The effects of the project on traffic levels on neighborhood streets in the project vicinity were analyzed under "existing plus project" conditions. **Table 8** displays the projected increase in PM peak hour trips resulting from the project on various residential streets. Data is shown for the PM peak hour (versus AM peak hour) because volumes are greater during the PM peak hour on nearly every study roadway.

This table indicates that the project would cause a one to three percent increase in traffic on segments of T Street and 39th Street east of Stockton Boulevard. Project-related increases in traffic on 37th Street and S Street are greater, both in terms of the volume added and the percentage increase. However, both streets would continue carrying less than 100 vehicles during the PM peak hour, which is well within the comfortable carrying capacity of each street.

| TABLE 8: NEIGHBORHOOD STREET TRAFFIC VOLUMES – EXISTING PLUS PROJECT CONDITIONS | | | | | | | |
|--|----------------------------------|-------------------------------------|--|------------|--|--|--|
| | PM | Peak Hour Volume | (in Both Directions) | | | | |
| Segment | Existing Conditions ¹ | Project-Related Traffic Increase | Existing Plus Project Conditions ² | % Increase | | | |
| T Street east of 37 th Street | 644 | 12 | 656 | 1.9% | | | |
| T Street east of 39 th Street | 652 | 7 | 659 | 1.1% | | | |
| 39 th Street north of S Street | 535 | 15 | 550 | 2.8% | | | |
| 39 th Street south of T Street | 401 | 4 | 405 | 1.0% | | | |
| 37 th Street north of T Street | 30 | 62 | 92 | 206.7% | | | |
| S Street east of 37 th Street | 21 | 16 | 37 | 76.2% | | | |

Notes:

¹ Existing volume based on counts collected in October 2014 while schools were in session.

² Existing Plus Project volume based on project's expected travel characteristics (including trip generation, distribution, and route assignment through neighborhoods).

Source: Fehr & Peers, 2015

4. CUMULATIVE CONDITIONS

This chapter describes cumulative transportation conditions in the project vicinity assuming development of the proposed project. All technical calculations are contained in Appendix D.

TRAFFIC FORECASTS

Fehr & Peers used the most recent version of SACOG's travel demand model to develop traffic forecasts in the study area. This model has recently been used for other studies in the City such as the Entertainment Sports Center (ESC) EIR, I Street Bridge Study, and Downtown Transportation Study. Fehr & Peers added additional land use and roadway network detail to the model to better match the existing roadway system and loading of trips onto streets.

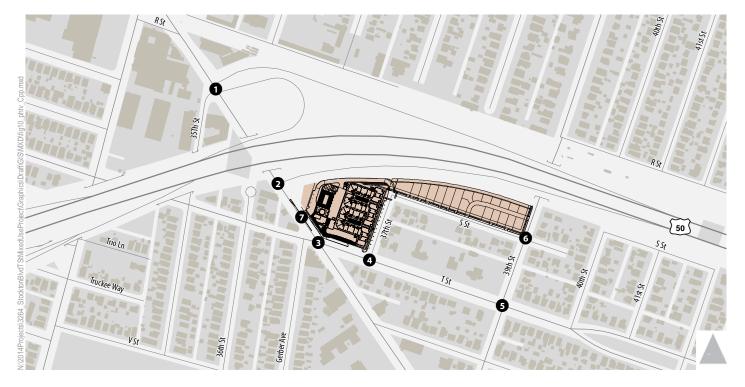
A forecasting procedure known as the "difference method" was utilized to develop the cumulative background forecasts. This method accounts for potential differences between the base year model and existing traffic counts that could otherwise transfer to the future year model and traffic forecast. This forecasting procedure is calculated as follows:

Cumulative Traffic Forecast = Existing Volume + (Cumulative TDM Forecast – Base Year TDM Forecast)

Trips associated with the proposed project were then added to the cumulative forecast using the same trip generation, distribution, and assignment procedures described in Chapter 3. **Figure 10** displays the resulting cumulative plus project peak hour traffic forecasts at the study intersections. As shown, the same lane configurations and traffic controls as currently exist were assumed at the study intersections since there are no planned roadway improvements in the area.

A comparison of Figures 4 and 10 indicates that the Stockton Boulevard/T Street intersection is forecast to accommodate 23 percent more PM peak hour traffic under cumulative plus project conditions than currently exists. About 11 percent of this growth is attributable to the proposed project, while 89 percent of the growth is attributable to travel.

Like most travel demand models, the SACOG model is not sensitive to the effects of ramp metering on travel time and route choice. The model projected a net increase of 72 vehicles being added to the WB loop on-ramp. An even greater increase (184 PM peak hour vehicles) was projected for the EB diagonal on-ramp, which is not currently ramp metered. However, access to this on-ramp is adversely affected by queuing caused by ramp metering on the WB loop on-ramp. Thus, the cumulative forecasts shown in Figure 10 are considered conservative and may overstate the actual growth in traffic expected on the Stockton Boulevard corridor.



| 1. Stockton Blvd/35th St/US 50 WB Ramps | 2. Stockton Blvd/US 50 EB On-Ramp | 3. Stockton Blvd/T St/Gerber Ave | 4. 37th St/T St | | |
|--|--|---|---|--|--|
| (0, L) (1, L) | 1,048 (1,332) 4 (2) 1,048 (1,332) 1 (2) 341 (538) 35 | $\begin{array}{c} \begin{array}{c} & & & & & & & & & & & & & & & & & & &$ | Image: Second state Image: Second state Ima | | |
| 5. 39th St/T St | 6. 39th St/S St | 7. Stockton Blvd/New Driveway | | | |
| at si | 38th St | n Blvd | 1 Study Intersection | | |
| (157) (158) (46) | (0) 5 (14) (0) 1 (1) (0) 1 (1) (0) 1 (1) | 60) Siackian Biva | Project Site | | |
| 61 (78) 132 (262) 11 (21) | | (099) 80 81 81 81 81 81 81 81 81 81 81 81 81 81 | 🚽 Turn Lane | | |
| T Street | <u>s st</u> | New Driveway | AM (PM) Peak Hour Traffic Volume | | |
| 19 (50) | 10 (15) | ♥♥ ↑↑ @@ | Traffic Signal | | |
| 194 (262) ★ (366) 194 (262) ★ (366) 63 (23) 15 10 10 10 10 10 10 10 10 10 10 10 10 10 | (0) 0 (3) 3 (3) 5 (3) 7 (3) 8 (3) 8 (3 | 1,372 (1,856) ; 5 (8) | 👳 Stop Sign | | |

Figure 10

Peak Hour Traffic Volumes and Lane Configurations -Cumulative Plus Project Conditions



INTERSECTION OPERATIONS

Table 9 displays the operational results at the study intersections under cumulative plus project conditions. This table indicates that operations at the Stockton Boulevard/T Street intersection are expected to operate at LOS F during the PM peak hour.

| TABLE 9: INTERSECTION OPERATIONS – CUMULATIVE PLUS PROJECT CONDITIONS | | | | | | | |
|--|------------------|--------------------|--------|--------------------|-------|--|--|
| | | AM Pea | k Hour | PM Peak | Hour | | |
| Intersection | Control | Delay (sec/veh) | LOS | Delay (sec/veh) | LOS | | |
| 1. Stockton Boulevard/35 th Street/US 50 WB Ramps | Signal | 31.1 | С | 55.7 | Е | | |
| 2. Stockton Boulevard/US 50 EB Ramps | Uncontrolled | 3.7 (18.4) | A (C) | 24.3 (108.0) | C (F) | | |
| 3. Stockton Boulevard/T Street/Gerber Avenue | Signal | 37.0 | D | 185.2 | F | | |
| 4. T Street/37 th Street | Side-Street Stop | 2.1 (6.3) | A (A) | 9.6 (22.3) | A (C) | | |
| 5. T Street/39 th Street | Signal | 15.7 | В | 16.6 | В | | |
| 6. S Street/39 th Street | Side-Street Stop | 0.8 (8.0) | A (A) | 1.0 (7.1) | A (A) | | |
| Notes: | | • | | | | | |

¹ For signalized intersections, the LOS is based on the average delay experienced by all vehicles passing through the intersection. For uncontrolled and side-street stop controlled intersections, the delay and LOS for the worst case movement (in parentheses) is reported along with the average delay for the entire intersection and for the overall movement not in parentheses.

Source: Fehr & Peers, 2015

Due to the severity of congestion under this scenario, maximum vehicle queue estimates are not provided.

TRIP GENERATION COMPARISON

If the proposed project is not approved and constructed, then it is probable that the existing office building would remain and have new tenants. **Table 10** compares the expected vehicular trip generation between the existing office building and the proposed project on a daily basis, and during the AM and PM peak hours. This table shows that the proposed project would generate 35 percent less AM peak hour traffic and 17 percent less PM peak hour traffic when compared to the trip generation potential of the existing office building. On a daily basis, the proposed project would generate 7 percent less traffic than the office building.

However, the proposed project would generate substantially greater number of AM peak hour outbound and PM peak hour inbound trips when compared to the office building due to the differing directional travel characteristics between residential and office projects.

| | | TRIP GEN | TABLE 10: IERATION CO | MPARISON | | | |
|--------------------------------------|--|---------------|--------------------------|---------------|-----------------|---------------|---------------|
| | External AM Peak Hour Vehicle Trips External PM Peak Hour Vehicl | | | | | /ehicle Trips | |
| Scenario | Vehicle Trips | In | Out | Total | In | Out | Total |
| Proposed Project | 1,178 | 19 | 64 | 83 | 68 | 41 | 109 |
| Office Building (120,000 sq. ft.) | 1,099 | 113 | 15 | 128 | 22 | 110 | 132 |
| Difference ¹ | +79 (+7%) | -94 (-83%) | + 49 (+327%) | -45 (-35%) | + 46 (+209%) | -69 (-63%) | -23 (-17%) |

Notes:

1. Difference in trips calculated as follows: Plus Project minus No Project. Results shown in green represent a reduction in vehicle trips due to the proposed land use change. Results shown in red represent an increase in vehicle trips due to the proposed land use change.

5. PROJECT ACCESS AND CIRCULATION EVALUATION

This chapter analyzes the following access provisions for the proposed project:

- Proposed on-street angled parking on T Street
- Right-turn only driveway on Stockton Boulevard
- Full access driveway on 37th Street
- Single-family residence driveway locations
- Proposed lane width modifications on Stockton Boulevard

In addition, the project site plan's proposed on-site circulation system is also reviewed. The recommendations from this chapter are illustrated on **Figure 11**.

PROPOSED ON-STREET PARKING ON T STREET

The project site plan shows eight (8) traditional angled parking spaces along T Street between Stockton Boulevard and 37th Street. The City of Sacramento has an on-street angled parking program³ for streets, which begins with a request petition followed by a flow chart that outlines the request and evaluation process. The flow chart includes several minimum criteria for considering angled parking. One criterion is that the average daily traffic (ADT) volume not exceed 4,000 vehicles. Although an ADT value is not available for this segment of T Street, it is estimated to carry 6,700 vehicles per day based on an industry-standard assumption that 10 percent of the daily volume occurs during the PM peak hour. Therefore, the placement of angled parking on this segment of T Street would conflict with this minimum requirement. Additionally, it is noted that angled parking would not function very well from an operational perspective due to lengthy westbound right-turn queues that would frequent block ingress/egress to the spaces. Accordingly, Fehr & Peers recommends the following:

• Replace the proposed angled parking on T Street with parallel parking and limit the length of parallel parking so that spaces (likely to be three or four total) do not encroach into the right-turn lane.

Motorists on eastbound T Street may be tempted to perform a u-turn at 37th Street to access on-street parking on westbound T Street. The width of the T Street/37th Street intersection is sufficient so as to allow this movement. However, any vehicles performing this movement would effectively block continuing eastbound through traffic. And the u-turn movement may experience additional delays due to westbound T Street traffic queuing back from Stockton Boulevard into the intersection. Accordingly, Fehr & Peers recommends the following:

³ Found at: <u>http://portal.cityofsacramento.org/Public-Works/Transportation/Programs-and-Services/Angle-Parking</u>

• Post a "No U-turn" sign in the median planter island that is visible to eastbound traffic approaching the T Street/37th Street intersection.

RIGHT-TURN ONLY DRIVEWAY ON STOCKTON BOULEVARD

According to the SimTraffic results, this driveway is expected to have a maximum queue length of three (3) outbound vehicles (or 75 feet). The site plan indicates that in excess of 75 feet of storage is provided on-site. Therefore, no queuing problems are expected at this driveway.

The proposed driveway is 30 feet wide, which is sufficient to accommodate simultaneous inbound and outbound traffic. This driveway meets all applicable dimensions and spacing requirements as set forth in the City's zoning code (<u>http://www.qcode.us/codes/sacramento/</u>).

FULL ACCESS DRIVEWAY ON 37TH STREET

The most recent project site plan (dated 1/22/2015) includes project access from the 37th Street/S Street intersection. The proposed design of a conventional three-way intersection represents an improvement over the previous configuration in which the driveway was a 'cut' within the curb radius of the existing intersection. The proposed driveway is 26 feet wide, which is sufficient to accommodate simultaneous inbound and outbound traffic. Crosswalks are proposed on all approaches to the intersection. For these reasons, operational or safety problems are not expected at this driveway, and no recommendations are offered.

SINGLE-FAMILY RESIDENCE DRIVEWAY LOCATIONS

The project site plan has been modified to eliminate three (3) single-family residences with driveways that were proposed to front onto 39th Street. Access to these areas would instead be provided by a new internal street that extends between S Street and 39th Street.

PROPOSED LANE WIDTH MODIFICATIONS ON STOCKTON BOULEVARD

The project site plan indicates that the width of the travel lanes on Stockton Boulevard would be modified such that a narrow 2-foot raised median could be constructed northerly from T Street for a distance of about 140 feet. This would restrict movements at the project driveway to right-turns only. To accommodate the raised median, the width of the outside southbound through lane is proposed to be decreased from 18 to 14 feet. While this lane width is typically more than adequate, the southbound Stockton Boulevard right-turn movement onto westbound T Street requires a greater than 90-degree turn. Accordingly, Fehr & Peers recommends the following:

• The project applicant should confirm that the proposed lane width modifications along Stockton Boulevard provide adequate lane alignments and still enable trucks to turn right onto westbound T Street.

REVIEW OF ON-SITE CIRCULATION

An internal drive aisle would connect the Stockton Boulevard driveway with the S Street driveway. This internal roadway would generally be 20-feet wide with the exception of widening to 25 feet along the curvature in the northwest quadrant of the project site.

Motorists exiting the parking garage access (on the north side of the project site) could potentially have an impeded line of sight of oncoming driveway traffic due to trees (looking to the left) and a trash enclosure (looking to the right). Accordingly, Fehr & Peers recommends the following:

• Ensure that adequate sight distance is provided at parking garage access.



Project Site

Figure 11

Recommendations

6. IMPACTS AND MITIGATION MEASURES

This chapter evaluates the significance of project impacts using the criteria described in Chapter 1. Where impacts are deemed significant according to the criteria, mitigation measures are recommended to lessen their significance.

EVALUATION OF POTENTIAL INTERSECTION IMPACTS

Table 6 indicates that the proposed project would cause the average delay at the Stockton Boulevard/T Street intersection to increase from 56 to 71 seconds per vehicle during the PM peak hour. Since LOS E operations would be maintained and are considered acceptable at this location, the added delay, in and of itself, is not considered a significant impact. However, the effects of the project on increased vehicle queuing and the ability to safely pass through the Stockton Boulevard/T Street intersection are considered significant.

The southbound left-turn is the primary movement of concern. During the PM peak hour, the project would cause the volume in this turn lane to increase from 33 to 53 vehicles. Only 25 percent of existing left-turn traffic is able to perform this movement during the green indication, with 75 percent making this movement during the yellow or all-red phase. On average, there are about 40 cycles per hour at this intersection. The addition of 20 project trips means an average of one more vehicle turning left every other cycle. This additional traffic would cause more frequent instances in which two vehicles simultaneously wait in the southbound left-turn lane throughout the green indication, and then both turn left (i.e., 'sneakers") during the yellow or all-red phase. ⁴

<u>Impact TR-1</u>: The addition of project traffic would cause adverse queuing effects and safety concerns in the southbound left-turn lane at the Stockton Boulevard/T Street intersection.

Mitigation Measure TR-1

The project applicant shall work with the City of Sacramento to modify the traffic signal at the Stockton Boulevard/T Street intersection to operate the northbound and southbound left-turns with protected phasing.

Table 11 describes proposed Mitigation Measure TR-1 in detail including timing, responsibility, and operational benefits. The effectiveness of this mitigation measure was tested using SimTraffic. The effectiveness of this mitigation was tested assuming a 4.5-second protected left-turn phase, followed by a 3.5-second yellow phase. In addition, the maximum green time for the north-south through phase was increased by eight seconds and east-west through phase maximum green time was increased by six seconds based on

⁴ Although the existing office building would generate a greater number of total trips when compared to the project, the office building would not exacerbate this situation to the same degree as the proposed project. This is because the majority of inbound office trips are during the AM peak hour, and the majority of outbound office trips are during the PM peak hour.

preliminary SimTraffic results that showed otherwise substantially increased queuing. The net result was the cycle length increasing from 90 to 110 seconds.

Table 12 displays the the effectiveness of this mitigation measure under existing plus project conditions. As shown, operations would remain at an acceptable LOS E with this mitigation in place. The maximum vehicle queue in the southbound left-turn lane would be reduced, while the maximum vehicle queue in the northbound through lanes would increase.

This mitigation was also tested under cumulative plus project conditions. Operations would remain at LOS F with this mitigation in place. However, the average delay would decrease by four seconds.

| | TABLE 11: DETAILS OF MITIGATION MEASURE TR-1 | | | | |
|---|---|--|--|--|--|
| Торіс | Discussion | | | | |
| Physical / Operational Improvements | Mitigation Measure TR-1 would convert the northbound and southbound left-turn movements from permitted to protected. Instead of waiting for a gap in opposing traffic to perform their turn, motorists would turn left during a protected left-turn phase (in which a green arrow would be shown). This mitigation would require the replacement of the signal poles in the southwest and northeast quadrants of the intersection with larger poles that can accommodate longer mast arms and a greater load. Modifications to the Type 1-B poles in the southeast and northwest quadrants would also be necessary. A preliminary review of the proposed improvements suggests they are feasible. | | | | |
| Mitigation Effectiveness | <u>Level of Service</u> : LOS E is maintained (see Table 12). <u>Queuing</u> : Maximum expected queue would not exceed the available storage in the southbound left-turn lane (see Table 12). <u>Safety</u> : Benefits provided by operating left-turn with protected signal phase. | | | | |
| Timing | To be completed prior to building occupancy | | | | |
| Responsibility | To be implemented by project applicant. | | | | |
| Source: Fehr & Peers, 2015 | | | | | |

Mitigation Measure TR-1 would reduce Impact TR-1 to *less than significant*.

| TABLE 12: MITIGATION MEASURE EFFECTIVENESS AT STOCKTON BOULEVARD/T STREET INTERSECTION – EXISTING PLUS PROJECT CONDITIONS | | | | | | | |
|---|-------------------------------|-----------------------------------|-----------|------------|-----------------|---|--|
| | | | | | PM Peak Hou | r | |
| Intersection | Performance | nce Standard Available Storage | | Existing | Existing Plus P | roject Conditions | |
| | | | Storage | Conditions | No Mitigation | With Protected Left- Turn Phasing ² | |
| | Overall Average Delay | | | 55.9 | 71.2 | 68.2 | |
| | Overall | LOS | | E | E | E | |
| Stockton Blvd. Ln / T Street / | | SB Left- Turn Lane | 175 ft. | 25 ft. | 125 ft. | 50 ft. | |
| Gerber Ave. | Maximum Queue ¹ | NB Through/ Right Lane | 1,100 ft. | 750 ft. | 1,000 ft. | 875 ft. | |

Notes:

¹ All queues are expressed on a 'per lane" basis. Modeled results based on 95th percentile queue length reported from SimTraffic. Queue lengths are rounded to 25' increments based on an average car length of 25'.

² This mitigation test consists of adding a protected phase for the northbound and southbound left-turn lanes (refer to previous text for detailed signal timing parameters).

Source: Fehr & Peers, 2015.

Project impacts at this intersection under cumulative conditions are considered **less than significant** because the No Project condition (i.e., office building remains and is occupied by tenants) would cause greater increases in delays due to its greater AM and PM peak hour trip generation.

The average delay on the yield-controlled US 50 EB on-ramp/Stockton Boulevard intersection southbound left-turn movement would increase from 52 to 62 seconds per vehicle with the project. This represents a degradation of LOS F conditions. The increase in delay at this Caltrans-maintained intersection is not considered a significant impact because operations are at LOS F due to Caltrans operating a ramp meter on the westbound loop on-ramp. If this ramp meter were not in operation, this yield-controlled movement would operate at an acceptable LOS D. Thus, by operating the westbound loop on-ramp, Caltrans has decided to accept LOS F conditions at the US 50 EB on-ramp/Stockton Boulevard intersection.

EVALUATION OF BICYCLE IMPACTS

The proposed project would not interfere with any existing bicycle facilities. It would construct a Class II bicycle lane in the westbound direction of T Street approaching Stockton Boulevard. It would also not preclude construction of any new lanes such as a Class II lane on T Street, or a future Class II lane planned on Stockton Boulevard south of T Street. The project would include a 'bike lounge' and bicycle parking along its frontage on Stockton Boulevard. Proposed project impacts to bicycle facilities are considered **less-than-significant**. Therefore, mitigations are not required.

EVALUATION OF PEDESTRIAN IMPACTS

The proposed project would construct a pedestrian plaza area along its frontages on Stockton Boulevard and T Street. The proposed project would also construct a new five-foot wide sidewalk on the west side of 37th Street with gated pedestrian linkages into the apartment courtyards. It would also construct a sidewalk along the northern driveway between 37th Street and the parking garage entry. The proposed project would construct a new five-foot wide sidewalk on the north side of S Street. The project would provide accessible and safe pedestrian connections between its buildings and adjacent streets and transit facilities. The project would not disrupt existing or planned pedestrian facilities or conflict with adopted City pedestrian plans, guidelines, policies, or standards. For these reasons, proposed project impacts to pedestrian facilities are considered *less-than-significant*. Therefore, mitigations are not required.

EVALUATION OF POTENTIAL TRANSIT IMPACTS

According to Table 4, the proposed project could generate 11 new transit riders during the AM peak hour and 13 new transit riders during the PM peak hour. These riders may use light rail via the 39th Street Gold line stop, public bus (via Routes 38, and 212/213/214), and the Capital City Hospital Shuttle, which transports employees, patients, and visitors to the Mercy, Sutter, UC Davis Medical Centers located in Midtown and East Sacramento. Each of these routes can be accessed via existing pedestrian facilities including sidewalks and crosswalks. Since operations would remain at an acceptable LOS E at the Stockton Boulevard/T Street intersection, the project would not adversely affect public transit operations. The project would not disrupt existing or planned transit facilities or conflict with adopted City transit plans, guidelines, policies, or standards. For these reasons, proposed project impacts to transit facilities are considered *less-than-significant*. Therefore, mitigations are not required.

EVALUATION OF POTENTIAL EMERGENCY VEHICLE ACCESS IMPACTS

The proposed project would not result in inadequate emergency access during construction and/or operation. The Stockton Boulevard/T Street intersection features emergency vehicle pre-emption on all four approaches. For these reasons, proposed project impacts to emergency vehicle access are considered **less-than***significant*. Therefore, mitigations are not required.

EVALUATION OF POTENTIAL CONSTRUCTION IMPACTS

Construction of the proposed project would generate a variety of truck and employee trips during demolition of the existing office building, and construction of the proposed project. Since the magnitude of these trips during peak hours would be less than that of the proposed project, absolute impacts (in terms of delay and queuing) when compared to project operations would not be significant. Construction staging and lane closures could cause adverse effects if not carefully planned. Thus, the project could potentially cause a temporary but prolonged impact due to lane closures, traffic hazards to bikes/pedestrians, damage to roadbed, or truck traffic on roadways not designated as truck routes. For these reasons, proposed project impacts during construction are potentially *significant*.

Mitigation TR-2

The project applicant shall develop a Construction Traffic Management Plan to the satisfaction of the City's Community Development Department. The plan would include items such as: the number and size of trucks per day, expected arrival/departure times, truck circulation patterns, location of truck staging areas, location/amount of employee parking, and the proposed use of traffic control/partial street closures on public streets. The overall goal of the Construction Traffic Management Plan would be to minimize traffic impacts to public streets and maintain a high level of safety for all roadway users. The Construction TMP shall adhere to the following performance standards throughout project construction:

- 1) Delivery trucks do not idle/stage on Stockton Boulevard and T Street.
- *2)* With the exception of trucks coming from local destinations via 39th Street, all delivery trucks shall use Stockton Boulevard to access the site.
- 3) Any lane closures on northbound Stockton Boulevard during the demolition of the existing office building or proposed project construction are limited to a single lane during off-peak hours (9:00 AM to 2:30 PM).
- 4) Roadways, sidewalks, crosswalks, and bicycle facilities shall be maintained clear of debris (e.g., rocks) that could otherwise impede travel and impact public safety.

Implementation of this mitigation measure would reduce this impact to a *less than significant* level.

Each of the above conclusions regarding the significance of project impacts applies to both project-specific impacts and cumulatively considerable impacts.

APPENDIX A: EXISTING INTERSECTION CONDITIONS



SimTraffic Post-Processor Average Data from 10 Runs Intersection Volume and Delay

| Stockton & T |
|----------------------------|
| Existing Conditions |
| AM Peak Hour |

| | | Demand Volume | | Serv Percent | ved Volume (Standard | (vph) | | | Tota | al Delay (sec/ | ′veh) | |
|---------------------------------------|------------------|------------------|---------|-----------------|--------------------------|---------|---------|---------|-----------|----------------|---------|-----|
| Intersection | Control | (vph) | Average | Served | Deviation | Minimum | Maximum | Average | Std. Dev. | Minimum | Maximum | LOS |
| 1 Stockton Blvd/35th St-WB HWY 50 ram | | 2,382 | 2,405 | 101.0% | 118 | 2,240 | 2,644 | 23.5 | 4.9 | 16.9 | 32.6 | С |
| 2 Stockton Blvd/none-EB HWY 50 on ram | | 1,944 | 1,949 | 100.2% | 90 | 1,824 | 2,080 | 10.5 | 2.0 | 8.5 | 14.2 | В |
| 4 37th St-none/T St | Side-street Stop | 478 | 467 | 97.7% | 66 | 344 | 560 | 6.2 | 4.2 | 0.0 | 14.7 | A |
| 5 39th St/T St | Signal | 846 | 832 | 98.3% | 54 | 724 | 920 | 14.1 | 1.2 | 12.1 | 16.6 | В |
| 6 39th St/S St | Side-street Stop | 457 | 444 | 97.2% | 45 | 380 | 516 | 3.5 | 5.0 | 0.0 | 12.8 | А |
| 3 Stockton Blvd/T St | Signal | 2 548 | 2,540 | 99.7% | 91 | 2 272 | 2 554 | 25.9 | 5.7 | 20.7 | 40.0 | C |
| 3 Stockton Bivd/1 St | Signal | 2,548 | 2,540 | 99.7% | 91 | 2,372 | 2,664 | 25.9 | 5.7 | 20.7 | 40.0 | С |
| Network Summa | | - | | | | | | | | | | |
| Total Demand Volume (veh/hr) | 8,655 | - | | | | | | | | | | |
| Total Volume Served (veh/hr) | 8,636 | | | | | | | | | | | |
| Percent Served | 99.8% | | | | | | | | | | | |
| GEH Statistic | 0.2 | | | | | | | | | | | |

Stockton & T Existing Conditions AM Peak Hour

Intersection 1

Stockton Blvd/35th St-WB HWY 50 ramps

Signal

| | | Demand | Served Vo | lume (vph) | Total | Delay (sec/ve | h) |
|-----------|------------|--------------|-----------|------------|---------|---------------|-----|
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS |
| | Left Turn | 6 | 8 | 126.7% | 37.0 | 23.2 | D |
| NB | Through | 443 | 443 | 100.0% | 14.9 | 2.0 | В |
| IND | Right Turn | 410 | 410 | 99.9% | 7.3 | 0.9 | А |
| | Subtotal | 859 | 860 | 100.1% | 11.5 | 1.4 | В |
| | Left Turn | 42 | 44 | 103.8% | 30.3 | 12.6 | С |
| SB | Through | 380 | 387 | 101.9% | 14.0 | 2.2 | В |
| 30 | Right Turn | 2 | 2 | 100.0% | 0.4 | 1.4 | А |
| | Subtotal | 424 | 433 | 102.1% | 15.6 | 2.0 | В |
| EB | Left Turn | 10 | 11 | 108.0% | 35.2 | 18.2 | D |
| | Through | 58 | 62 | 106.2% | 40.5 | 18.5 | D |
| LD | Right Turn | 72 | 61 | 85.0% | 20.2 | 12.2 | С |
| | Subtotal | 140 | 134 | 95.4% | 31.0 | 15.7 | С |
| | Left Turn | 314 | 312 | 99.5% | 53.6 | 16.1 | D |
| WB | Through | 73 | 69 | 94.8% | 54.1 | 14.8 | D |
| VVD | Right Turn | 572 | 597 | 104.3% | 25.5 | 11.2 | С |
| | Subtotal | 959 | 978 | 102.0% | 36.5 | 11.1 | D |
| | Total | 2,382 | 2,405 | 101.0% | 23.5 | 4.9 | С |

Intersection 2

Stockton Blvd/none-EB HWY 50 on ramp

Uncontrolled

| | | Demand | Served Vo | lume (vph) | Total | Delay (sec/ve | h) |
|-----------|------------|--------------|-----------|------------|---------|---------------|-----|
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS |
| | Left Turn | | | | | | |
| NB | Through | 857 | 859 | 100.3% | 1.0 | 0.1 | А |
| IND | Right Turn | 321 | 317 | 98.7% | 1.0 | 0.1 | А |
| | Subtotal | 1,178 | 1,176 | 99.8% | 1.0 | 0.1 | А |
| | Left Turn | 202 | 195 | 96.4% | 10.5 | 2.0 | В |
| SB | Through | 564 | 578 | 102.5% | 0.9 | 0.1 | А |
| 30 | Right Turn | | | | | | |
| | Subtotal | 766 | 773 | 100.9% | 3.3 | 0.6 | А |
| | Left Turn | | | | | | |
| EB | Through | | | | | | |
| LD | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| | Left Turn | | | | | | |
| WB | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| | Total | 1,944 | 1,949 | 100.2% | 1.9 | 0.3 | А |

Intersection 4

37th St-none/T St

| Side-street S | Stop |
|---------------|------|
|---------------|------|

Existing Conditions

Stockton & T

AM Peak Hour

| | | Demand | Served Vo | lume (vph) | Total | Delay (sec/vel | h) |
|-----------|------------|--------------|-----------|------------|---------|----------------|-----|
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS |
| | Left Turn | | | | | | |
| NB | Through | | | | | | |
| IND | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| | Left Turn | 7 | 10 | 142.9% | 6.2 | 4.2 | Α |
| SB | Through | | | | | | |
| 30 | Right Turn | 20 | 18 | 90.0% | 3.0 | 1.0 | А |
| SB | Subtotal | 27 | 28 | 103.7% | 4.2 | 1.1 | А |
| | Left Turn | 15 | 16 | 106.7% | 3.5 | 1.4 | А |
| EB | Through | 253 | 244 | 96.4% | 2.5 | 0.4 | А |
| ED | Right Turn | | | | | | |
| | Subtotal | 268 | 260 | 97.0% | 2.5 | 0.4 | А |
| | Left Turn | | | | | | |
| WB | Through | 180 | 174 | 96.4% | 1.0 | 0.1 | А |
| VVD | Right Turn | 3 | 5 | 173.3% | 0.4 | 0.7 | А |
| | Subtotal | 183 | 179 | 97.7% | 1.0 | 0.2 | А |
| | Total | 478 | 467 | 97.7% | 2.1 | 0.3 | А |

Intersection 5

39th St/T St

Signal

| | I | Demand | Served Vo | lume (vph) | Total | Delay (sec/ve | h) |
|-----------|------------|--------------|-----------|------------|---------|---------------|-----|
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS |
| | Left Turn | 6 | 5 | 80.0% | 10.9 | 11.6 | В |
| NB | Through | 131 | 146 | 111.1% | 12.0 | 2.1 | В |
| IND | Right Turn | 11 | 13 | 116.4% | 4.6 | 3.5 | А |
| | Subtotal | 148 | 163 | 110.3% | 11.7 | 1.9 | В |
| | Left Turn | 30 | 23 | 76.0% | 30.4 | 7.5 | С |
| C D | Through | 161 | 158 | 98.1% | 27.9 | 2.1 | С |
| 30 | Right Turn | 49 | 45 | 91.4% | 19.8 | 3.3 | В |
| SB | Subtotal | 240 | 226 | 94.0% | 26.6 | 2.3 | С |
| | Left Turn | 19 | 14 | 73.7% | 10.5 | 6.6 | В |
| EB | Through | 181 | 171 | 94.4% | 10.6 | 3.0 | В |
| LD | Right Turn | 60 | 62 | 102.7% | 8.2 | 2.3 | А |
| | Subtotal | 260 | 246 | 94.8% | 10.0 | 2.5 | В |
| | Left Turn | 11 | 17 | 152.7% | 9.3 | 4.6 | А |
| \A/D | Through | 128 | 126 | 98.8% | 7.4 | 1.5 | А |
| WB | Right Turn | 59 | 53 | 90.2% | 3.2 | 1.6 | А |
| | Subtotal | 198 | 196 | 99.2% | 6.5 | 1.3 | А |
| | Total | 846 | 832 | 98.3% | 14.1 | 1.2 | В |

~

Stockton & T Existing Conditions AM Peak Hour

Side-street Stop

Intersection 6

39th St/S St

Served Volume (vph) Demand Total Delay (sec/veh) Direction Movement Volume (vph) Average Percent Average Std. Dev. LOS Left Turn 2 1 60.0% 0.9 1.6 А 207 212 Through 102.2% 1.1 0.2 А NB **Right Turn** Subtotal 209 213 101.8% 1.1 0.2 А Left Turn Through 235 218 92.6% 0.3 0.1 А SB **Right Turn** 4 4 90.0% 0.0 0.1 А Subtotal 239 221 92.6% 0.3 0.1 А Left Turn Through EB Right Turn 5 5 104.0% 2.1 1.5 А Subtotal 5 5 104.0% 2.1 1.5 А Left Turn Through 3 2 53.3% 3.5 5.0 А WB Right Turn 1 3 320.0% 1.7 1.5 А Subtotal 4 5 120.0% 4.5 3.5 А Total 457 444 97.2% 0.7 0.1 А

Intersection 0

Side-street Stop

Intersection 3

Stockton Blvd/T St

| | | Demand | Served Vo | lume (vph) | Total | Delay (sec/vel | n) |
|-----------|------------|--------------|-----------|------------|---------|----------------|-----|
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS |
| | Left Turn | 48 | 46 | 95.0% | 41.4 | 7.7 | D |
| NB | Through | 910 | 923 | 101.5% | 19.1 | 3.5 | В |
| ND | Right Turn | 22 | 20 | 89.1% | 21.0 | 6.4 | С |
| | Subtotal | 980 | 988 | 100.9% | 20.2 | 3.3 | С |
| | Left Turn | 23 | 21 | 92.2% | 40.1 | 18.2 | D |
| SB | Through | 518 | 538 | 103.9% | 12.6 | 1.0 | В |
| 50 | Right Turn | 23 | 20 | 87.0% | 8.3 | 4.9 | А |
| | Subtotal | 564 | 579 | 102.7% | 13.4 | 1.2 | В |
| | Left Turn | 106 | 98 | 92.8% | 38.2 | 12.7 | D |
| EB | Through | 224 | 214 | 95.7% | 35.2 | 14.5 | D |
| LD | Right Turn | 443 | 436 | 98.4% | 49.6 | 18.9 | D |
| | Subtotal | 773 | 749 | 96.9% | 43.9 | 16.3 | D |
| | Left Turn | 25 | 26 | 104.0% | 39.7 | 12.6 | D |
| NE | Through | | | | | | |
| | Right Turn | 3 | 5 | 173.3% | 29.5 | 22.8 | С |
| | Subtotal | 28 | 31 | 111.4% | 39.6 | 9.6 | D |
| | Left Turn | 9 | 6 | 71.1% | 21.9 | 18.1 | С |
| WB | Through | 52 | 46 | 87.7% | 17.6 | 5.6 | В |
| VV D | Right Turn | 142 | 140 | 98.9% | 20.3 | 3.4 | С |
| | Subtotal | 203 | 192 | 94.8% | 20.0 | 1.6 | В |
| | Total | 2,548 | 2,540 | 99.7% | 25.9 | 5.7 | С |

Stockton & T Existing Conditions AM Peak Hour

Signal

SimTraffic Post-Processor Average Data from 10 Runs Intersection Volume and Delay

| Stockton & T |
|----------------------------|
| Existing Conditions |
| PM Peak hour |

| | | | Demand | | Ser | ved Volume | (vph) | ĺ | | | | | |
|------|--|------------------|--------|---------|---------|------------|---------|---------|---------|-----------|----------------|-------|-----|
| | | | Volume | | Percent | Standard | | | | Tota | al Delay (sec/ | /veh) | |
| | Intersection | Control | (vph) | Average | Served | Deviation | Minimum | Maximum | Average | Std. Dev. | | | LOS |
| 1 | Stockton Blvd-Stockton/35th Street-WB HWY 50 ramps | Signal | 2,804 | 2,651 | 94.6% | 116 | 2,492 | 2,836 | 43.4 | 7.9 | 34.2 | 62.7 | D |
| 2 | Stockton Blvd-Stockton/none-EB HWY 50 on-ramp | Uncontrolled | 2,380 | 2,237 | 94.0% | 107 | 2,076 | 2,380 | 52.1 | 26.7 | 20.9 | 110.7 | F |
| | | | | | | | | | | | | | |
| 4 | 37th Street/T Street | Side-street Stop | 668 | 664 | 99.4% | 66 | 588 | 772 | 24.8 | 29.6 | 12.6 | 108.8 | С |
| 5 | 39th Street/T Street | Signal | 1,112 | 1,093 | 98.3% | 78 | 972 | 1,212 | 14.8 | 8.6 | 10.9 | 39.2 | В |
| 6 | 39th Street/S Street | Side-street Stop | 543 | 532 | 98.0% | 26 | 496 | 572 | 7.4 | 2.0 | 5.2 | 12.1 | А |
| | | | | | | | | | | | | | |
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| | | | | | | | | | | | | | |
| 3 | Stockton Blvd-Gerber Avenue/T Street | Signal | 2,767 | 2,639 | 95.4% | 147 | 2,316 | 2,816 | 55.9 | 15.6 | 26.6 | 78.4 | Е |
| J | Stockton blvd-derber Avender i Street | Jigilai | 2,707 | 2,035 | 55.470 | 147 | 2,510 | 2,010 | 55.5 | 15.0 | 20.0 | 70.4 | L |
| | Network Summary | | | | | | | | | | | | |
| Tota | al Demand Volume (veh/hr) | 10,274 | | | | | | | | | | | |
| | al Volume Served (veh/hr) | 9,817 | | | | | | | | | | | |
| | cent Served | 95.5% | | | | | | | | | | | |
| | I Statistic | 4.6 | | | | | | | | | | | |
| GLI | i Statistic | 4.0 | | | | | | | | | | | |

Stockton & T Existing Conditions PM Peak hour

Intersection 1

Stockton Blvd-Stockton/35th Street-WB HWY 50 ramps

Signal

| | | Demand | Served Vo | lume (vph) | Total | Delay (sec/ve | h) |
|-----------|------------|--------------|-----------|------------|---------|---------------|-----|
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS |
| | Left Turn | 14 | 18 | 128.6% | 30.9 | 12.2 | С |
| NB | Through | 492 | 476 | 96.8% | 19.3 | 2.6 | В |
| ND | Right Turn | 614 | 532 | 86.7% | 103.0 | 5.5 | F |
| | Subtotal | 1,120 | 1,027 | 91.7% | 63.1 | 3.5 | E |
| | Left Turn | 73 | 69 | 94.8% | 76.1 | 47.4 | E |
| SB | Through | 621 | 600 | 96.6% | 38.7 | 28.6 | D |
| 50 | Right Turn | 8 | 8 | 95.0% | 8.7 | 9.2 | А |
| | Subtotal | 702 | 676 | 96.4% | 42.5 | 30.4 | D |
| | Left Turn | 16 | 20 | 122.5% | 37.1 | 19.5 | D |
| EB | Through | 49 | 48 | 98.0% | 49.6 | 22.0 | D |
| LD | Right Turn | 30 | 37 | 124.0% | 32.1 | 28.7 | С |
| | Subtotal | 95 | 105 | 110.3% | 40.9 | 21.7 | D |
| | Left Turn | 184 | 183 | 99.3% | 32.3 | 13.3 | С |
| WB | Through | 133 | 120 | 90.5% | 33.1 | 11.7 | С |
| VVD | Right Turn | 570 | 540 | 94.7% | 13.6 | 4.8 | В |
| | Subtotal | 887 | 843 | 95.1% | 20.4 | 7.3 | С |
| | Total | 2,804 | 2,651 | 94.6% | 43.4 | 7.9 | D |

Intersection 2

Stockton Blvd-Stockton/none-EB HWY 50 on-ramp

Uncontrolled

| | | Demand | Served Vo | lume (vph) | Total | Delay (sec/ve | h) |
|-----------|------------|--------------|-----------|------------|---------|---------------|-----|
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS |
| | Left Turn | | | | | | |
| NB | Through | 1,120 | 1,035 | 92.4% | 9.8 | 3.2 | А |
| IND | Right Turn | 417 | 374 | 89.7% | 8.6 | 2.6 | А |
| | Subtotal | 1,537 | 1,409 | 91.7% | 9.5 | 3.0 | А |
| | Left Turn | 376 | 362 | 96.2% | 52.1 | 26.7 | F |
| SB | Through | 467 | 467 | 100.0% | 1.3 | 0.3 | А |
| 50 | Right Turn | | | | | | |
| | Subtotal | 843 | 828 | 98.3% | 23.6 | 11.8 | С |
| | Left Turn | | | | | | |
| EB | Through | | | | | | |
| LD | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| | Left Turn | | | | | | |
| WB | Through | | | | | | |
| 0 00 | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| | Total | 2,380 | 2,237 | 94.0% | 14.8 | 4.6 | В |

Intersection 0

Stockton & T Existing Conditions PM Peak hour

Signal

| | | Demand | Served Vo | lume (vph) | Total | Delay (sec/ve | h) |
|-----------------------------------|------------|--------------|-----------|------------|---------|---------------|------|
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS |
| | Left Turn | #N/A | #N/A | #N/A | #N/A | #N/A | #N/A |
| ND | Through | #N/A | #N/A | #N/A | #N/A | #N/A | #N/A |
| IND | Right Turn | #N/A | #N/A | #N/A | #N/A | #N/A | #N/A |
| | Subtotal | #N/A | #N/A | #N/A | #N/A | #N/A | #N/A |
| | Left Turn | #N/A | #N/A | #N/A | #N/A | #N/A | #N/A |
| CD | Through | #N/A | #N/A | #N/A | #N/A | #N/A | #N/A |
| Direction NB SB EB WB | Right Turn | #N/A | #N/A | #N/A | #N/A | #N/A | #N/A |
| | Subtotal | #N/A | #N/A | #N/A | #N/A | #N/A | #N/A |
| | Left Turn | #N/A | #N/A | #N/A | #N/A | #N/A | #N/A |
| | Through | #N/A | #N/A | #N/A | #N/A | #N/A | #N/A |
| ED | Right Turn | #N/A | #N/A | #N/A | #N/A | #N/A | #N/A |
| | Subtotal | #N/A | #N/A | #N/A | #N/A | #N/A | #N/A |
| | Left Turn | #N/A | #N/A | #N/A | #N/A | #N/A | #N/A |
| | Through | #N/A | #N/A | #N/A | #N/A | #N/A | #N/A |
| WB | Right Turn | #N/A | #N/A | #N/A | #N/A | #N/A | #N/A |
| | Subtotal | #N/A | #N/A | #N/A | #N/A | #N/A | #N/A |
| | Total | #N/A | #N/A | #N/A | #N/A | #N/A | #N/A |

Intersection 4

37th Street/T Street

Side-street Stop

| | | Demand | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|--------------|---------------------|---------|-----------------------|-----------|-----|
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS |
| NB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| SB | Left Turn | 1 | 0 | 40.0% | 13.3 | 1.8 | В |
| | Through | | | | | | |
| | Right Turn | 10 | 9 | 92.0% | 24.8 | 29.6 | С |
| | Subtotal | 11 | 10 | 87.3% | 22.0 | 31.2 | С |
| EB | Left Turn | 14 | 14 | 100.0% | 7.7 | 4.8 | А |
| | Through | 326 | 314 | 96.2% | 3.6 | 0.3 | А |
| | Right Turn | | | | | | |
| | Subtotal | 340 | 328 | 96.4% | 3.8 | 0.4 | А |
| WB | Left Turn | | | | | | |
| | Through | 314 | 324 | 103.3% | 22.3 | 51.7 | С |
| | Right Turn | 3 | 2 | 80.0% | 0.4 | 0.7 | Α |
| | Subtotal | 317 | 327 | 103.1% | 22.3 | 51.7 | С |
| Total | | 668 | 664 | 99.4% | 12.9 | 24.5 | В |

Intersection 5

39th Street/T Street

| | | Demand | Served Vo | lume (vph) | Total | Delay (sec/vel | n) |
|-----------|------------|--------------|-----------|------------|---------|----------------|-----|
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS |
| | Left Turn | 14 | 17 | 122.9% | 39.9 | 75.5 | D |
| NB | Through | 171 | 173 | 101.1% | 20.0 | 19.8 | В |
| ND | Right Turn | 33 | 32 | 97.0% | 14.8 | 25.0 | В |
| | Subtotal | 218 | 222 | 101.8% | 20.9 | 24.5 | С |
| | Left Turn | 39 | 34 | 86.2% | 22.8 | 21.4 | С |
| SB | Through | 152 | 148 | 97.4% | 15.3 | 8.5 | В |
| 30 | Right Turn | 55 | 50 | 91.6% | 12.3 | 13.2 | В |
| | Subtotal | 246 | 232 | 94.3% | 15.7 | 11.0 | В |
| | Left Turn | 48 | 48 | 100.0% | 16.1 | 4.7 | В |
| EB | Through | 259 | 247 | 95.4% | 12.5 | 2.4 | В |
| ED | Right Turn | 20 | 14 | 68.0% | 11.3 | 5.6 | В |
| | Subtotal | 327 | 309 | 94.4% | 13.1 | 2.2 | В |
| | Left Turn | 11 | 10 | 90.9% | 15.5 | 14.5 | В |
| WB | Through | 248 | 256 | 103.4% | 12.3 | 4.9 | В |
| VVD | Right Turn | 62 | 64 | 103.2% | 6.1 | 1.4 | А |
| | Subtotal | 321 | 330 | 102.9% | 11.2 | 4.2 | В |

1,093

98.3%

14.8

Intersection 6

Total

39th Street/S Street

1,112

Side-street Stop

В

8.6

| | | Demand | Served Vo | lume (vph) | Total | Delay (sec/vel | h) |
|-----------|------------|--------------|-----------|------------|---------|----------------|-----|
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS |
| | Left Turn | 1 | 0 | 40.0% | 0.4 | 1.2 | А |
| NB | Through | 278 | 282 | 101.6% | 1.1 | 0.2 | А |
| IND | Right Turn | 2 | 2 | 80.0% | 0.7 | 1.0 | А |
| | Subtotal | 281 | 284 | 101.2% | 1.1 | 0.2 | А |
| | Left Turn | 1 | 1 | 80.0% | 0.7 | 1.7 | А |
| SB | Through | 241 | 228 | 94.8% | 1.0 | 2.4 | А |
| 30 | Right Turn | 6 | 6 | 100.0% | 0.7 | 2.1 | А |
| | Subtotal | 248 | 235 | 94.8% | 1.0 | 2.4 | А |
| | Left Turn | 9 | 9 | 97.8% | 7.4 | 2.0 | А |
| EB | Through | | | | | | |
| LD | Right Turn | 5 | 4 | 80.0% | 3.1 | 2.8 | А |
| | Subtotal | 14 | 13 | 91.4% | 6.4 | 2.4 | А |
| | Left Turn | | | | | | |
| WB | Through | | | | | | |
| VVD | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| | Total | 543 | 532 | 98.0% | 1.2 | 1.2 | А |

Stockton & T Existing Conditions PM Peak hour

| Intersection | 3 | Stockton Blvd-Gerber Avenue/T Street | | | | | | | |
|--------------|------------|--------------------------------------|-----------|------------|---------|----------------|-----|--|--|
| | | Demand | Served Vo | lume (vph) | Total | Delay (sec/veł | ו) | | |
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS | | |
| | Left Turn | 62 | 60 | 96.1% | 72.2 | 25.4 | E | | |
| NB | Through | 1,194 | 1,081 | 90.5% | 70.4 | 28.5 | Е | | |
| ND | Right Turn | 6 | 4 | 73.3% | 77.4 | 86.8 | Е | | |
| | Subtotal | 1,262 | 1,145 | 90.7% | 70.6 | 28.3 | Е | | |
| | Left Turn | 33 | 29 | 88.5% | 133.8 | 104.7 | F | | |
| SB | Through | 401 | 405 | 100.9% | 12.9 | 1.9 | В | | |
| 30 | Right Turn | 33 | 31 | 93.3% | 10.6 | 5.0 | В | | |
| | Subtotal | 467 | 465 | 99.5% | 22.3 | 12.7 | С | | |
| | Left Turn | 121 | 116 | 95.9% | 73.5 | 21.5 | E | | |
| EB | Through | 301 | 294 | 97.5% | 55.9 | 12.7 | Е | | |
| LD | Right Turn | 267 | 266 | 99.8% | 47.9 | 12.9 | D | | |
| | Subtotal | 689 | 676 | 98.1% | 56.0 | 13.8 | Е | | |
| | Left Turn | 24 | 19 | 78.3% | 87.0 | 82.6 | F | | |
| NE | Through | | | | | | | | |
| INC | Right Turn | 1 | 4 | 400.0% | 51.8 | 56.4 | D | | |
| _ | Subtotal | 25 | 23 | 91.2% | 75.7 | 63.4 | E | | |
| | Left Turn | 3 | 1 | 40.0% | 65.0 | 152.8 | E | | |
| WB | Through | 122 | 120 | 98.4% | 41.5 | 47.2 | D | | |
| VV D | Right Turn | 199 | 209 | 105.1% | 52.2 | 30.0 | D | | |
| | Subtotal | 324 | 330 | 102.0% | 50.4 | 33.0 | D | | |
| | Total | 2,767 | 2,639 | 95.4% | 55.9 | 15.6 | E | | |

| 12/22/201 | 4 |
|-----------|---|
|-----------|---|

Intersection: 3: Stockton Boulevard & T Street

| Movement | EB | EB | WB | WB | NB | NB | NB | SB | SB | SB | NE | |
|-----------------------|------|-----|--|-----|--|------|------|-----|-----|-----|-----------|--|
| Directions Served | LT | TR> | <lt< td=""><td>R</td><td><l< td=""><td>Т</td><td>TR</td><td>L</td><td>Т</td><td>TR></td><td><lr></lr></td><td></td></l<></td></lt<> | R | <l< td=""><td>Т</td><td>TR</td><td>L</td><td>Т</td><td>TR></td><td><lr></lr></td><td></td></l<> | Т | TR | L | Т | TR> | <lr></lr> | |
| Maximum Queue (ft) | 345 | 342 | 94 | 174 | 83 | 873 | 896 | 60 | 106 | 129 | 68 | |
| Average Queue (ft) | 249 | 257 | 32 | 89 | 23 | 536 | 577 | 23 | 60 | 73 | 35 | |
| 95th Queue (ft) | 392 | 392 | 88 | 201 | 87 | 981 | 988 | 83 | 114 | 138 | 85 | |
| Link Distance (ft) | 1512 | | 176 | 176 | | 3144 | 3144 | 117 | 117 | 117 | 336 | |
| Upstream Blk Time (%) | | | | 7 | | | | 3 | 1 | 1 | | |
| Queuing Penalty (veh) | | | | 12 | | | | 4 | 1 | 2 | | |
| Storage Bay Dist (ft) | | 425 | | | 100 | | | | | | | |
| Storage Blk Time (%) | 0 | 0 | | | 0 | 10 | | | | | | |
| Queuing Penalty (veh) | 1 | 0 | | | 0 | 6 | | | | | | |

APPENDIX B: MXD MODEL



MIXED USE TRIP GENERATION MODEL - BASIC INPUT

All shaded cells are inputs Regular inputs (project-specific) Inputs that may depend on regional values from census data, travel demand model, etc...

| Site Name | Stockton B | lvd./T Street | int/sq mi | 640 | | | | |
|--|--|--|---|---|---|---|--|--|
| Geographic | | Notes / Instructions | • | | | | | |
| Developed Area (in acres) | | Include streets, ROW | | | | | | |
| Number of Intersections | 5 | Count intersections e | either within or on th | e perimeter of the N | IXD. Check resultin | g intersection | is per square | e mile in blue abo |
| s Transit (bus or rail) present within the site or across the street? Proportion of households within 1/4 mile of a transit stop | Yes 100% | Enter as a percentag | 10 | | | | | |
| | 100 /0 | Enter us a percentag | | | | | | |
| Land Use - Surrounding Area | | Answering "Yes" will | reduce the HBO an | d NHB purpose spli | its for retail use to th | ose found in | smaller | |
| s the site in a Central Business District and/or TOD? | No | stores. The nature o | f the stores (large v | s. small) should be | | | | |
| Employment within one mile of the MXD | | Do not include emplo | oyment within the M | XD itself | | | | |
| Employment within a 30 minute Transit Trip (Door-to-door) | | Per Sacmet Model. | | | lf in the Onesute F | | | C |
| Fotal Regional Employment | 900,900 | Employment at MPO | or similar level | | If in the 9 county E | say Area, can | i use the wit | CJODSWITHINGOW |
| Site Demographics Enter Population Directly? | No | If "No", will apply ave | rage HH size factor | rs (immediately belo | w) to dwelling unit to | otale in sectio | n 2 | |
| Population | | You do not need to e | | | | | | e HH sizes. |
| Jse Surrounding Area (Block Group) Demographics for On-Site Average HH Size? | No | If no project-specific | | | | | | |
| Ise Surrounding Area (Block Group) Demographics for On-Site Average Veh Own? | No | If no project-specific | information exists, o | can use block group | average veh owned | (see below) | | |
| urrounding Area (Block Group) Demographics | | | | | | | | |
| | | | | | | | | |
| | 1.75 | | See http:// | /factfinder2.census. | gov/ | | | |
| werage HH size near Site | | | | | | | | |
| | 1.00 | | See http:// | /factfinder2.census. | gov/ | | | |
| verage Vehicles Owned per Dwelling Unit near Site | | | | | 5 | | | |
| | | | | | | | | |
| Section 2 - Trip Generation | | | Trip Equation M | -44 | | | | |
| | | | TTP Equation W | ethoa | | | | |
| | | | | | | | | |
| | | | | | | AM Peak | PM Peak | |
| | Quantity | Units | Daily | AM Peak Hour | PM Peak Hour | Hour | Hour | Hour |
| lumber of Dwelling Units | | | | | | | | |
| Single Family Multi-Family | | | Log Equation | Linear Equation | Log Equation | 27 | 29 | Yes |
| | | | | | Linear Equation | 0 | | |
| | | | Linear Equation | Linear Equation | Linear Equation | 0 | 0 101 | Yes |
| Townhouse (du's adjusted to match mid-rise ITE apt trip estimate) High Rise Condo | 189 | DU | Linear Equation Log Equation Linear Equation | Linear Equation Log Equation Linear Equation | Linear Equation Log Equation Linear Equation | 0 86 0 | | Yes |
| Townhouse (du's adjusted to match mid-rise ITE apt trip estimate) | 189 | DU | Log Equation | Log Equation | Log Equation | 86 | 101 | |
| Townhouse (du's adjusted to match mid-rise ITE apt trip estimate) High Rise Condo | 189 | DU | Log Equation | Log Equation | Log Equation | 86 | 101 | |
| Townhouse (du's adjusted to match mid-rise ITE apt trip estimate) High Rise Condo etail (note: if you use job units for retail, the spreadsheet will convert before pplying trip rates, using the rate in section 2 which you can change) | 189 0 | DU DU | Log Equation Linear Equation | Log Equation Linear Equation | Log Equation Linear Equation | 86 0 | 101 0 | Yes |
| Townhouse (du's adjusted to match mid-rise ITE apt trip estimate) High Rise Condo etail (note: if you use job units for retail, the spreadsheet will convert before pplying trip rates, using the rate in section 2 which you can change) General Retail other than those listed below | 189 0 | DU DU ksf | Log Equation Linear Equation | Log Equation Linear Equation | Log Equation Linear Equation | 86 0 6 | 101 0 22 | Yes |
| Townhouse (du's adjusted to match mid-rise ITE apt trip estimate) High Rise Condo etail (note: if you use job units for retail, the spreadsheet will convert before pplying trip rates, using the rate in section 2 which you can change) General Retail other than those listed below Supermarket | 189 0 6 | DU DU ksf ksf | Log Equation Linear Equation Average Rate Average Rate | Log Equation Linear Equation Average Rate Average Rate | Log Equation Linear Equation Average Rate Average Rate | 86 0 6 0 | 101 0 22 0 | Yes Yes Yes |
| Townhouse (du's adjusted to match mid-rise ITE apt trip estimate) High Rise Condo etail (note: if you use job units for retail, the spreadsheet will convert before oplying trip rates, using the rate in section 2 which you can change) General Retail other than those listed below | 189 0 6 0 0 0 | DU DU ksf ksf | Log Equation Linear Equation | Log Equation Linear Equation | Log Equation Linear Equation | 86 0 6 | 101 0 22 | Yes |
| Townhouse (du's adjusted to match mid-rise ITE apt trip estimate) High Rise Condo etail (note: if you use job units for retail, the spreadsheet will convert before oplying trip rates, using the rate in section 2 which you can change) General Retail other than those listed below Supermarket Bank Health Club Restaurant (non-fast food) | 189 0 6 0 0 0 0 0 0 0 0 0 0 0 0 0 | DU DU ksf ksf ksf ksf ksf | Log Equation Linear Equation | Log Equation Linear Equation Average Rate Average Rate Average Rate Average Rate Average Rate | Log Equation Linear Equation | 86 0 0 0 0 0 | 101 0 22 0 0 0 0 0 | Yes Yes Yes Yes Yes Yes Yes |
| Townhouse (du's adjusted to match mid-rise ITE apt trip estimate) High Rise Condo etail (note: if you use job units for retail, the spreadsheet will convert before oplying trip rates, using the rate in section 2 which you can change) General Retail other than those listed below Supermarket Bank Health Club Restaurant (non-fast food) Fast-Food Restaurant | 189 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | DU DU ksf ksf ksf ksf ksf ksf | Log Equation Linear Equation | Log Equation Linear Equation Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate | Log Equation Linear Equation | 86 0 0 0 0 0 0 | 101 0 22 0 0 0 0 0 0 | Yes Yes Yes Yes Yes Yes Yes |
| Townhouse (du's adjusted to match mid-rise ITE apt trip estimate) High Rise Condo etail (note: if you use job units for retail, the spreadsheet will convert before pplying trip rates, using the rate in section 2 which you can change) General Retail other than those listed below Supermarket Bank Health Club Restaurant (non-fast food) Fast-Food Restaurant Gas Station | 189 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | DU DU ksf ksf ksf ksf ksf ksf ksf | Log Equation Linear Equation Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate | Log Equation Linear Equation Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate | Log Equation Linear Equation | 86 0 0 0 0 0 0 0 0 | 101 0 22 0 0 0 0 0 0 0 0 | Yes Yes Yes Yes Yes Yes Yes Yes Yes |
| Townhouse (du's adjusted to match mid-rise ITE apt trip estimate) High Rise Condo etail (note: if you use job units for retail, the spreadsheet will convert before oplying trip rates, using the rate in section 2 which you can change) General Retail other than those listed below Supermarket Bank Health Club Restaurant (non-fast food) Fast-Food Restaurant Gas Station Auto Repair | 189 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | DU DU ksf ksf ksf ksf ksf ksf ksf ksf ksf | Log Equation Linear Equation Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate | Log Equation Linear Equation | Log Equation Linear Equation | 86 0 0 0 0 0 0 0 0 0 0 0 0 0 | 101 0 22 0 0 0 0 0 0 0 0 0 0 | Yes Yes Yes Yes Yes Yes Yes Yes Yes |
| Townhouse (du's adjusted to match mid-rise ITE apt trip estimate) High Rise Condo etail (note: if you use job units for retail, the spreadsheet will convert before oplying trip rates, using the rate in section 2 which you can change) General Retail other than those listed below Supermarket Bank Health Club Restaurant (non-fast food) Fast-Food Restaurant Gas Station Auto Repai Home Improvement Superstore | 189 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | DU DU ksf ksf ksf ksf ksf ksf ksf ksf ksf ksf | Log Equation Linear Equation Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate | Log Equation Linear Equation Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate | Log Equation Linear Equation Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate | 86 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 101 0 22 0 0 0 0 0 0 0 0 0 0 0 0 | Yes Yes Yes Yes Yes Yes Yes Yes Yes Yes |
| Townhouse (du's adjusted to match mid-rise ITE apt trip estimate) High Rise Condo etail (note: if you use job units for retail, the spreadsheet will convert before pplying trip rates, using the rate in section 2 which you can change) General Retail other than those listed below Supermarket Bank Health Club Restaurant (non-fast food) Fast-Food Restaurant Gas Station Auto Repair Home Improvement Superstore Free-Standing Discount | 189 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | DU DU ksf ksf ksf ksf ksf ksf ksf ksf ksf ksf | Log Equation Linear Equation Average Rate Average Rate | Log Equation Linear Equation Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate | Log Equation Linear Equation Average Rate Average Rate | 86 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 101 0 22 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | Yes Yes Yes Yes Yes Yes Yes Yes Yes Yes |
| Townhouse (du's adjusted to match mid-rise ITE apt trip estimate) High Rise Condo etail (note: if you use job units for retail, the spreadsheet will convert before pplying trip rates, using the rate in section 2 which you can change) General Retail other than those listed below Supermarket Bank Health Club Restaurant (non-fast food) Fast-Food Restaurant Gas Station Auto Repai Home Improvement Superstore Free-Standing Discount | | DU DU ksf ksf ksf ksf ksf ksf ksf ksf ksf ksf | Log Equation Linear Equation | Log Equation Linear Equation | Log Equation Linear Equation | 86 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 101 0 22 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | Yes Yes Yes Yes Yes Yes Yes Yes Yes Yes |
| Townhouse (du's adjusted to match mid-rise ITE apt trip estimate) High Rise Condo Letail (note: if you use job units for retail, the spreadsheet will convert before pplying trip rates, using the rate in section 2 which you can change) General Retail other than those listed below Supermarket Bank Health Club Restaurant (non-fast food) Fast-Food Restaurant Gas Station Auto Repair Home Improvement Superstore Free-Standing Discount | | DU DU ksf ksf ksf ksf ksf ksf ksf ksf ksf ksf | Log Equation Linear Equation Average Rate Average Rate | Log Equation Linear Equation Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate | Log Equation Linear Equation Average Rate Average Rate | 86 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 101 0 22 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | Yes Yes Yes Yes Yes Yes Yes Yes Yes Yes |
| Townhouse (du's adjusted to match mid-rise ITE apt trip estimate) High Rise Condo etail (note: if you use job units for retail, the spreadsheet will convert before pplying trip rates, using the rate in section 2 which you can change) General Retail other than those listed below Supermarket Bank Health Club Restaurant (non-fast food) Fast-Food Restaurant Gas Station Auto Repair Home Improvement Superstore Free-Standing Discount ffice Non-Medical Medical | | DU DU DU ksf ksf ksf ksf ksf ksf ksf ksf ksf ksf | Log Equation Linear Equation Average Rate Average Rate | Log Equation Linear Equation Average Rate Average Rate | Log Equation Linear Equation | 86 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 101 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | Yes Yes Yes Yes Yes Yes Yes Yes Yes Yes |
| Townhouse (du's adjusted to match mid-rise ITE apt trip estimate) High Rise Condo stall (note: if you use job units for retail, the spreadsheet will convert before pplying trip rates, using the rate in section 2 which you can change) General Retail other than those listed below Supermarket Bank Health Club Restaurant (non-fast food) Fast-Food Restaurant Gas Station Auto Repai Home Improvement Superstore Free-Standing Discount ffice Non-Medical Medical dustrial | | DU DU DU ksf ksf ksf ksf ksf ksf ksf ksf ksf ksf | Log Equation Linear Equation Average Rate Average Rate | Log Equation Linear Equation Average Rate Average Rate | Log Equation Linear Equation | 86 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 101 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | Yes Yes Yes Yes Yes Yes Yes Yes Yes Yes |
| Townhouse (du's adjusted to match mid-rise ITE apt trip estimate) High Rise Condo atail (note: if you use job units for retail, the spreadsheet will convert before oplying trip rates, using the rate in section 2 which you can change) General Retail other than those listed below Supermarket Bank Health Club Restaurant (non-fast food) Fast-Food Restaurant Gas Station Auto Repair Home Improvement Superstore Free-Standing Discount ffice Non-Medical dustrial | | DU DU DU ksf ksf ksf ksf ksf ksf ksf ksf ksf ksf | Log Equation Linear Equation Average Rate Average Rate | Log Equation Linear Equation Average Rate Average Rate | Log Equation Linear Equation | 86 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 101 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | Yes Yes Yes Yes Yes Yes Yes Yes Yes Yes |
| Townhouse (du's adjusted to match mid-rise ITE apt trip estimate) High Rise Condo etail (note: if you use job units for retail, the spreadsheet will convert before pplying trip rates, using the rate in section 2 which you can change) General Retail other than those listed below Supermarket Bank Health Club Restaurant (non-fast food) Fast-Food Restaurant Gas Station Auto Repair Home Improvement Superstore Free-Standing Discount ffice Non-Medical Medical dustrial Light Industrial Warehousing / Self-Storage | | DU DU DU ksf ksf ksf ksf ksf ksf ksf ksf ksf ksf | Log Equation Linear Equation Average Rate Average Rate | Log Equation Linear Equation Average Rate Average Rate | Log Equation Linear Equation | 86 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 101 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | Yes Yes Yes Yes Yes Yes Yes Yes Yes Yes |
| Townhouse (du's adjusted to match mid-rise ITE apt trip estimate) High Rise Condo atali (note: if you use job units for retail, the spreadsheet will convert before oplying trip rates, using the rate in section 2 which you can change) General Retail other than those listed below Supermarket Bank Health Club Restaurant (non-fast food) Fast-Food Restaurant Gas Station Auto Repair Home Improvement Superstore Free-Standing Discount ffice Non-Medical Medical dustrial Light Industrial Light Industrial Superbound of Self-Storage | | DU DU DU ksf ksf ksf ksf ksf ksf ksf ksf ksf ksf | Log Equation Linear Equation | Log Equation Linear Equation | Log Equation Linear Equation | 86 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 101 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | Yes Yes Yes Yes Yes Yes Yes Yes Yes Yes |
| Townhouse (du's adjusted to match mid-rise ITE apt trip estimate) High Rise Condo stall (note: if you use job units for retail, the spreadsheet will convert before oplying trip rates, using the rate in section 2 which you can change) General Retail other than those listed below Supermarket Bank Health Club Restaurant (non-fast food) Fast-Food Restaurant Gas Station Auto Repain Home Improvement Superstore Free-Standing Discount ffice Non-Medical Medical dustrial Light Industrial Manufacturing bate (including restaurant, facilities, etc) otel ovie Theater (Theater with Matinee) | | DU DU SU ksf ksf ksf ksf ksf ksf ksf ksf ksf ksf | Log Equation Linear Equation Average Rate Average Rate | Log Equation Linear Equation | Log Equation Linear Equation Average Rate Average Rate | 86 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 101 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | Yes Yes Yes Yes Yes Yes Yes Yes Yes Yes |
| Townhouse (du's adjusted to match mid-rise ITE apt trip estimate) High Rise Condo stall (note: if you use job units for retail, the spreadsheet will convert before oplying trip rates, using the rate in section 2 which you can change) General Retail other than those listed below Supermarket Bank Health Club Restaurant (non-fast food) Fast-Food Restaurant Gas Station Auto Repair Home Improvement Superstore Free-Standing Discount ffice Non-Medical dustrial Light Industrial Light Industrial Manufacturing Warehousing / Self-Storage otel (including restaurant, facilities, etc) otel ovie Theater (Theater with Matinee) ovie Theater (Multiplex) | | DU DU SU ksf ksf ksf ksf ksf ksf ksf ksf ksf ksf | Log Equation Linear Equation | Log Equation Linear Equation | Log Equation Linear Equation | 86 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 101 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | Yes Yes Yes Yes Yes Yes Yes Yes Yes Yes |
| Townhouse (du's adjusted to match mid-rise ITE apt trip estimate) High Rise Condo stall (note: If you use job units for retail, the spreadsheet will convert before oplying trip rates, using the rate in section 2 which you can change) General Retail other than those listed below Supermarket Bank Health Club Restaurant (non-fast food) Fast-Food Restaurant Gas Station Auto Repain Home Improvement Superstore Free-Standing Discount ffice Non-Medical dustrial Light Industrial Manufacturing Warehousing / Self-Storage otel (including restaurant, facilities, etc) otel ovie Theater (Theater with Matinee) ovie Theater (Multiplex) | | DU DU DU ksf ksf ksf ksf ksf ksf ksf ksf ksf ksf | Log Equation Linear Equation Average Rate Average Rate | Log Equation Linear Equation Average Rate Average Rate | Log Equation Linear Equation Average Rate Average Rate | 86 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 101 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | Yes Yes Yes Yes Yes Yes Yes Yes Yes Yes |
| Townhouse (du's adjusted to match mid-rise ITE apt trip estimate) High Rise Condo etail (note: if you use job units for retail, the spreadsheet will convert before pplying trip rates, using the rate in section 2 which you can change) General Retail other than those listed below Supermarket Bank Health Club Restaurant (non-fast food) Fast-Food Restaurant Gas Station Auto Repair Home Improvement Superstore Free-Standing Discount ffice Non-Medical Medical dustrial Light Industrial Clight Industrial Clight Industrial State (including restaurant, facilities, etc) Iotel Iovie Theater (Theater with Matinee) Iovie Theater (Multiplex) chool | | DU DU DU ksf ksf ksf ksf ksf ksf ksf ksf ksf ksf | Log Equation Linear Equation | Log Equation Linear Equation Average Rate Average Rate | Log Equation Linear Equation Average Rate Average Rate | 86 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 101 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | Yes Yes Yes Yes Yes Yes Yes Yes Yes Yes |
| Townhouse (du's adjusted to match mid-rise ITE apt trip estimate) High Rise Condo stall (note: If you use job units for retail, the spreadsheet will convert before oplying trip rates, using the rate in section 2 which you can change) General Retail other than those listed below Supermarket Bank Health Club Restaurant (non-fast food) Fast-Food Restaurant Gas Station Auto Repain Home Improvement Superstore Free-Standing Discount ffice Non-Medical dustrial Light Industrial Manufacturing botel (including restaurant, facilities, etc) otel ovie Theater (Theater with Matinee) ovie Theater (Multiplex) chool | | DU DU DU ksf ksf ksf ksf ksf ksf ksf ksf ksf ksf | Log Equation Linear Equation Average Rate Average Rate | Log Equation Linear Equation Average Rate Average Rate | Log Equation Linear Equation Average Rate Average Rate | 86 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 101 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | Yes Yes Yes Yes Yes Yes Yes Yes Yes Yes |
| Townhouse (du's adjusted to match mid-rise ITE apt trip estimate) High Rise Condo setail (note: If you use job units for retail, the spreadsheet will convert before oplying trip rates, using the rate in section 2 which you can change) General Retail other than those listed below Supermarket Bank Health Club Restaurant (non-fast food) Fast-Food Restaurant Gas Station Auto Repain Home Improvement Superstore Free-Standing Discount ffice Non-Medical Medical dustrial Light Industrial Manufacturing Warehousing / Self-Storage otel (including restaurant, facilities, etc) otel ovie Theater (Theater with Matinee) ovie Theater (Multiplex) chool | | DU DU DU ksf ksf ksf ksf ksf ksf ksf ksf ksf ksf | Log Equation Linear Equation | Log Equation Linear Equation Average Rate Average Rate | Log Equation Linear Equation Average Rate Average Rate | 86 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 101 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | Yes Yes Yes Yes Yes Yes Yes Yes Yes Yes |
| Townhouse (du's adjusted to match mid-rise ITE apt trip estimate) High Rise Condo setail (note: If you use job units for retail, the spreadsheet will convert before oplying trip rates, using the rate in section 2 which you can change) General Retail other than those listed below Supermarket Bank Health Club Restaurant (non-fast food) Fast-Food Restaurant Gas Station Auto Repain Home Improvement Superstore Free-Standing Discount ffice Non-Medical dustrial Light Industrial Manufacturing Varehousing / Self-Storage otel (including restaurant, facilities, etc) otel ovie Theater (Theater with Matinee) ovie Theater (Multiplex) chool | | DU DU DU ksf ksf ksf ksf ksf ksf ksf ksf ksf ksf | Log Equation Linear Equation Average Rate Average Rate | Log Equation Linear Equation Average Rate Average Rate | Log Equation Linear Equation Average Rate Average Rate | 86 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 101 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | Yes Yes Yes Yes Yes Yes Yes Yes Yes Yes |
| Townhouse (du's adjusted to match mid-rise ITE apt trip estimate) High Rise Condo stall (note: If you use job units for retail, the spreadsheet will convert before oplying trip rates, using the rate in section 2 which you can change) General Retail other than those listed below Supermarket Bank Health Club Restaurant (non-fast food) Fast-Food Restaurant Gas Station Auto Repain Home Improvement Superstore Free-Standing Discount ffice Non-Medical dustrial Light Industrial Manufacturing Warehousing / Self-Storage otel (including restaurant, facilities, etc) otel ovie Theater (Multiplex) chool | | DU DU DU ksf ksf ksf ksf ksf ksf ksf ksf ksf ksf | Log Equation Linear Equation Average Rate Average Rate | Log Equation Linear Equation Average Rate Average Rate | Log Equation Linear Equation Average Rate Average Rate | 86 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | 101 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 | Yes Yes Yes Yes Yes Yes Yes Yes Yes Yes |

AM Peak PM Peak Daily Hour Hour 1,658 118 153

Total "Raw" ITE Trips

MIXED USE TRIP GENERATION MODEL - ADVANCED OUTPUT

MODEL APPLICATION - ALL TRIPS

| | Daily | | AM Peak Hour | | PM Peal | k Hour |
|--|--------|----------------------|--------------|--------|---------|---------------------|
| | HBW | HBO | HBW | HBO | HBW | HBO |
| Number of "Raw" ITE Trips Subject to Model | | | | | | |
| Productions | 316 | 847 | 52 | 50 | 41 | 69 |
| Attractions | 26 | 312 | 2 | 13 | 3 | 25 |
| Total | 342 | 1159 | 53 | 63 | 44 | 93 |
| Predicted Probabilities: | | | | | | |
| Productions | | | | | | |
| Internal Capture | 2.44% | 2.19% <mark>-</mark> | 9.69% | 5.95% | 10.55% | <mark>6.48%</mark> |
| Walking External | 1.90% | 18.01% | 2.51% | 23.77% | 1.90% | <mark>18.01%</mark> |
| Transit External | 7.82% | 3.18% <mark>-</mark> | 11.11% | 6.85% | 12.13% | 6.37% |
| Attractions | | | | | | |
| Internal Capture | 7.09% | 4.30% | 9.69% | 5.95% | 10.55% | <mark>6.48%</mark> |
| Walking External | 9.80% | 29.69% | 12.93% | 39.18% | 9.80% | 29.69% |
| Transit External | 26.75% | 8.45% <mark>-</mark> | 37.99% | 18.16% | 41.47% | <mark>16.89%</mark> |
| Total | | | | | | |
| Internal Capture | 7.02% | 4.31% | 6.07% | 6.35% | 9.16% | 6.44% |
| Walking External | 2.24% | 21.03% | 2.51% | 26.57% | 2.12% | 20.89% |
| Transit External | 8.63% | 4.54% | 11.11% | 8.90% | 12.94% | <mark>8.97%</mark> |
| Number of Trips: | | | | | | |
| Productions | | | | | | |
| Internal Capture | 12 | 25 | 2 | 2 | 2 | 3 |
| Walking External | 6 | 148 | 1 | 11 | 1 | 12 |
| Transit External | 24 | 26 | 6 | 3 | 5 | 4 |
| Attractions | | | | | | |
| Internal Capture | 12 | 25 | 2 | 2 | 2 | 3 |
| Walking External | 1 | 85 | 0 | 4 | 0 | 6 |
| Transit External | 4 | 24 | 0 | 2 | 0 | 4 |
| Total | | | | | | |
| Internal Capture | 24 | 50 | 3 | 4 | 4 | 6 |
| Walking External | 7 | 233 | 1 | 16 | 1 | 18 |
| Transit External | 27 | 50 | 6 | 5 | 5 | 8 |

MIXED USE TRIP GENERATION MODEL - BASIC INPUT

All shaded cells are inputs Regular inputs (project-specific) Inputs that may depend on regional values from census data, travel demand model, etc...

Section 1 - General Site Information

| Site Name | Stockton B | Ivd./T Street Office | int/sq mi | 640 | |
|--|---|---|---|--|--|
| Coorresphie | | Natao / Instructions | | | |
| Geographic | | Notes / Instructions | | et norke De not in | |
| Developed Area (in acres) | | Include streets, ROV | | | |
| Number of Intersections | Yes | Count intersections e | auner within or on th | le perimeter of the M | AD. Check resulting |
| Is Transit (bus or rail) present within the site or across the street? | | Entor on a normantar | • | | |
| Proportion of households within 1/4 mile of a transit stop | 100% | Enter as a percentag | e | | |
| Land Use - Surrounding Area | | | | | |
| | | those found in smalle | | | |
| Is the site in a Central Business District and/or TOD? | No | be the primary factor | | | |
| Employment within one mile of the MXD | | Do not include emplo | | | |
| Employment within a 30 minute Transit Trip (Door-to-door) | | Per Sacmet Model. | | | |
| Total Regional Employment | 966,900 | Employment at MPO | or similar level | | If in the 9 county Ba |
| | | | | | |
| Site Demographics Enter Population Directly? | No | If "No" will opply ovo | rago UU aizo fosta | a (immodiataly bala | w) to dwelling unit tot |
| Population Directly? | No | | | | ed based on dwelling |
| Use Surrounding Area (Block Group) Demographics for On-Site Average HH Size? | No | If no project-specific | | | |
| Use Surrounding Area (Block Group) Demographics for On-Site Average Veh Own? | No | If no project-specific | | | |
| | | | | <u>-</u> | g |
| Surrounding Area (Block Group) Demographics | | | | | |
| | | | | | |
| | 1.75 | | See http://factfine | der2.census.gov/ | |
| Average HH size near Site | | | | | |
| | | | | | |
| | 1.00 | | See http://factfine | der2 census aov/ | |
| Augusta Mahisha Oranada a Duglika Haita a 2014 | 1.00 | | Oce mp.//actim | derz.census.gov/ | |
| Average Vehicles Owned per Dwelling Unit near Site | | | | | |
| Continu D. Trin Constantion | | | | | |
| Section 2 - Trip Generation | | | | | |
| | | | Trip Equation M | ethod | |
| | | | | | |
| | | | | | |
| | | | | | |
| | Quantity | Units | Daily | AM Peak Hour | PM Peak Hour |
| | , | | , | | |
| Number of Dwelling Units | | | | | |
| Single Family | y C | DU | Log Equation | Linear Equation | Log Equation |
| Multi-Family | y C | DU | Linear Equation | Linear Equation | Linear Equation |
| Townhouse (du's adjusted to match mid-rise ITE apt trip estimate |) (| DU | Log Equation | Log Equation | Log Equation |
| High Rise Condo | o <mark> (</mark> | DU | Linear Equation | Linear Equation | Linear Equation |
| | | | | | |
| Parts 11 for stars 16 merets 1 and 16 merets 11 stars and a large star 110 merets at the form | | | | | |
| Retail (note: if you use job units for retail, the spreadsheet will convert before | | | | | |
| applying trip rates, using the rate in section 2 which you can change) | | kof | Average Deta | Average Date | Average Date |
| General Retail other than those listed belov Supermarke | | | Average Rate Average Rate | Average Rate Average Rate | Average Rate Average Rate |
| Bani | | | Average Rate | Average Rate | Average Rate |
| Health Club | | | Average Rate | Average Rate | Average Rate |
| Restaurant (non-fast food | | | Average Rate | Average Rate | Average Rate |
| Fast-Food Restauran | | | Average Rate | Average Rate | Average Rate |
| Gas Station | | | Average Rate | Average Rate | Average Rate |
| Auto Repai | | | Average Rate | Average Rate | Average Rate |
| Home Improvement Superstore | | ksf | Average Rate | Average Rate | Average Rate |
| Free-Standing Discoun | | ksf | Average Rate | Average Rate | Average Rate |
| Office | | | _ | | _ |
| Non-Medica | | | Log Equation | Log Equation | Linear Equation |
| Medica | l <mark> C</mark> | ksf | Average Rate | Average Rate | Average Rate |
| Industrial | | 1 | A | A | A |
| Light Industria | | | Average Rate | Average Rate | Average Rate |
| | | ksf | Average Rate | Average Rate Average Rate | Average Rate Average Rate |
| Manufacturing Warehousing / Solf Storage | | kef | | | |
| Manufacturing Warehousing / Self-Storage | | ksf | Average Rate | /weitige Hate | Average Nate |
| Warehousing / Self-Storage | e (| | | _ | 5 |
| Warehousing / Self-Storage | | | - Average Rate | - Average Rate | Average Rate |
| Warehousing / Self-Storage Hotel (including restaurant, facilities, etc) Motel | e (| Rooms | Average Rate Average Rate | Average Rate Average Rate | Average Rate Average Rate |
| Warehousing / Self-Storage | e (| Rooms Rooms | - Average Rate | - Average Rate | Average Rate |
| Warehousing / Self-Storage Hotel (including restaurant, facilities, etc) Motel Movie Theater (Theater with Matinee) | é (| Rooms Rooms | Average Rate Average Rate Average Rate Average Rate | Average Rate Average Rate Average Rate | Average Rate Average Rate Average Rate Average Rate |
| Warehousing / Self-Storage Hotel (including restaurant, facilities, etc) Motel Movie Theater (Theater with Matinee) Movie Theater (Multiplex) | | Rooms Rooms Screens Students | Average Rate Average Rate Average Rate Average Rate | Average Rate Average Rate Average Rate Average Rate Average Rate | Average Rate Average Rate Average Rate Average Rate Average Rate |
| Warehousing / Self-Storage Hotel (including restaurant, facilities, etc) Motel Movie Theater (Theater with Matinee) Movie Theater (Multiplex) School University High Schoo | 5 (((((() () () () () () () () () () | Rooms Rooms Screens Students Students | Average Rate Average Rate Average Rate Average Rate Average Rate | Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate | Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate |
| Warehousing / Self-Storage Hotel (including restaurant, facilities, etc) Motel Movie Theater (Theater with Matinee) Movie Theater (Multiplex) School Universit High Schoo Middle Schoo | | Rooms Rooms Screens Students Students Students | Average Rate Average Rate Average Rate Average Rate Linear Equation Average Rate Average Rate | Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate | Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate |
| Warehousing / Self-Storage Hotel (including restaurant, facilities, etc) Motel Movie Theater (Theater with Matinee) Movie Theater (Multiplex) School University High Schoo | | Rooms Rooms Screens Students Students Students | Average Rate Average Rate Average Rate Average Rate Average Rate | Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate | Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate Average Rate |

| Trips from Land uses not covered above ==> | |
|--|--|
|--|--|

Daily AM Peak Hour PM Peak Hour

AM Peak PM Peak
 Hour
 Hour

 1,508
 221
 213
 Daily

0

Total "Raw" ITE Trips

Jobs in those Land Uses

MIXED USE TRIP GENERATION MODEL - ADVANCED OUTPUT

MODEL APPLICATION - ALL TRIPS

| | Dai | Daily | | AM Peak Hour | | Hour |
|--|--------------|--------|--------|--------------|--------|--------|
| | HBW | HBO | HBW | HBO | HBW | HBO |
| Number of "Raw" ITE Trips Subject to Model | | | | | | |
| Productions | | 0 | 0 | 0 | 0 | 0 |
| Attractions | | 589 | 146 | 62 | 89 | 66 |
| Tota | i 503 | 589 | 146 | 62 | 89 | 66 |
| Predicted Probabilities: | | | | | | |
| Production | | | | | | |
| Internal Captur | | | | | | |
| Walking Externa | | | | | | |
| Transit Externa | al | | | | | |
| Attraction | S | | | | | |
| Internal Captur | e 2.34% | 1.35% | | | | |
| Walking Externa | al 5.25% | 15.72% | | | | |
| Transit Externa | al 26.75% | 7.40% | | | | |
| Tota | | | | | | |
| Internal Captur | | 0.00% | 0.00% | 0.00% | 0.00% | 0.00% |
| Walking Externa | | 15.72% | 6.93% | 20.75% | 5.25% | 15.72% |
| Transit Externa | | 7.40% | 37.99% | 15.91% | 41.47% | 14.80% |
| | | | | | | |
| Number of Trips: | _ | | | | | |
| Productions | | 0 | 0 | 0 | 0 | 0 |
| Internal Captur | | 0 | 0 | 0 | 0 | 0 |
| Walking Externa | | 0 0 | 0 | 0 0 | 0 | 0 |
| Transit Externa | al O | 0 | 0 | 0 | 0 | 0 |
| Attractions | s | | | | | |
| Internal Captur | e 0 | 0 | 0 | 0 | 0 | 0 |
| Walking Externa | | 93 | 10 | 13 | 5 | 10 |
| Transit Externa | al 134 | 44 | 55 | 10 | 37 | 10 |
| Tota | d. | | | | | |
| Internal Captur | | 0 | 0 | 0 | 0 | 0 |
| Walking Externa | | 93 | 10 | 13 | 5 | 10 |
| Transit Externa | | 44 | 55 | 10 | 37 | 10 |
| | | | | | | |

APPENDIX C: EXISTING PLUS PROJECT INTERSECTION CONDITIONS



SimTraffic Post-Processor Average Data from 10 Runs Intersection Volume and Delay

| | | | Demand | | Sen | ved Volume | (vph) | | | | | | |
|------|---------------------------------|------------------|--------|---------|---------|------------|---------|---------|---------|-----------|----------------|-------|-----|
| | | | Volume | | Percent | Standard | (•p/ | | | Tota | al Delay (sec/ | (veh) | |
| | Intersection | Control | (vph) | Average | Served | Deviation | Minimum | Maximum | Average | Std. Dev. | | | LOS |
| 1 | Stockton/35th-WB HWY 50 ramps | Signal | 2,413 | 2,458 | 101.9% | 107 | 2,284 | 2,652 | 22.5 | 4.8 | 16.1 | 33.3 | С |
| 2 | Stockton/none-EB HWY 50 on ramp | Uncontrolled | 1,987 | 2,038 | 102.6% | 107 | 1,844 | 2,180 | 11.8 | 2.2 | 8.0 | 15.0 | В |
| 4 | 37th/T St | Side-street Stop | 530 | 524 | 98.8% | 31 | 460 | 564 | 5.5 | 2.7 | 0.0 | 9.0 | А |
| 5 | 39th/T St | Signal | 856 | 837 | 97.8% | 67 | 772 | 964 | 14.4 | 1.2 | 12.8 | 16.6 | В |
| 6 | 39th/S St | Side-street Stop | 473 | 458 | 96.7% | 31 | 424 | 520 | 5.9 | 3.0 | 0.0 | 10.4 | А |
| | | | | | | | | | | | | | |
| 3 | Stockton/T St | Signal | 2,593 | 2,587 | 99.8% | 115 | 2,356 | 2,740 | 29.3 | 7.5 | 20.8 | 41.5 | С |
| | Network Summary | | | | | | | | | | | | |
| Tota | al Demand Volume (veh/hr) | 8,852 | | | | | | | | | | | |
| Tota | al Volume Served (veh/hr) | 8,901 | | | | | | | | | | | |
| Per | cent Served | 100.6% | | | | | | | | | | | |
| GEH | l Statistic | 0.5 | | | | | | | | | | | |
| | | | | | | | | | | | | | |

Stockton & T E+P AM Peak Hour

Intersection 1

Stockton/35th-WB HWY 50 ramps

Signal

| | | Demand | Served Vo | lume (vph) | Total | Delay (sec/ve | h) |
|-----------|------------|--------------|-----------|------------|---------|---------------|-----|
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS |
| | Left Turn | 6 | 3 | 46.7% | 16.8 | 24.6 | В |
| NB | Through | 453 | 448 | 98.9% | 15.1 | 2.2 | В |
| NB | Right Turn | 427 | 432 | 101.2% | 7.8 | 2.1 | Α |
| | Subtotal | 886 | 883 | 99.6% | 11.6 | 1.7 | В |
| | Left Turn | 42 | 41 | 98.1% | 30.2 | 7.8 | С |
| SB | Through | 381 | 398 | 104.4% | 14.4 | 1.3 | В |
| 50 | Right Turn | 2 | 3 | 140.0% | 2.2 | 2.5 | Α |
| | Subtotal | 425 | 442 | 103.9% | 15.8 | 1.2 | В |
| | Left Turn | 10 | 10 | 104.0% | 37.3 | 13.3 | D |
| EB | Through | 58 | 66 | 113.1% | 32.7 | 10.4 | С |
| ED | Right Turn | 72 | 79 | 109.4% | 17.1 | 7.9 | В |
| | Subtotal | 140 | 155 | 110.6% | 25.2 | 8.9 | С |
| | Left Turn | 317 | 330 | 104.0% | 53.1 | 20.8 | D |
| WB | Through | 73 | 68 | 92.6% | 56.2 | 19.1 | E |
| VVD | Right Turn | 572 | 582 | 101.7% | 21.6 | 6.9 | С |
| | Subtotal | 962 | 979 | 101.7% | 34.8 | 12.0 | С |
| | Total | 2,413 | 2,458 | 101.9% | 22.5 | 4.8 | С |

Intersection 2

Stockton/none-EB HWY 50 on ramp

Uncontrolled

| | | Demand | Served Vo | lume (vph) | Total Delay (sec/veh) | | |
|-----------|------------|--------------|-----------|------------|-----------------------|-----------|-----|
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS |
| | Left Turn | | | | | | |
| NB | Through | 886 | 895 | 101.0% | 1.1 | 0.1 | А |
| IND | Right Turn | 329 | 331 | 100.5% | 1.0 | 0.0 | А |
| | Subtotal | 1,215 | 1,226 | 100.9% | 1.1 | 0.1 | А |
| | Left Turn | 202 | 197 | 97.6% | 11.8 | 2.2 | В |
| SB | Through | 570 | 616 | 108.0% | 1.0 | 0.1 | А |
| 30 | Right Turn | | | | | | |
| | Subtotal | 772 | 813 | 105.3% | 3.6 | 0.6 | А |
| | Left Turn | | | | | | |
| EB | Through | | | | | | |
| LD | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| | Left Turn | | | | | | |
| WB | Through | | | | | | |
| VVB | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| | Total | 1,987 | 2,038 | 102.6% | 2.1 | 0.2 | А |

Stockton & T E+P AM Peak Hour

Intersection 4

37th/T St

Side-street Stop

| | I | Demand | Served Vo | lume (vph) | Total | Delay (sec/ve | h) |
|-----------|------------|--------------|-----------|------------|---------|---------------|-----|
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS |
| | Left Turn | | | | | | |
| NB | Through | | | | | | |
| ND | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| | Left Turn | 12 | 11 | 90.0% | 5.5 | 2.7 | А |
| SB | Through | | | | | | |
| 50 | Right Turn | 51 | 45 | 87.8% | 2.9 | 0.4 | А |
| | Subtotal | 63 | 56 | 88.3% | 3.5 | 0.8 | А |
| | Left Turn | 29 | 29 | 99.3% | 4.5 | 1.2 | А |
| EB | Through | 253 | 256 | 101.2% | 2.6 | 0.4 | А |
| LD | Right Turn | | | | | | |
| | Subtotal | 282 | 285 | 101.0% | 2.8 | 0.5 | А |
| | Left Turn | | | | | | |
| WB | Through | 182 | 180 | 98.7% | 1.2 | 0.2 | А |
| VV B | Right Turn | 3 | 4 | 120.0% | 0.5 | 0.6 | А |
| | Subtotal | 185 | 183 | 99.0% | 1.2 | 0.2 | А |
| | Total | 530 | 524 | 98.8% | 2.3 | 0.3 | А |

Intersection 5

39th/T St

| | | Demand | Served Vo | lume (vph) | Total | Delay (sec/vel | h) |
|-----------|------------|--------------|-----------|------------|---------|----------------|-----|
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS |
| | Left Turn | 6 | 6 | 93.3% | 18.0 | 16.6 | В |
| NB | Through | 131 | 117 | 89.5% | 12.4 | 3.0 | В |
| IND | Right Turn | 11 | 9 | 83.6% | 4.2 | 4.9 | А |
| | Subtotal | 148 | 132 | 89.2% | 12.2 | 3.0 | В |
| | Left Turn | 32 | 34 | 106.3% | 29.7 | 4.5 | С |
| SB | Through | 162 | 156 | 96.0% | 27.6 | 2.6 | С |
| 30 | Right Turn | 50 | 48 | 96.0% | 19.9 | 4.6 | В |
| | Subtotal | 244 | 238 | 97.4% | 26.4 | 2.3 | С |
| | Left Turn | 19 | 18 | 96.8% | 14.3 | 6.2 | В |
| EB | Through | 183 | 188 | 102.5% | 9.8 | 2.6 | А |
| LD | Right Turn | 63 | 61 | 96.5% | 6.2 | 2.6 | А |
| | Subtotal | 265 | 267 | 100.7% | 9.2 | 2.0 | А |
| | Left Turn | 11 | 12 | 105.5% | 15.6 | 9.2 | В |
| WB | Through | 129 | 124 | 95.8% | 9.4 | 1.5 | А |
| WB | Right Turn | 59 | 65 | 110.5% | 4.2 | 2.5 | А |
| | Subtotal | 199 | 200 | 100.7% | 8.2 | 1.8 | А |
| | Total | 856 | 837 | 97.8% | 14.4 | 1.2 | В |

Stockton & T E+P AM Peak Hour

Intersection 6

39th/S St

| | | Demand | Served Vo | lume (vph) | Total | Total Delay (sec/veh) | | |
|-----------|------------|--------------|-----------|---|---------|-----------------------|-----|--|
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS | |
| | Left Turn | 2 | 1 | 40.0% | 0.5 | 1.2 | А | |
| NB | Through | 207 | 201 | 97.0% | 1.0 | 0.2 | А | |
| IND | Right Turn | | | | | | | |
| | Subtotal | 209 | 202 | 96.5% | 1.0 | 0.2 | А | |
| | Left Turn | | | | | | | |
| SB | Through | 236 | 222 | 93.9% | 0.3 | 0.1 | А | |
| 30 | Right Turn | 6 | 8 | 140.0% | 0.1 | 0.2 | А | |
| | Subtotal | 242 | 230 | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | А | | | |
| | Left Turn | 10 | 8 | 84.0% | 5.9 | 3.0 | А | |
| EB | Through | | | | | | | |
| LD | Right Turn | 8 | 12 | 155.0% | 4.0 | 1.1 | А | |
| | Subtotal | 18 | 21 | 115.6% | 5.0 | 1.4 | А | |
| | Left Turn | | | | | | | |
| WB | Through | 3 | 2 | 80.0% | 3.2 | 3.5 | А | |
| VVD | Right Turn | 1 | 3 | 280.0% | 2.3 | 2.8 | А | |
| | Subtotal | 4 | 5 | 130.0% | 4.7 | 2.8 | А | |
| | Total | 473 | 458 | 96.7% | 0.9 | 0.2 | А | |

Intersection 0

Side-street Stop

| | [| Demand | Served Vo | lume (vph) | Total | Delay (sec/ve | n) |
|-----------|------------|--------------|-----------|------------|---------|---------------|-----|
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS |
| | Left Turn | | | | | | |
| NB | Through | | | | | | |
| ND | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| | Left Turn | | | | | | |
| SB | Through | | | | | | |
| 30 | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| | Left Turn | | | | | | |
| EB | Through | | | | | | |
| LD | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| | Left Turn | | | | | | |
| WB | Through | | | | | | |
| VVD | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| | Total | | | | | | |

Intersection 3

Stockton/T St

| | | Demand | Served Vo | lume (vph) | Total | Delay (sec/ve | h) |
|-----------|------------|--------------|-----------|------------|---------|---------------|-----|
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS |
| | Left Turn | 48 | 45 | 94.2% | 41.6 | 12.3 | D |
| NB | Through | 911 | 908 | 99.7% | 19.5 | 2.4 | В |
| IND | Right Turn | 23 | 24 | 102.6% | 20.4 | 5.6 | С |
| | Subtotal | 982 | 977 | 99.5% | 20.6 | 2.5 | С |
| | Left Turn | 29 | 28 | 95.2% | 35.6 | 14.3 | D |
| SB | Through | 518 | 567 | 109.5% | 12.3 | 1.4 | В |
| 30 | Right Turn | 23 | 21 | 92.2% | 9.1 | 3.9 | А |
| | Subtotal | 570 | 616 | 108.1% | 13.4 | 1.1 | В |
| | Left Turn | 109 | 113 | 103.5% | 47.8 | 22.6 | D |
| EB | Through | 228 | 232 | 101.8% | 48.0 | 19.6 | D |
| LD | Right Turn | 443 | 395 | 89.2% | 61.3 | 29.5 | Е |
| | Subtotal | 780 | 740 | 94.9% | 55.2 | 24.8 | Е |
| | Left Turn | 25 | 29 | 115.2% | 37.2 | 6.8 | D |
| NE | Through | | | | | | |
| INE | Right Turn | 3 | 4 | 133.3% | 42.8 | 32.2 | D |
| | Subtotal | 28 | 33 | 117.1% | 38.3 | 7.3 | D |
| | Left Turn | 14 | 11 | 77.1% | 33.5 | 11.8 | С |
| WB | Through | 56 | 51 | 90.7% | 22.2 | 8.7 | С |
| VVD | Right Turn | 163 | 160 | 97.9% | 22.6 | 3.1 | С |
| | Subtotal | 233 | 221 | 94.9% | 22.9 | 3.4 | С |
| | Total | 2,593 | 2,587 | 99.8% | 47.2 | 12.4 | D |

Signal

E+P

Stockton & T

AM Peak Hour

SimTraffic Post-Processor Average Data from 10 Runs Intersection Volume and Delay

| Stockton & T |
|--------------|
| E+P |
| PM Peak Hour |

| | | | Demand Volume | | Serv Percent | ved Volume (Standard | vph) | | | Tota | l Delay (sec/ | veh) | |
|------|-------------------------------|------------------|------------------|---------|-----------------|--------------------------|---------|---------|---------|------|---------------|-------|-----|
| | Intersection | Control | (vph) | Average | Served | Deviation | Minimum | Maximum | Average | | Minimum | | LOS |
| 1 | Stockton/35th-WB HWY 50 ramps | Signal | 2,847 | 2,632 | 92.5% | 94 | 2,496 | 2,803 | 42.2 | 7.7 | 35.5 | 61.3 | D |
| 2 | Stockton/EB HWY 50 on ramp | Uncontrolled | 2,427 | 2,152 | 88.7% | 92 | 1,989 | 2,269 | 61.5 | 28.5 | 24.1 | 111.9 | F |
| 4 | 38th/T St | Side-street Stop | 740 | 699 | 94.5% | 58 | 595 | 799 | 21.6 | 34.1 | 2.2 | 113.1 | С |
| 5 | 39th/T St | Signal | 1,128 | 1,053 | 93.3% | 68 | 968 | 1,167 | 14.8 | 1.8 | 11.0 | 17.4 | В |
| 6 | 39th/S St | Side-street Stop | 563 | 519 | 92.2% | 57 | 422 | 599 | 7.6 | 2.6 | 4.2 | 13.9 | Α |
| | | | | | | | | | | | | | |
| 3 | Stockton/T | Signal | 2,855 | 2,536 | 88.8% | 149 | 2,323 | 2,730 | 71.2 | 18.1 | 42.1 | 103.9 | E |
| | Network Summary | | | | | | | | | | | | |
| Tota | al Demand Volume (veh/hr) | 10,560 | | | | | | | | | | | |
| Tota | al Volume Served (veh/hr) | 9,592 | | | | | | | | | | | |
| Perc | cent Served | 90.8% | | | | | | | | | | | |
| GEH | l Statistic | 9.6 | | | | | | | | | | | |

Stockton & T E+P PM Peak Hour

Intersection 1

Stockton/35th-WB HWY 50 ramps

Signal

| | | Demand | Served Vo | lume (vph) | Total | Total Delay (sec/veh) | | |
|-----------|------------|--------------|-----------|------------|---------|-----------------------|-----|--|
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS | |
| | Left Turn | 14 | 8 | 60.3% | 38.1 | 21.5 | D | |
| NB | Through | 499 | 440 | 88.1% | 18.9 | 3.6 | В | |
| IND | Right Turn | 630 | 505 | 80.2% | 102.8 | 11.3 | F | |
| | Subtotal | 1,143 | 953 | 83.4% | 64.0 | 6.9 | Е | |
| | Left Turn | 73 | 71 | 97.8% | 54.7 | 28.1 | D | |
| SB | Through | 631 | 624 | 98.8% | 29.4 | 14.7 | С | |
| 30 | Right Turn | 8 | 10 | 124.8% | 10.1 | 10.8 | В | |
| | Subtotal | 712 | 705 | 99.0% | 31.8 | 16.1 | С | |
| | Left Turn | 16 | 11 | 67.2% | 44.5 | 32.0 | D | |
| EB | Through | 49 | 47 | 95.6% | 63.4 | 34.9 | Е | |
| ED | Right Turn | 30 | 27 | 90.9% | 41.1 | 53.3 | D | |
| | Subtotal | 95 | 85 | 89.3% | 53.2 | 38.7 | D | |
| | Left Turn | 194 | 197 | 101.7% | 34.9 | 6.4 | С | |
| WB | Through | 133 | 118 | 88.9% | 38.9 | 8.0 | D | |
| WB | Right Turn | 570 | 574 | 100.6% | 18.7 | 5.3 | В | |
| | Subtotal | 897 | 889 | 99.1% | 25.2 | 4.6 | С | |
| | Total | 2,847 | 2,632 | 92.5% | 42.2 | 7.7 | D | |

Intersection 2

Stockton/EB HWY 50 on ramp

Uncontrolled

| | | Demand | Served Vo | lume (vph) | Total | Delay (sec/ve | h) |
|-----------|------------|--------------|-----------|------------|---------|---------------|-----|
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS |
| | Left Turn | | | | | | |
| NB | Through | 1,143 | 953 | 83.4% | 11.3 | 3.2 | В |
| IND | Right Turn | 421 | 355 | 84.3% | 9.8 | 3.0 | А |
| | Subtotal | 1,564 | 1,308 | 83.7% | 10.9 | 3.2 | В |
| | Left Turn | 376 | 355 | 94.5% | 61.5 | 28.5 | F |
| SB | Through | 487 | 489 | 100.4% | 1.9 | 1.4 | А |
| 30 | Right Turn | | | | | | |
| | Subtotal | 863 | 844 | 97.8% | 26.8 | 11.4 | D |
| | Left Turn | | | | | | |
| EB | Through | | | | | | |
| LD | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| | Left Turn | | | | | | |
| WB | Through | | | | | | |
| VVB | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| | Total | 2,427 | 2,152 | 88.7% | 17.0 | 4.4 | С |

Stockton & T E+P PM Peak Hour

Intersection 4

38th/T St

Side-street Stop

| | I | Demand | Served Vo | lume (vph) | Total | Delay (sec/vel | h) |
|-----------|------------|--------------|-----------|------------|---------|----------------|-----|
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS |
| | Left Turn | | | | | | i |
| NB | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| | Left Turn | 3 | 2 | 64.0% | 7.7 | 12.2 | Α |
| SB | Through | | | | | | |
| 30 | Right Turn | 24 | 26 | 107.2% | 21.6 | 34.1 | С |
| | Subtotal | 27 | 28 | 102.4% | 22.0 | 33.7 | С |
| | Left Turn | 60 | 53 | 88.3% | 8.8 | 3.9 | Α |
| EB | Through | 327 | 297 | 90.8% | 3.9 | 0.5 | А |
| LD | Right Turn | | | | | | |
| | Subtotal | 387 | 350 | 90.4% | 4.7 | 0.9 | А |
| | Left Turn | | | | | | |
| WB | Through | 321 | 315 | 98.2% | 11.7 | 20.8 | В |
| WB | Right Turn | 5 | 7 | 130.6% | 2.6 | 5.3 | А |
| | Subtotal | 326 | 322 | 98.7% | 11.6 | 20.6 | В |
| | Total | 740 | 699 | 94.5% | 8.7 | 11.2 | А |

Intersection 5

39th/T St

| | I | Demand | Served Vo | lume (vph) | Total | Delay (sec/ve | h) |
|-----------|------------|--------------|-----------|------------|---------|---------------|-----|
| Direction | Movement | Volume (vph) | | Percent | Average | Std. Dev. | LOS |
| | Left Turn | 15 | 14 | 92.2% | 18.1 | 10.6 | В |
| NB | Through | 171 | 159 | 92.7% | 14.2 | 2.1 | В |
| IND | Right Turn | 33 | 33 | 98.9% | 8.6 | 3.2 | А |
| | Subtotal | 219 | 205 | 93.6% | 13.7 | 2.3 | В |
| | Left Turn | 40 | 40 | 100.8% | 35.1 | 8.2 | D |
| SB | Through | 153 | 142 | 92.9% | 28.2 | 4.2 | С |
| 30 | Right Turn | 60 | 60 | 99.2% | 22.7 | 4.7 | С |
| | Subtotal | 253 | 242 | 95.6% | 27.9 | 4.4 | С |
| | Left Turn | 48 | 36 | 76.0% | 15.9 | 2.8 | В |
| EB | Through | 260 | 243 | 93.6% | 10.5 | 2.2 | В |
| LD | Right Turn | 22 | 20 | 89.0% | 8.2 | 5.0 | А |
| | Subtotal | 330 | 300 | 90.8% | 11.1 | 2.1 | В |
| | Left Turn | 11 | 10 | 87.3% | 9.4 | 7.0 | А |
| WB | Through | 251 | 232 | 92.4% | 9.1 | 1.4 | А |
| WB | Right Turn | 64 | 65 | 101.4% | 5.5 | 2.1 | А |
| | Subtotal | 326 | 306 | 94.0% | 8.4 | 1.3 | А |
| | Total | 1,128 | 1,053 | 93.3% | 14.8 | 1.8 | В |

Stockton & T E+P PM Peak Hour

Intersection 6

39th/S St

| | | Demand | Served Vo | lume (vph) | Total | Delay (sec/vel | h) |
|-----------|------------|--------------|-----------|------------|---------|----------------|-----|
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS |
| | Left Turn | 3 | 3 | 102.4% | 2.2 | 2.3 | А |
| NB | Through | 278 | 257 | 92.3% | 1.1 | 0.1 | А |
| IND | Right Turn | 2 | 1 | 38.4% | 0.1 | 0.4 | А |
| | Subtotal | 283 | 260 | 92.0% | 1.1 | 0.1 | А |
| | Left Turn | 1 | 0 | 38.4% | 0.2 | 0.6 | Α |
| SB | Through | 245 | 229 | 93.4% | 0.3 | 0.2 | А |
| 30 | Right Turn | 12 | 10 | 86.4% | 0.1 | 0.1 | А |
| | Subtotal | 258 | 240 | 92.9% | 0.3 | 0.2 | А |
| | Left Turn | 14 | 10 | 71.3% | 7.6 | 2.6 | А |
| EB | Through | | | | | | |
| EB | Right Turn | 8 | 9 | 115.2% | 5.2 | 2.6 | А |
| | Subtotal | 22 | 19 | 87.3% | 6.5 | 1.5 | А |
| | Left Turn | | | | | | |
| WB | Through | | | | | | |
| VVD | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| | Total | 563 | 519 | 92.2% | 1.0 | 0.1 | А |

Intersection 0

Side-street Stop

| | I | Demand | Served Vo | lume (vph) | Total | Delay (sec/vel | h) |
|-----------|------------|--------------|-----------|------------|---------|----------------|-----|
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS |
| | Left Turn | | | | | | |
| NB | Through | | | | | | |
| NB | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| | Left Turn | | | | | | |
| SB | Through | | | | | | |
| 50 | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| | Left Turn | | | | | | |
| EB | Through | | | | | | |
| LD | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| | Left Turn | | | | | | |
| WB | Through | | | | | | |
| VVD | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| | Total | | | | | | |

Intersection 3

Stockton/T

| | | Demand | Served Vo | lume (vph) | Total | Delay (sec/ve | h) |
|-----------|------------|--------------|-----------|------------|---------|---------------|-----|
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS |
| | Left Turn | 62 | 51 | 83.0% | 96.8 | 26.8 | F |
| NB | Through | 1,195 | 984 | 82.4% | 95.2 | 29.4 | F |
| IND | Right Turn | 11 | 8 | 73.3% | 102.7 | 45.8 | F |
| | Subtotal | 1,268 | 1,044 | 82.3% | 95.3 | 29.0 | F |
| | Left Turn | 53 | 44 | 82.6% | 212.6 | 139.0 | F |
| SB | Through | 401 | 396 | 98.6% | 12.9 | 2.0 | В |
| 30 | Right Turn | 33 | 37 | 112.9% | 10.7 | 4.0 | В |
| | Subtotal | 487 | 477 | 97.9% | 31.5 | 12.6 | С |
| | Left Turn | 125 | 118 | 94.3% | 101.1 | 45.9 | F |
| EB | Through | 322 | 296 | 91.9% | 74.2 | 28.5 | E |
| LD | Right Turn | 282 | 248 | 88.0% | 65.8 | 24.1 | Е |
| | Subtotal | 729 | 662 | 90.8% | 75.8 | 29.3 | E |
| | Left Turn | 24 | 22 | 89.6% | 94.8 | 69.2 | F |
| NE | Through | | | | | | |
| INC | Right Turn | 2 | 2 | 76.8% | 43.4 | 95.3 | D |
| | Subtotal | 26 | 23 | 88.6% | 96.7 | 71.7 | F |
| | Left Turn | 4 | 4 | 96.0% | 63.4 | 59.8 | E |
| WB | Through | 126 | 121 | 95.7% | 37.6 | 16.2 | D |
| VVD | Right Turn | 215 | 206 | 95.7% | 46.5 | 21.6 | D |
| | Subtotal | 345 | 330 | 95.7% | 43.7 | 15.3 | D |
| | Total | 2,855 | 2,536 | 88.8% | 71.2 | 18.1 | E |

Stockton & T E+P PM Peak Hour

| 12/22/20 |)14 |
|----------|-----|
|----------|-----|

Intersection: 3: Stockton Boulevard & T Street

| Movement | EB | EB | WB | WB | NB | NB | NB | SB | SB | SB | NE | |
|-----------------------|------|-----|--|-----|--|------|------|-----|-----|-----|-----------|--|
| Directions Served | LT | TR> | <lt< td=""><td>R</td><td><l< td=""><td>Т</td><td>TR</td><td>L</td><td>Т</td><td>TR></td><td><lr></lr></td><td></td></l<></td></lt<> | R | <l< td=""><td>Т</td><td>TR</td><td>L</td><td>Т</td><td>TR></td><td><lr></lr></td><td></td></l<> | Т | TR | L | Т | TR> | <lr></lr> | |
| Maximum Queue (ft) | 518 | 404 | 125 | 170 | 69 | 1122 | 1153 | 137 | 103 | 134 | 60 | |
| Average Queue (ft) | 346 | 314 | 49 | 93 | 16 | 670 | 710 | 90 | 63 | 87 | 35 | |
| 95th Queue (ft) | 633 | 467 | 135 | 209 | 72 | 1115 | 1135 | 199 | 110 | 146 | 78 | |
| Link Distance (ft) | 1512 | | 176 | 176 | | 3144 | 3144 | 117 | 117 | 117 | 336 | |
| Upstream Blk Time (%) | | | 3 | 9 | | | | 28 | 0 | 2 | | |
| Queuing Penalty (veh) | | | 5 | 15 | | | | 45 | 0 | 4 | | |
| Storage Bay Dist (ft) | | 425 | | | 100 | | | | | | | |
| Storage Blk Time (%) | 7 | 4 | | | 0 | 10 | | | | | | |
| Queuing Penalty (veh) | 31 | 12 | | | 0 | 7 | | | | | | |

APPENDIX D: CUMULATIVE PLUS PROJECT INTERSECTION CONDITIONS



SimTraffic Post-Processor Average Data from 10 Runs Intersection Volume and Delay

| Stockton & T |
|--------------------------------|
| Cumulative Plus Project |
| AM Peak Hour |

| | | Demand Served Volume (vph) | | | | | | | | | | |
|---|------------------------|----------------------------|------------------|-----------------|-----------------------|----------------|----------------|-----------------|------------|---------------------------|--------------|--------|
| Intersection | Control | Volume | Average | Percent | Standard Deviation | Minimum | Maximum | Average | | al Delay (sec/ Minimum | | LOS |
| | | (vph) 3,401 | Average 2,954 | Served 86.9% | 85 | 2,776 | 3,088 | Average 31.1 | 1.4 | 29.3 | 33.6 | |
| Stockton/35th-HWY 50 WB ramps Stockton/none-HWY 50 on ramp | Signal Uncontrolled | 3,401 2,969 | 2,954 2,449 | 86.9% 82.5% | 85 90 | 2,776 2,240 | 3,088 2,560 | 31.1 18.4 | 1.4 3.2 | 29.3 14.1 | 33.6 24.5 | C C |
| 4 37th/T St | Side-street Stop | 2,909 | 520 | 67.4% | 90 57 | 428 | 2,300 616 | 6.3 | 3.4 | 0.0 | 24.5 12.9 | A |
| 5 39th/T St | Signal | 1,216 | 925 | 76.1% | 67 | 428 796 | 1,012 | 0.5 15.7 | 5.4 1.1 | 0.0 14.1 | 12.9 | B |
| 6 39th/S St | Side-street Stop | 617 | 523 | 84.7% | 37 | 468 | 592 | 8.0 | 5.6 | 0.0 | 17.1 | A |
| 0 39(1)33(| Side-street Stop | 017 | 525 | 04.7% | 57 | 400 | 592 | 8.0 | 5.0 | 0.0 | 10.1 | A |
| | | | | | | | | | | | | |
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| | | | | | | | | | | | | |
| | | | | ~~ ~~ / | | | | | | | | _ |
| 3 Stockton/T St | Signal | 3,410 | 2,847 | 83.5% | 84 | 2,704 | 2,948 | 37.0 | 12.9 | 25.1 | 65.1 | D |
| Network Summary | | | | | | | | | | | | |
| Total Demand Volume (veh/hr) | 12,384 | | | | | | | | | | | |
| Total Volume Served (veh/hr) | 10,218 | | | | | | | | | | | |
| Percent Served | 82.5% | | | | | | | | | | | |
| GEH Statistic | 20.4 | | | | | | | | | | | |
| SET Statistic | L 20.4 | | | | | | | | | | | |

Stockton & T Cumulative Plus Project AM Peak Hour

Intersection 1

Stockton/35th-HWY 50 WB ramps

Signal

| | | Demand | Served Vo | lume (vph) | Total | Delay (sec/ve | h) |
|-----------|------------|--------------|-----------|------------|---------|---------------|-----|
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS |
| | Left Turn | 14 | 7 | 48.6% | 29.1 | 24.2 | С |
| NB | Through | 636 | 601 | 94.5% | 16.5 | 1.0 | В |
| IND | Right Turn | 682 | 406 | 59.5% | 7.1 | 0.4 | А |
| | Subtotal | 1,332 | 1,014 | 76.1% | 12.9 | 0.7 | В |
| | Left Turn | 73 | 54 | 74.0% | 32.1 | 6.4 | С |
| SB | Through | 868 | 699 | 80.6% | 15.9 | 2.6 | В |
| 30 | Right Turn | 8 | 2 | 20.0% | 1.4 | 3.3 | А |
| | Subtotal | 949 | 755 | 79.5% | 16.9 | 2.5 | В |
| | Left Turn | 44 | 10 | 22.7% | 25.2 | 13.0 | С |
| EB | Through | 49 | 60 | 122.4% | 34.1 | 9.5 | С |
| ED | Right Turn | 30 | 70 | 232.0% | 18.2 | 8.9 | В |
| | Subtotal | 123 | 140 | 113.5% | 25.8 | 8.6 | С |
| | Left Turn | 194 | 296 | 152.8% | 66.0 | 14.6 | E |
| WB | Through | 168 | 96 | 56.9% | 70.4 | 17.6 | Е |
| VVD | Right Turn | 635 | 654 | 103.0% | 54.3 | 6.7 | D |
| | Subtotal | 997 | 1,046 | 104.9% | 59.6 | 4.1 | E |
| | Total | 3,401 | 2,954 | 86.9% | 31.1 | 1.4 | С |

Intersection 2

Stockton/none-HWY 50 on ramp

Uncontrolled

| | | Demand | Served Vo | lume (vph) | Total | Delay (sec/ve | h) |
|-----------|------------|--------------|-----------|------------|---------|---------------|-----|
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS |
| | Left Turn | | | | | | |
| NB | Through | 1,332 | 1,015 | 76.2% | 1.2 | 0.1 | А |
| IND | Right Turn | 537 | 352 | 65.5% | 1.1 | 0.1 | А |
| | Subtotal | 1,869 | 1,366 | 73.1% | 1.1 | 0.1 | А |
| | Left Turn | 440 | 370 | 84.0% | 18.4 | 3.2 | С |
| SB | Through | 660 | 713 | 108.0% | 1.1 | 0.1 | А |
| 30 | Right Turn | | | | | | |
| | Subtotal | 1,100 | 1,082 | 98.4% | 7.0 | 1.2 | А |
| | Left Turn | | | | | | |
| EB | Through | | | | | | |
| LD | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| | Left Turn | | | | | | |
| WB | Through | | | | | | |
| VV B | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| | Total | 2,969 | 2,449 | 82.5% | 3.7 | 0.5 | А |

Stockton & T Cumulative Plus Project AM Peak Hour

Intersection 4

37th/T St

Side-street Stop

| | | Demand | Served Vo | lume (vph) | Total Delay (sec/veh) | | | |
|-----------|------------|--------------|-----------|------------|-----------------------|-----------|-----|--|
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS | |
| | Left Turn | | | | | | | |
| NB | Through | | | | | | | |
| IND | Right Turn | | | | | | | |
| | Subtotal | | | | | | | |
| | Left Turn | 4 | 9 | 230.0% | 6.3 | 3.4 | А | |
| SB | Through | | | | | | | |
| 30 | Right Turn | 27 | 41 | 152.6% | 3.1 | 0.4 | А | |
| | Subtotal | 31 | 50 | 162.6% | 3.8 | 0.7 | А | |
| | Left Turn | 62 | 22 | 36.1% | 4.5 | 1.8 | А | |
| EB | Through | 331 | 252 | 76.0% | 2.2 | 0.2 | А | |
| ED | Right Turn | | | | | | | |
| | Subtotal | 393 | 274 | 69.7% | 2.4 | 0.2 | А | |
| | Left Turn | | | | | | | |
| WB | Through | 341 | 189 | 55.5% | 1.2 | 0.2 | А | |
| VVD | Right Turn | 6 | 6 | 106.7% | 1.2 | 1.2 | А | |
| | Subtotal | 347 | 196 | 56.4% | 1.2 | 0.2 | А | |
| | Total | 771 | 520 | 67.4% | 2.1 | 0.1 | А | |

Intersection 5

39th/T St

| | I | Demand | Served Vo | lume (vph) | Total | Delay (sec/vel | h) |
|-----------|------------|--------------|-----------|------------|---------|----------------|-----|
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS |
| | Left Turn | 28 | 19 | 67.1% | 16.9 | 7.1 | В |
| NB | Through | 198 | 160 | 80.8% | 13.6 | 2.5 | В |
| IND | Right Turn | 33 | 18 | 55.8% | 7.5 | 4.3 | А |
| | Subtotal | 259 | 197 | 76.1% | 13.3 | 2.7 | В |
| | Left Turn | 46 | 57 | 123.5% | 31.3 | 5.5 | С |
| SB | Through | 158 | 164 | 104.1% | 29.8 | 2.7 | С |
| 30 | Right Turn | 57 | 54 | 95.4% | 22.5 | 2.5 | С |
| | Subtotal | 261 | 276 | 105.6% | 28.6 | 2.9 | С |
| | Left Turn | 50 | 16 | 31.2% | 15.0 | 7.0 | В |
| EB | Through | 262 | 180 | 68.5% | 10.8 | 1.4 | В |
| LD | Right Turn | 23 | 62 | 269.6% | 6.8 | 1.5 | А |
| | Subtotal | 335 | 257 | 76.8% | 10.1 | 1.6 | В |
| | Left Turn | 21 | 10 | 45.7% | 16.6 | 15.9 | В |
| WB | Through | 262 | 124 | 47.2% | 7.7 | 1.7 | А |
| VVD | Right Turn | 78 | 62 | 79.5% | 4.2 | 1.1 | А |
| | Subtotal | 361 | 195 | 54.1% | 6.9 | 1.3 | А |
| | Total | 1,216 | 925 | 76.1% | 15.7 | 1.1 | В |

Stockton & T Cumulative Plus Project AM Peak Hour

Intersection 6

39th/S St

Side-street Stop

| | I | Demand | Served Vo | lume (vph) | Total | Delay (sec/vel | h) |
|-----------|------------|--------------|-----------|------------|---------|----------------|-----|
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS |
| | Left Turn | 2 | 2 | 80.0% | 1.0 | 1.4 | Α |
| NB | Through | 322 | 237 | 73.5% | 1.1 | 0.1 | А |
| IND | Right Turn | 2 | 0 | 0.0% | 0.0 | 0.0 | А |
| | Subtotal | 326 | 238 | 73.1% | 1.1 | 0.1 | А |
| | Left Turn | 1 | 0 | 0.0% | 0.0 | 0.0 | А |
| SB | Through | 255 | 266 | 104.3% | 0.3 | 0.2 | А |
| 30 | Right Turn | 14 | 5 | 34.3% | 0.0 | 0.0 | А |
| | Subtotal | 270 | 271 | 100.3% | 0.3 | 0.2 | А |
| | Left Turn | 15 | 7 | 48.0% | 8.0 | 5.6 | А |
| EB | Through | | | | | | |
| ED | Right Turn | 6 | 6 | 106.7% | 4.7 | 4.3 | А |
| | Subtotal | 21 | 14 | 64.8% | 6.0 | 2.9 | А |
| | Left Turn | | | | | | |
| WB | Through | | | | | | |
| VVD | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| | Total | 617 | 523 | 84.7% | 0.8 | 0.2 | А |

Intersection 0

Side-street Stop

| | [| Demand | Served Vo | lume (vph) | Total | Delay (sec/ve | n) |
|-----------|------------|--------------|-----------|------------|---------|---------------|-----|
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS |
| | Left Turn | | | | | | |
| NB | Through | | | | | | |
| ND | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| | Left Turn | | | | | | |
| SB | Through | | | | | | |
| 30 | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| | Left Turn | | | | | | |
| EB | Through | | | | | | |
| LD | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| | Left Turn | | | | | | |
| WB | Through | | | | | | |
| VVD | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| | Total | | | | | | |

Intersection 3

Stockton/T St

| | | Demand Served Volume (vph) Total Delay (sec, | | | | | h) |
|-----------|------------|--|-------------|-----------|---------|--|-----|
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS |
| | Left Turn | 123 | 44 | 35.4% | 40.2 | 10.4 | D |
| NB | Through | 1,423 | 1,062 | 74.7% | 21.1 | 2.4 | С |
| ND | Right Turn | 12 | 22 | 180.0% | 19.0 | 10.0 | В |
| | Subtotal | 1,558 | 1,128 72.4% | | 21.8 | 2.7 | С |
| | Left Turn | 58 | 38 | 66.2% | 59.3 | 19.010.021.82.759.319.212.91.412.75.815.42.575.248.671.447.688.151.8 | |
| SB | Through | 569 | 654 | 115.0% | 12.9 | 1.4 | В |
| 50 | Right Turn | 33 | 21 | 64.2% | 12.7 | 5.8 | В |
| | Subtotal | 660 | 714 | 108.2% | 15.4 | 2.5 | В |
| | Left Turn | 194 | 103 | 53.2% | 75.2 | 48.6 | Е |
| EB | Through | 323 | 213 | 66.0% | 71.4 | 47.6 | Е |
| ED | Right Turn | 282 | 439 | 155.7% | 88.1 | 51.8 | F |
| | Subtotal | 799 | 756 | 94.6% | 81.5 | 49.6 | F |
| | Left Turn | 24 | | | 5.4 | D | |
| NE | Through | | | | | | |
| INE | Right Turn | 1 | 3 | 280.0% | 34.2 | 23.3 | С |
| | Subtotal | 25 | 28 | 113.6% | 40.5 | 4.3 | D |
| | Left Turn | 6 | 9 | 146.7% | 76.7 | 57.9 | Е |
| WB | Through | 138 | 58 | 41.7% | 43.6 | 36.6 | D |
| VVB | Right Turn | 224 | 155 | 69.1% | 20.8 | 4.2 | С |
| | Subtotal | 368 | 221 | 221 60.1% | | 11.8 | С |
| | Total | 3,410 | 2,847 | 83.5% | 37.0 | 12.9 | D |

AM Peak Hour

Signal

Stockton & T

Cumulative Plus Project

SimTraffic Post-Processor Average Data from 10 Runs Intersection Volume and Delay

| Stockton & T |
|--------------------------------|
| Cumulative Plus Project |
| PM Peak Hour |

| VolumeVolumePercentStandardTotal Delay (sec/veh)IntersectionControl(vph)AverageServedDeviationMinimumMaximumAverageStd. Dev.MinimumMaximum1Stockton/35th-HWY 50 WB rampsSignal3,4013,06890.2%612,9563,13255.719.737.490.62Stockton/none-HWY 50 on rampUncontrolled2,9692,49684.1%812,3322,588108.019.068.3135.3437th/T StSide-street Stop77168288.5%6354074422.362.70.0200.1 | LOS E F C |
|--|--------------------|
| 2 Stockton/none-HWY 50 on ramp Uncontrolled 2,969 2,496 84.1% 81 2,332 2,588 108.0 19.0 68.3 135.3 | F |
| | • |
| 4 27th /T St Side street Step 771 692 99 5% 62 540 744 222 627 0.0 2001 | С |
| 4 37th/T St Side-street Stop 771 682 88.5% 63 540 744 22.3 62.7 0.0 200.1 | |
| 5 39th/T St Signal 1,216 1,127 92.7% 48 1,012 1,200 16.6 1.6 15.5 20.6 | В |
| 6 39th/S St Side-street Stop 617 584 94.7% 64 488 680 7.1 2.0 4.5 10.7 | Α |
| | |
| 3 Stockton/T St Signal 3,410 2,846 83.4% 152 2,564 3,056 185.2 23.8 141.1 224.9 | F |
| Network Summary | |
| Total Demand Volume (veh/hr) 12,384 | |
| Total Volume Served (veh/hr) 10,803 | |
| Percent Served 87.2% | |
| GEH Statistic 14.7 | |

Stockton & T Cumulative Plus Project PM Peak Hour

Intersection 1

Stockton/35th-HWY 50 WB ramps

Signal

| | | Demand | Served Vo | lume (vph) | Total | Delay (sec/ve | h) |
|-----------|------------|--------------|-----------|------------|---------|---------------|-----|
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS |
| | Left Turn | 14 | 8 | 60.0% | 50.9 | 8.2 | D |
| NB | Through | 636 | 500 | 78.6% | 18.0 | 2.3 | В |
| IND | Right Turn | 682 | 524 | 76.8% | 108.9 | 7.9 | F |
| | Subtotal | 1,332 | 1,032 | 77.5% | 64.6 | 6.3 | E |
| | Left Turn | 73 | 71 | 97.5% | 104.3 | 66.7 | F |
| SB | Through | 868 | 859 | 98.9% | 75.0 | 57.6 | E |
| 50 | Right Turn | 8 | 9 | 115.0% | 24.5 | 16.5 | С |
| | Subtotal | 949 | 939 | 99.0% | 76.9 | 57.9 | E |
| | Left Turn | 44 | 43 | 98.2% | 44.5 | 16.6 | D |
| EB | Through | 49 | 54 | 110.2% | 56.1 | 11.8 | E |
| LD | Right Turn | 30 | 26 | 88.0% | 36.2 | 23.6 | D |
| | Subtotal | 123 | 124 | 100.5% | 48.0 | 15.5 | D |
| | Left Turn | 194 | 184 | 94.8% | 38.5 | 15.1 | D |
| WB | Through | 168 | 174 | 103.6% | 39.5 | 13.8 | D |
| VVD | Right Turn | 635 | 615 | 96.9% | 21.4 | 8.7 | С |
| | Subtotal | 997 | 973 | 97.6% | 28.0 | 9.8 | С |
| | Total | 3,401 | 3,068 | 90.2% | 55.7 | 19.7 | E |

Intersection 2

Stockton/none-HWY 50 on ramp

Uncontrolled

| | | Demand | Served Vo | lume (vph) | Total | Delay (sec/ve | h) |
|-----------|------------|--------------|-----------|------------|---------|---------------|-----|
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS |
| | Left Turn | | | | | | |
| NB | Through | 1,332 | 1,034 | 77.7% | 11.1 | 3.7 | В |
| IND | Right Turn | 537 | 407 | 75.8% | 10.5 | 3.8 | В |
| | Subtotal | 1,869 | 1,441 | 77.1% | 11.0 | 3.7 | В |
| | Left Turn | 440 | 400 | 90.8% | 108.0 | 19.0 | F |
| SB | Through | 660 | 655 | 99.3% | 3.9 | 5.5 | А |
| 30 | Right Turn | | | | | | |
| | Subtotal | 1,100 | 1,055 | 95.9% | 43.1 | 8.8 | E |
| | Left Turn | | | | | | |
| EB | Through | | | | | | |
| LD | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| | Left Turn | | | | | | |
| WB | Through | | | | | | |
| VVD | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| | Total | 2,969 | 2,496 | 84.1% | 24.3 | 3.7 | С |

Stockton & T Cumulative Plus Project PM Peak Hour

Intersection 4

37th/T St

Side-street Stop

| | | Demand | Served Vo | lume (vph) | Total | Delay (sec/ve | h) |
|-----------|------------|--------------|-----------|------------|---------|---------------|-----|
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS |
| | Left Turn | | | | | | |
| NB | Through | | | | | | |
| IND | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| | Left Turn | 4 | 5 | 130.0% | 12.2 | 27.0 | В |
| SB | Through | | | | | | |
| 30 | Right Turn | 27 | 23 | 84.4% | 18.6 | 24.1 | С |
| | Subtotal | 31 | 28 | 90.3% | 17.8 | 23.5 | С |
| | Left Turn | 62 | 56 | 91.0% | 6.7 | 1.5 | Α |
| EB | Through | 331 | 263 | 79.5% | 3.9 | 0.2 | А |
| ED | Right Turn | | | | | | |
| | Subtotal | 393 | 320 | 81.3% | 4.5 | 0.5 | А |
| | Left Turn | | | | | | |
| WB | Through | 341 | 328 | 96.3% | 13.5 | 20.8 | В |
| VVD | Right Turn | 6 | 6 | 106.7% | 22.3 | 62.7 | С |
| | Subtotal | 347 | 335 | 96.5% | 13.4 | 20.8 | В |
| | Total | 771 | 682 | 88.5% | 9.6 | 10.6 | А |

Intersection 5

39th/T St

| | I | Demand | Served Vo | lume (vph) | Total Delay (sec/veh) | | | | |
|-----------|------------|--------------|-----------|------------|-----------------------|-----------|-----|--|--|
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS | | |
| | Left Turn | 28 | 37 | 132.9% | 15.5 | 7.0 | В | | |
| NB | Through | 198 | 191 | 96.6% | 17.2 | 1.6 | В | | |
| IND | Right Turn | 33 | 38 | 113.9% | 10.6 | 3.8 | В | | |
| | Subtotal | 259 | 266 | 102.7% | 16.1 | 2.2 | В | | |
| | Left Turn | 46 | 41 | 88.7% | 38.5 | 9.9 | D | | |
| SB | Through | 158 | 155 | 98.0% | 33.0 | 3.5 | С | | |
| 30 | Right Turn | 57 | 59 | 103.2% | 26.8 | 5.4 | С | | |
| | Subtotal | 261 | 254 | 97.5% | 32.2 | 2.6 | С | | |
| | Left Turn | 50 | 37 | 74.4% | 15.7 | 3.5 | В | | |
| EB | Through | 262 | 209 | 79.7% | 10.5 | 1.6 | В | | |
| LD | Right Turn | 23 | 23 | 99.1% | 5.3 | 3.6 | А | | |
| | Subtotal | 335 | 269 | 80.2% | 10.9 | 1.4 | В | | |
| | Left Turn | 21 | 20 | 93.3% | 11.6 | 4.8 | В | | |
| WB | Through | 262 | 242 | 92.4% | 10.2 | 2.7 | В | | |
| VVD | Right Turn | 78 | 76 | 97.9% | 6.8 | 1.5 | А | | |
| | Subtotal | 361 | 338 | 93.6% | 9.5 | 2.2 | А | | |
| | Total | 1,216 | 1,127 | 92.7% | 16.6 | 1.6 | В | | |

Stockton & T Cumulative Plus Project PM Peak Hour

Intersection 6

39th/S St

Side-street Stop

| | I | Demand | Served Vo | lume (vph) | Total | Delay (sec/vel | h) |
|-----------|------------|--------------|-----------------|------------|---------|----------------|-----|
| Direction | Movement | Volume (vph) | Average Percent | | Average | Std. Dev. | LOS |
| | Left Turn | 2 | 0 | 20.0% | 0.3 | 0.9 | Α |
| NB | Through | 322 | 304 | 94.3% | 1.2 | 0.1 | А |
| INB | Right Turn | 2 | 3 | 140.0% | 0.3 | 0.6 | А |
| | Subtotal | 326 | 307 | 94.1% | 1.2 | 0.1 | А |
| | Left Turn | 1 | 1 | 80.0% | 0.3 | 0.7 | Α |
| SB | Through | 255 | 245 | 96.0% | 0.4 | 0.1 | А |
| 30 | Right Turn | 14 | 13 | 94.3% | 0.0 | 0.1 | А |
| | Subtotal | 270 | 259 | 95.9% | 0.4 | 0.1 | А |
| | Left Turn | 15 | 12 | 77.3% | 7.1 | 2.0 | Α |
| EB | Through | | | | | | |
| EB | Right Turn | 6 | 7 | 113.3% | 3.3 | 2.3 | А |
| | Subtotal | 21 | 18 | 87.6% | 6.6 | 2.0 | А |
| | Left Turn | | | | | | |
| WB | Through | | | | | | |
| VVB | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| | Total | 617 | 584 | 94.7% | 1.0 | 0.1 | А |

Intersection 0

Side-street Stop

| | | Demand | Served Vol | lume (vph) | Total | Delay (sec/ve | h) |
|-----------|------------|--------------|------------|------------|---------|---------------|-----|
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS |
| | Left Turn | | | | | | |
| NB | Through | | | | | | |
| IND | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| | Left Turn | | | | | | |
| SB | Through | | | | | | |
| 30 | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| | Left Turn | | | | | | |
| EB | Through | | | | | | |
| LD | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| | Left Turn | | | | | | |
| WB | Through | | | | | | |
| VVD | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| | Total | | | | | | |

Intersection 3

Stockton/T St

| | | Demand | Served Vo | lume (vph) | Total | Delay (sec/vel | h) |
|-----------|------------|--------------|-----------|------------|---------|----------------|-----|
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS |
| | Left Turn | 123 | 100 | 81.6% | 331.8 | 44.2 | F |
| NB | Through | 1,423 | 1,038 | 72.9% | 311.4 | 49.3 | F |
| IND | Right Turn | 12 | 6 | 53.3% | 252.1 | 117.7 | F |
| | Subtotal | 1,558 | 1,145 | 73.5% | 312.9 | 48.2 | F |
| | Left Turn | 58 | 39 | 66.9% | 247.4 | 129.8 | F |
| SB | Through | 569 | 570 | 100.1% | 15.4 | 2.1 | В |
| 30 | Right Turn | 33 | 32 | 97.0% | 13.8 | 4.4 | В |
| | Subtotal | 660 | 640 | 97.0% | 29.1 | 6.6 | С |
| | Left Turn | 194 | 158 | 81.2% | 239.6 | 42.8 | F |
| EB | Through | 323 | 273 | 84.5% | 187.5 | 39.2 | F |
| ED | Right Turn | 282 | 252 | 89.5% | 174.0 | 46.3 | F |
| | Subtotal | 799 | 683 | 85.5% | 194.0 | 40.3 | F |
| | Left Turn | 24 | 27 | 113.3% | 81.7 | 36.8 | F |
| NE | Through | | | | | | |
| INE | Right Turn | 1 | 1 | 80.0% | 68.9 | 0.0 | Е |
| | Subtotal | 25 | 28 | 112.0% | 81.6 | 36.8 | F |
| | Left Turn | 6 | 4 | 66.7% | 83.8 | 145.6 | F |
| WB | Through | 138 | 133 | 96.5% | 40.3 | 38.2 | D |
| VVB | Right Turn | 224 | 212 | 94.8% | 54.9 | 28.9 | D |
| | Subtotal | 368 | 350 | 95.0% | 47.3 | 21.6 | D |
| | Total | 3,410 | 2,846 | 83.4% | 185.2 | 23.8 | F |

Signal

Stockton & T

PM Peak Hour

Cumulative Plus Project

APPENDIX E: MITIGATION MEASURES



SimTraffic Post-Processor Average Data from 10 Runs Intersection Volume and Delay

| | | | Demand Volume | Served Volume (vph) Percent Standard | | | Total Delay (sec/veh) | | | | | | |
|------|-------------------------------|------------------|------------------|---|--------|-----------|-----------------------|---------|---------|-----------|---------|---------|-----|
| | Intersection | Control | (vph) | Average | Served | Deviation | Minimum | Maximum | Average | Std. Dev. | Minimum | Maximum | LOS |
| 1 | Stockton/35th-HWY 50 WB ramps | Signal | 3,401 | 3,148 | 92.5% | 89 | 2,960 | 3,256 | 32.8 | 7.1 | 20.2 | 40.0 | С |
| 2 | Stockton/none-HWY 50 on ramp | Uncontrolled | 2,969 | 2,670 | 89.9% | 106 | 2,464 | 2,828 | 52.7 | 18.6 | 34.6 | 89.6 | F |
| 4 | 37th/T St | Side-street Stop | 771 | 717 | 93.0% | 51 | 612 | 768 | 28.0 | 65.5 | 2.4 | 212.3 | D |
| 5 | 39th/T St | Signal | 1,216 | 1,125 | 92.5% | 32 | 1,080 | 1,160 | 18.3 | 2.2 | 14.6 | 23.0 | В |
| 6 | 39th/S St | Side-street Stop | 617 | 588 | 95.4% | 34 | 528 | 636 | 7.2 | 2.9 | 0.0 | 9.8 | А |
| | | | | | | | | | | | | | |
| 3 | Stockton/T St | Signal | 3,410 | 2,986 | 87.6% | 122 | 2,736 | 3,148 | 181.5 | 12.4 | 161.0 | 195.7 | F |
| | Network Summary | | | | | | | | | | | | |
| Tota | al Demand Volume (veh/hr) | 12,384 | | | | | | | | | | | |
| | al Volume Served (veh/hr) | 11,234 | | | | | | | | | | | |
| | cent Served | 90.7% | | | | | | | | | | | |
| | I Statistic | 10.6 | | | | | | | | | | | |
| | | | | | | | | | | | | | |

Stockton & T Cumulative Plus Project NB/SB protected left turn PM Peak Hour

Intersection 1

Stockton/35th-HWY 50 WB ramps

Signal

| | | Demand | Served Vo | lume (vph) | Total | Total Delay (sec/veh) | | |
|-----------|------------|--------------|-----------|------------|---------|-----------------------|-----|--|
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS | |
| | Left Turn | 14 | 10 | 74.3% | 40.3 | 20.9 | D | |
| NB | Through | 636 | 558 | 87.7% | 18.1 | 2.8 | В | |
| ND | Right Turn | 682 | 546 | 80.1% | 55.3 | 38.3 | Е | |
| | Subtotal | 1,332 | 1,115 | 83.7% | 36.8 | 20.2 | D | |
| | Left Turn | 73 | 63 | 86.6% | 39.1 | 7.0 | D | |
| SB | Through | 868 | 870 | 100.2% | 22.1 | 4.5 | С | |
| 50 | Right Turn | 8 | 7 | 85.0% | 12.3 | 9.9 | В | |
| | Subtotal | 949 | 940 | 99.0% | 23.2 | 4.6 | С | |
| | Left Turn | 44 | 45 | 101.8% | 47.8 | 20.0 | D | |
| EB | Through | 49 | 49 | 100.4% | 50.1 | 23.6 | D | |
| LD | Right Turn | 30 | 38 | 125.3% | 34.4 | 22.7 | С | |
| | Subtotal | 123 | 132 | 107.0% | 44.6 | 20.3 | D | |
| | Left Turn | 194 | 194 | 99.8% | 44.6 | 16.2 | D | |
| WB | Through | 168 | 165 | 98.1% | 46.1 | 17.8 | D | |
| | Right Turn | 635 | 603 | 95.0% | 29.4 | 14.2 | С | |
| | Subtotal | 997 | 962 | 96.4% | 36.0 | 14.0 | D | |
| | Total | 3,401 | 3,148 | 92.5% | 32.8 | 7.1 | С | |

Intersection 2

Stockton/none-HWY 50 on ramp

Uncontrolled

| | | Demand | Served Vo | lume (vph) | Total Delay (sec/veh) | | | |
|-----------|------------|--------------|-----------|------------|-----------------------|-----------|-----|--|
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS | |
| | Left Turn | | | | | | | |
| NB | Through | 1,332 | 1,118 | 83.9% | 3.4 | 2.9 | А | |
| IND | Right Turn | 537 | 461 | 85.8% | 3.1 | 2.6 | А | |
| | Subtotal | 1,869 | 1,579 | 84.5% | 3.3 | 2.8 | А | |
| | Left Turn | 440 | 424 | 96.3% | 52.7 | 18.6 | F | |
| SB | Through | 660 | 667 | 101.1% | 1.6 | 0.3 | А | |
| 30 | Right Turn | | | | | | | |
| | Subtotal | 1,100 | 1,091 | 99.2% | 21.3 | 7.2 | С | |
| | Left Turn | | | | | | | |
| EB | Through | | | | | | | |
| LD | Right Turn | | | | | | | |
| | Subtotal | | | | | | | |
| | Left Turn | | | | | | | |
| WB | Through | | | | | | | |
| | Right Turn | | | | | | | |
| | Subtotal | | | | | | | |
| | Total | 2,969 | 2,670 | 89.9% | 10.6 | 3.2 | В | |

Stockton & T Cumulative Plus Project NB/SB protected left turn PM Peak Hour

Intersection 4

37th/T St

Side-street Stop

| | | Demand | Served Volume (vph) | | Total | al Delay (sec/veh) | | |
|-----------|------------|--------------|---------------------|---------|---------|--------------------|-----|--|
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS | |
| | Left Turn | | | | | | | |
| NB | Through | | | | | | | |
| ND | Right Turn | | | | | | | |
| | Subtotal | | | | | | | |
| | Left Turn | 4 | 4 | 90.0% | 22.7 | 66.0 | С | |
| SB | Through | | | | | | | |
| 30 | Right Turn | 27 | 26 | 97.8% | 28.0 | 65.5 | D | |
| | Subtotal | 31 | 30 | 96.8% | 27.9 | 65.3 | D | |
| | Left Turn | 62 | 58 | 92.9% | 6.4 | 1.5 | Α | |
| EB | Through | 331 | 276 | 83.5% | 3.7 | 0.3 | А | |
| LD | Right Turn | | | | | | | |
| | Subtotal | 393 | 334 | 85.0% | 4.2 | 0.4 | А | |
| | Left Turn | | | | | | | |
| WB | Through | 341 | 344 | 100.9% | 11.7 | 22.3 | В | |
| VVB | Right Turn | 6 | 9 | 153.3% | 8.8 | 22.8 | Α | |
| | Subtotal | 347 | 353 | 101.8% | 11.7 | 22.4 | В | |
| | Total | 771 | 717 | 93.0% | 9.1 | 14.3 | А | |

Intersection 5

39th/T St

| | | Demand | Served Vo | lume (vph) | Total | Total Delay (sec/veh) | | |
|-----------|------------|--------------|-----------|------------|---------|-----------------------|-----|--|
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS | |
| | Left Turn | 28 | 26 | 92.9% | 17.7 | 7.8 | В | |
| NB | Through | 198 | 193 | 97.6% | 15.9 | 3.6 | В | |
| IND | Right Turn | 33 | 29 | 88.5% | 9.5 | 4.4 | А | |
| | Subtotal | 259 | 248 | 95.9% | 15.2 | 3.0 | В | |
| | Left Turn | 46 | 40 | 87.0% | 43.5 | 6.8 | D | |
| SB | Through | 158 | 156 | 98.5% | 37.2 | 4.9 | D | |
| 30 | Right Turn | 57 | 69 | 120.7% | 32.0 | 5.5 | С | |
| | Subtotal | 261 | 264 | 101.3% | 36.6 | 4.4 | D | |
| | Left Turn | 50 | 34 | 68.8% | 17.9 | 4.8 | В | |
| EB | Through | 262 | 219 | 83.5% | 11.7 | 3.8 | В | |
| LD | Right Turn | 23 | 16 | 71.3% | 7.0 | 5.2 | А | |
| | Subtotal | 335 | 270 | 80.5% | 12.2 | 3.4 | В | |
| | Left Turn | 21 | 18 | 83.8% | 17.0 | 5.2 | В | |
| WB | Through | 262 | 252 | 96.2% | 11.5 | 4.2 | В | |
| | Right Turn | 78 | 73 | 93.3% | 7.4 | 3.3 | А | |
| | Subtotal | 361 | 342 | 94.8% | 10.9 | 3.6 | В | |
| | Total | 1,216 | 1,125 | 92.5% | 18.3 | 2.2 | В | |

Stockton & T Cumulative Plus Project NB/SB protected left turn PM Peak Hour

Intersection 6

39th/S St

Side-street Stop

| | | Demand | Served Vo | Served Volume (vph) | | tal Delay (sec/veh) | | |
|-----------|------------|--------------|-----------|---------------------|---------|---------------------|-----|--|
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS | |
| | Left Turn | 2 | 2 | 80.0% | 1.6 | 2.1 | А | |
| NB | Through | 322 | 297 | 92.3% | 1.2 | 0.1 | А | |
| ND | Right Turn | 2 | 3 | 160.0% | 0.5 | 0.8 | А | |
| | Subtotal | 326 | 302 | 92.6% | 1.2 | 0.1 | А | |
| | Left Turn | 1 | 0 | 40.0% | 0.2 | 0.6 | Α | |
| SB | Through | 255 | 252 | 98.7% | 0.5 | 0.4 | А | |
| 30 | Right Turn | 14 | 14 | 97.1% | 0.2 | 0.2 | А | |
| | Subtotal | 270 | 266 | 98.4% | 0.5 | 0.4 | А | |
| | Left Turn | 15 | 13 | 88.0% | 7.2 | 2.9 | А | |
| EB | Through | | | | | | | |
| ED | Right Turn | 6 | 8 | 126.7% | 4.0 | 2.3 | А | |
| | Subtotal | 21 | 21 | 99.0% | 6.5 | 1.7 | А | |
| | Left Turn | | | | | | | |
| WB | Through | | | | | | | |
| | Right Turn | | | | | | | |
| | Subtotal | | | | | | | |
| | Total | 617 | 588 | 95.4% | 1.1 | 0.2 | А | |

Intersection 0

Side-street Stop

| | | Demand | Served Volume (vph) | | Total Delay (sec/veh) | | |
|-----------|------------|--------------|---------------------|---------|-----------------------|-----------|-----|
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS |
| | Left Turn | | | | | | |
| NB | Through | | | | | | |
| IND | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| | Left Turn | | | | | | |
| SB | Through | | | | | | |
| 30 | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| | Left Turn | | | | | | |
| EB | Through | | | | | | |
| LD | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| WB | Left Turn | | | | | | |
| | Through | | | | | | |
| | Right Turn | | | | | | |
| | Subtotal | | | | | | |
| | Total | | | | | | |

Stockton & T Cumulative Plus Project NB/SB protected left turn PM Peak Hour

Intersection 3

Stockton/T St

| | | Demand | Served Vo | lume (vph) | Total | Total Delay (sec/veh) | | |
|-----------|------------|--------------|-----------|------------|---------|-----------------------|-----|--|
| Direction | Movement | Volume (vph) | Average | Percent | Average | Std. Dev. | LOS | |
| | Left Turn | 123 | 95 | 77.1% | 325.1 | 52.5 | F | |
| NB | Through | 1,423 | 1,150 | 80.8% | 298.8 | 40.6 | F | |
| IND | Right Turn | 12 | 7 | 56.7% | 265.7 | 136.5 | F | |
| | Subtotal | 1,558 | 1,252 | 80.3% | 300.6 | 41.5 | F | |
| | Left Turn | 58 | 48 | 83.4% | 105.2 | 53.4 | F | |
| SB | Through | 569 | 560 | 98.3% | 21.3 | 1.7 | С | |
| 30 | Right Turn | 33 | 40 | 122.4% | 17.6 | 4.7 | В | |
| | Subtotal | 660 | 648 | 98.2% | 27.0 | 3.9 | С | |
| | Left Turn | 194 | 178 | 92.0% | 227.7 | 64.8 | F | |
| EB | Through | 323 | 278 | 85.9% | 188.1 | 58.2 | F | |
| EB | Right Turn | 282 | 232 | 82.3% | 184.9 | 54.0 | F | |
| | Subtotal | 799 | 688 | 86.1% | 197.4 | 57.1 | F | |
| | Left Turn | 24 | 21 | 86.7% | 47.4 | 13.2 | D | |
| NE | Through | | | | | | | |
| INE | Right Turn | 1 | 2 | 240.0% | 33.6 | 36.1 | С | |
| | Subtotal | 25 | 23 | 92.8% | 44.9 | 9.9 | D | |
| | Left Turn | 6 | 7 | 113.3% | 43.8 | 50.0 | D | |
| WB | Through | 138 | 137 | 99.1% | 43.5 | 22.9 | D | |
| | Right Turn | 224 | 232 | 103.4% | 33.7 | 5.3 | С | |
| | Subtotal | 368 | 375 | 102.0% | 38.5 | 10.7 | D | |
| | Total | 3,410 | 2,986 | 87.6% | 181.5 | 12.4 | F | |